

APPENDIX I
MAJOR MATERIAL DISPOSAL AREA
REMEDICATION, CANYON CLEANUPS, AND OTHER
CONSENT ORDER ACTIONS

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MAJOR MATERIAL DISPOSAL AREA REMEDIATION, CANYON CLEANUPS, AND OTHER CONSENT ORDER ACTIONS

Los Alamos National Laboratory (LANL) conducts operations in support of the National Nuclear Security Administration (NNSA), a semi-autonomous administration within the U.S. Department of Energy (DOE). This appendix addresses possible environmental impacts associated with investigations and corrective measures being conducted at LANL in accordance with the Atomic Energy Act of 1954, as amended, and the Resource Conservation and Recovery Act (RCRA) and related legislation, particularly the Hazardous and Solid Waste Amendments (HSWA). RCRA-related investigations and corrective actions will be conducted in accordance with a Compliance Order on Consent¹ (Consent Order) entered into by DOE, the University of California as the management and operating contractor, and the State of New Mexico on March 1, 2005.

The Consent Order includes schedules for completion of investigations and corrective measures by the end of 2015. This appendix accordingly addresses environmental consequences through fiscal year (FY) 2016.

The analyses performed for this Site-Wide Environmental Impact Statement (SWEIS) mainly consider levels of operations and new projects proposed for 2007 through about 2011; the analyses in this appendix consider environmental restoration activities through FY 2016. However, these analyses are applicable to actions that may be taken during this period of time, and if necessary beyond, as long as the actions are bounded by the analytical results presented in this appendix.

Implementing the Consent Order

NNSA intends to implement actions necessary to comply with the Compliance Order on Consent (Consent Order) regardless of decisions it makes on other actions analyzed in the LANL SWEIS. Actions associated with implementing the Consent Order are included in the Expanded Operations Alternative; however, their implementation is not contingent on other actions that are part of that alternative.

I.1 Introduction

I.1.1 Need for Agency Action

In accordance with statutes such as RCRA and the Atomic Energy Act, LANL staff has conducted an environmental restoration project to identify locations where radioactive and hazardous constituents may have been released into the environment and to conduct corrective action. These potential release sites (PRSs)² include:

- Material disposal areas (MDAs), where radioactive or hazardous constituents have been disposed of, generally by burial within soil or underlying tuff

¹ The Consent Order can be viewed at http://www.nmenv.state.nm.us/hwb/lanl/OrderConsent/03-01-05/Order_on_Consent_2-24-05.pdf.

² For this SWEIS, a potential release site (PRS) means a site suspected of releasing or having the potential to release contaminants (radioactive, chemical, or both). PRS is a general term that includes solid waste management units and areas of concern that are cited and defined in the March 2005 Consent Order.

- Firing sites, where radioactive or hazardous constituents have been explosively dispersed
- Outfalls, where soils, sediments, water bodies, or aquifers have become contaminated with radioactive or hazardous constituents contained in discharged effluents
- Other areas of possible surface, subsurface, or groundwater contamination

Correction action activities at LANL are regulated primarily by DOE pursuant to the Atomic Energy Act, and by the New Mexico Environment Department (NMED) pursuant to RCRA, HSWA, and the New Mexico Hazardous Waste Act. For activities regulated by NMED, since 1990, LANL has conducted investigations and corrective measures in accordance with its Hazardous Waste Facility Permit. But as of March 1, 2005, the corrective action program specified in the permit was replaced by the Consent Order.

The Consent Order prescribes investigation programs for LANL PRSs subject to RCRA and HSWA requirements. From the investigation program results, a determination may be made that no further action is required, or that corrective measures may be needed. If the latter, interim measures may be performed as directed by NMED or as proposed by DOE and approved by NMED. (Emergency interim measures may be implemented without prior NMED approval). As needed and as directed by NMED, alternative corrective measures may be evaluated. After NMED selects the corrective measures to be implemented at the PRSs, the selected corrective measures are implemented and completions of the corrective measures are documented. Activities to be performed in compliance with the Consent Order are similar to those that have taken place for years at LANL (such as drilling exploratory wells or performing removals). But the timing and extent of some activities may be different from those previously anticipated.

The Consent Order provides schedules for all subject PRS remedy completion. Some schedules are explicitly stated, but most are prescribed through aggregate area schedules for remediation completion. That is, there is a schedule for completing remedies in each aggregate area, and every subject PRS is in an aggregate area. If regulatory delays occur in the investigations or corrective measure selection processes, then the remedy completion schedules are adjusted to account for these delays.

An aggregate area is an area within a single watershed or canyon made up of one or more solid waste management units (SWMUs) and areas of concern (AOCs) and the media affected or potentially affected by SWMUs or AOCs releases and for which investigation or remediation, in part or in entirety, is conducted for the area as a whole to address area-wide contamination, ecological risk assessment, and other factors (NMED 2005).

The majority of investigations and corrective measures that will occur under the Consent Order will probably not be environmentally significant. For example, if a sump formerly used for drainage of liquids containing hazardous constituents is decontaminated, and a small amount of waste products are properly disposed of, then these corrective measures may be of such a short-term nature that they do not require a detailed National Environmental Policy Act (NEPA) analysis. But if a large number of small-scale corrective measures take place, then there may be concerns about the cumulative impacts of all actions. In addition, some corrective measures for some PRSs may be of larger significance in terms of cost, time to complete, and possible short- and long-term environmental impacts.

I.1.2 Purpose and Approach

The purpose of this appendix is to address Consent Order NEPA implications on LANL operations. The following approach is used:

- Review the Consent Order to identify and describe those PRSs that may require investigation or remediation through FY 2016 (Section I.2).
- Address in detail a limited number of large MDAs that may require significant efforts to remediate (Section I.3).
- Aggregate the remaining MDAs and other PRSs where remediation efforts will probably be more significant in totality than individually (Section I.3).
- Analyze a bounding range of remediation options (Section I.3).
- Review the environmental setting, emphasizing site-wide variations (Section I.4).
- Assess environmental impacts of the bounding range of options (Section I.5).

The analysis in this appendix is being conducted in advance of all information to be collected from the LANL corrective measure investigation program and is not meant to circumvent remediation decisions about any PRS. Work being performed to characterize, assess, and provide recommendations for corrective measures at all LANL PRSs may require several years to complete, and decisions will be made in accordance with prescribed regulatory processes. After a decision is reached on an MDA or PRS alternative, implementing that decision may require detailed engineering and safety assessments. Therefore, options in this appendix are meant to bound possible environmental impacts. The analysis is intended to provide information that could be used to develop mitigative measures, if needed, if a particular option is implemented. If it is determined that implementing an option may result in impacts that exceed those considered in this appendix, then additional NEPA review may be needed.

For this appendix, the PRSs that will be investigated and may be remediated through FY 2016 are grouped into large MDAs, small MDAs, and additional PRSs.

MDAs are emphasized because decisions about their remediation may significantly affect site-wide operations and the environment. Because MDAs contain contamination mainly in the subsurface, two broad-scope remediation options are envisioned: stabilization in place or removal (see Section I.1.3). Although several variations or suboptions may be addressed in future analyses, these two options should bound possible environmental impacts.

The large MDAs addressed in this appendix are listed in **Table I-1**. Schedules for submittal of corrective measure reports for these MDAs are presented in **Table I-2**. These MDAs generally contain larger inventories of hazardous and radioactive constituents compared with other MDAs and PRSs. A second group of smaller MDAs is listed in **Table I-3**.

Table I-1 Large Material Disposal Areas

| <i>Technical Area</i> | <i>MDA and SWMU</i> | <i>Description</i> |
|-----------------------|------------------------------------|---|
| TA-21 | MDA A 21-014 | Inactive. Contains two 50,000-gallon underground tanks, two small pits, and one large pit. |
| TA-21 | MDA B 21-015 | Inactive. Used for solid radioactive waste and chemical waste disposal. Uncertain number of disposal trenches. |
| TA-21 | MDA T 21-016(a)-99 | Inactive. Includes four absorption beds, more than 60 shafts, and other potential release sites associated with decommissioned waste treatment facilities and storage areas. Beds received untreated liquids containing plutonium from 1945 to 1952, and treated liquids thereafter until 1967. Liquids included fluoride and ammonium citrate. Shafts contain solids, sludge mixed with cement, and alkaline fluoride. |
| TA-21 ^a | MDA U ^a 21-017 (a-c) | Inactive. Contains two absorption beds used from 1948 to 1968 for subsurface disposal of contaminated liquid wastes. ^a |
| TA-49 | MDA AB 49-001 (a-g) | Inactive. Includes multiple shafts and chambers at depths between 60 and 80 feet that were used from 1959 to 1961 for hydronuclear safety experiments. Contains uranium-235, plutonium-239, solid lead shielding, and beryllium. |
| TA-50 | MDA C 50-009 | Inactive. Contains seven pits and 108 shafts. One chemical waste pit contains pyrophoric metals, hydrides, and powders, sodium-potassium alloy, and compressed gasses. Other pits contain process wastes, demolition waste, classified materials, and tuballoy (a uranium alloy) chips. Shafts were used for disposal of high-surface-exposure waste. |
| TA-54 | MDA G (multiple SWMUs) | MDA G is inactive. It consists of numerous pits and shafts within active Area G, which is used for low-level radioactive waste disposal and transuranic waste storage. Area G is being expanded but a portion will close consistent with the Consent Order requirement to complete corrective action for MDA G by August 2015 and with the need to develop new low-level radioactive waste disposal capacity. |
| TA-54 | MDA L (SWMU-54-006) | Inactive. MDA L was used for waste disposal from 1959 through 1985 (contains one chemical waste disposal pit, 34 disposal shafts, and three chemical waste impoundments). MDA L is within Area L, which is used for storage of RCRA, PCB, and mixed wastes. |

TA = technical area, MDA = material disposal area, SWMU = solid waste management unit, RCRA = Resource Conservation and Recovery Act, PCB = polychlorinated biphenyl.

^a MDA U is smaller than the other MDAs in this table, and, in September 2006, NMED issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b). It was included for purposes of NEPA analysis and because of its location in TA-21.

Note: To convert feet to meters, multiply by 0.3048; gallons to liters, multiply by 3.7854.

Table I-2 Updated Corrective Measure Report Schedules for Large Material Disposal Areas

| <i>MDA</i> | <i>Investigation Work Plan</i> | <i>Investigation Report</i> | <i>CME Work Plan</i> | <i>CME Report</i> | <i>Remedy Completion Report</i> |
|------------|--------------------------------|-----------------------------|----------------------|----------------------|---------------------------------|
| A | Submitted | Submitted | TBD | TBD | 3/11/2011 |
| B | Submitted | Not applicable | Not applicable | Not applicable | 12/31/2010 ^a |
| T | Submitted | Submitted | TBD | TBD | 12/19/2010 |
| U | Submitted | Submitted | TBD | TBD | 11/6/2011 ^b |
| C | Submitted | Submitted | TBD | TBD | 9/5/2010 |
| L | Submitted | Submitted | Submitted | Submitted | 7/9/2011 ^c |
| G | Submitted | Submitted | Submitted | Pending ^d | 12/6/2015 |
| AB | Submitted | 5/31/2010 | TBD | TBD | 1/31/2015 |

MDA = material disposal area, CME = corrective measure evaluation, TBD = to be determined.

^a MDA B will not go through the Corrective Measure Evaluation Process, but will proceed directly to remediation by removal.

^b In September 2006, NMED issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b).

^c The original schedule in the Consent Order was June 30, 2011.

^d Submittal is expected in September 2008.

Note: Current schedules have been approved by NMED and may differ from those in the Consent Order.

Table I-3 Additional Material Disposal Areas

| <i>Technical Area</i> | <i>MDA and SWMU</i> | <i>Description</i> |
|-----------------------|-----------------------|--|
| TA-6 | MDA F 6-007(a) | Contains an uncertain number of pits and trenches. |
| TA-8 | MDA Q 8-006(a) | Inactive site, received waste in 1946 from naval gun experiments for the Little Boy atomic weapon. |
| TA-15 | MDA N 15-007(a) | Small site containing a pit that received demolition wastes. |
| TA-15 | MDA Z 15-007(b) | Small site used from 1965 to 1981 for disposal of construction debris and other wastes. Some wastes are exposed. |
| TA-16 | MDA R 16-019 | Inactive site that received debris from a high-explosives burning ground. It was partially remediated after the Cerro Grande Fire. |
| TA-33 | MDA D 33-003(a, b) | Small site consisting of two underground chambers and elevator shafts used for explosives tests of weapons components. |
| TA-33 | MDA E 33-001(a)-99 | Site contains an underground experimental chamber used for explosives tests plus four disposal pits. |
| TA-33 | MDA K 33-002(a)-99 | Site currently consists of two small surface-disposal areas containing piled debris. |
| TA-36 | MDA AA 36-001 | Small site consists of at least two trenches containing firing site debris. |
| TA-39 | MDA Y 39-001(b) | Small site in Ancho Canyon containing three pits used for disposal of firing site debris. |

MDA = material disposal area, SWMU = solid waste management unit, TA = technical area.

The third group of PRSs comprises hundreds of sites containing low levels of radioactive or hazardous constituents, generally concentrated on the surface of the ground or in the near subsurface. A variety of remediation activities may take place, often requiring removal of relatively small quantities of wastes. These PRSs would be investigated as part of the aggregate area investigations. Schedules for conducting aggregate area investigations are specified in the Consent Order. Once an aggregate area investigation is complete, plans for remediating the PRSs in the aggregate area would be determined. Examples of PRSs composing this last group are shown in **Table I-4**.

Table I-4 Examples of Potential Release Sites Being Addressed Under the Consent Order

| <i>Technical Area</i> | <i>Potential Release Site</i> | <i>Description</i> |
|-----------------------|-------------------------------|---|
| TA-15 | Site E-F 15-004(f)-99 | High-explosives firing site; inactive. |
| TA-15 | Site R-44 15-006(c) | High-explosives firing site; inactive. |
| TA-16 | 260 Outfall 16-021(c)-99 | Site contaminated by outfall from an explosives manufacturing facility. |
| TA-73 | Ash pile 73-002 | Site contaminated by ashes from a former incinerator. |

TA = technical area.

I.1.3 Options Considered in this Appendix

Three broad-scope options are considered for purposes of NEPA:

- **No Action Option.** Environmental investigations and restoration efforts are assumed not to be carried out in accordance with the Consent Order provisions. The LANL environmental restoration project would continue at pre-Consent Order levels, but no extensive corrective measures would be conducted for major PRSs.
- **Capping Option.** The Consent Order would be implemented. For this appendix it was assumed that MDAs would be stabilized in place by placing final covers over them and conducting certain other environmental restoration activities such as remediating volatile organic compound plumes in soil at some MDAs. The underground “General’s Tanks” (see Section I.2.5.2.1) within MDA A would be grouted in place. Transuranic waste in subsurface storage at MDA G would be removed, processed, and shipped to the Waste Isolation Pilot Plant (WIPP). Because some of the stored, transuranic waste in subsurface shafts within MDA G may be difficult to retrieve, an option to leave this stored waste in place would be considered. If this option were pursued, a performance assessment pursuant to Title 40 of the *Code of Federal Regulations* (CFR) Part 191, may be required. If such an assessment is required, the assessment results may indicate the need for additional waste stabilization or MDA cover final design modification.

The No Action Option is considered in this appendix because such an action is required by NEPA. DOE is legally required to carry out the provisions of the Consent Order.

In addition, numerous other PRSs would be remediated by methods such as contamination removal, surge bed grouting, contaminated sediment natural flushing, permeable reactive barriers, pump and treat system installation, or other measures.

- **Removal Option.** The Consent Order would be implemented. For this appendix it was assumed that LANL MDA waste and contamination would be removed. Transuranic waste stored belowground at MDA G would be removed and shipped to WIPP along with other transuranic-contaminated material disposed of before 1970. Remediation of other PRSs would again occur by various methods as discussed for the Capping Option.

Environmental impacts assessed under the three options should bound those that could result from eventual implementation of MDA and PRS corrective measures. Remediation decisions will be made for specific MDAs and PRSs rather than groups and may prescribe a combination of corrective measures. For example, some waste within an MDA may be removed and the remainder may be stabilized in place.

For all options, appropriate safety and environmental surveillance and maintenance would continue at LANL to maintain compliance with DOE and external criteria and standards, including those for nuclear environmental sites (Section I.3.2.3).

I.1.4 Related National Environmental Policy Act Analyses

Two NEPA analyses related to this appendix are:

- *Environmental Assessment for Proposed Corrective Measures at Material Disposal Area H within Technical Area 54 at Los Alamos National Laboratory, Los Alamos, New Mexico* (DOE 2004b)
- *Categorical Exclusion for Proposed Remediation of MDA V within Technical Area 21 (TA-21)* (LANL 2004j)

I.2 Background

Introducing this chapter are sections summarizing (1) LANL’s general setting, and (2) LANL’s environmental restoration project and the March 1, 2005, Consent Order. The remaining sections address each PRS cited in the Consent Order consistent with their grouping in the Consent Order.

I.2.1 General Setting

LANL and its TAs are shown in **Figure I–1**. LANL is bordered by the Santa Fe National Forest to the north, west, and south. The Rio Grande and the Native American Pueblo of San Ildefonso border LANL on the east; the Bandelier National Monument and Bandelier Wilderness Area lie directly south. The areas surrounding LANL, Los Alamos County, and much of the neighboring counties are undeveloped. The two closest communities are the Los Alamos townsite and White Rock. Population centers within 50 miles (80 kilometers) of LANL include Española and Santa Fe. Thirteen American Indian Pueblos are within 50 miles (80 kilometers). LANL is on the Pajarito Plateau, consisting of east-southeast-trending canyons and mesas. The plateau mesas are generally devoid of surface water. Canyons may be wet or dry. Wet canyons contain continuous streams and may contain groundwater in canyon bottom alluvium. Dry canyons contain streams only occasionally flowing with water, and lack alluvial groundwater (LANL 1999b). The LANL region contains numerous natural and cultural resources, including habitats of threatened and endangered species such as the Mexican spotted owl (*Strix occidentalis lucida*), bald eagle (*Haliaeetus leucocephalus*), and southwestern willow flycatcher (*Empidonax treillii extimus*) (see Chapter 4, Table 4–22, of this SWEIS).

I.2.2 The Los Alamos National Laboratory Environmental Restoration Project

Some of the hazardous and radioactive materials used at LANL have been released into the environment or disposed of as waste. Public and environmental protection has been maintained through a combination of site natural features; technology implementation; administrative and institutional controls; health, safety, and environmental monitoring; and adherence to applicable standards. Nonetheless, concerns about future efficacy of disposal and discharge areas to retain contaminants within regulatory standards have prompted efforts to remediate LANL areas where hazardous constituent releases may have occurred (LANL 2000b).

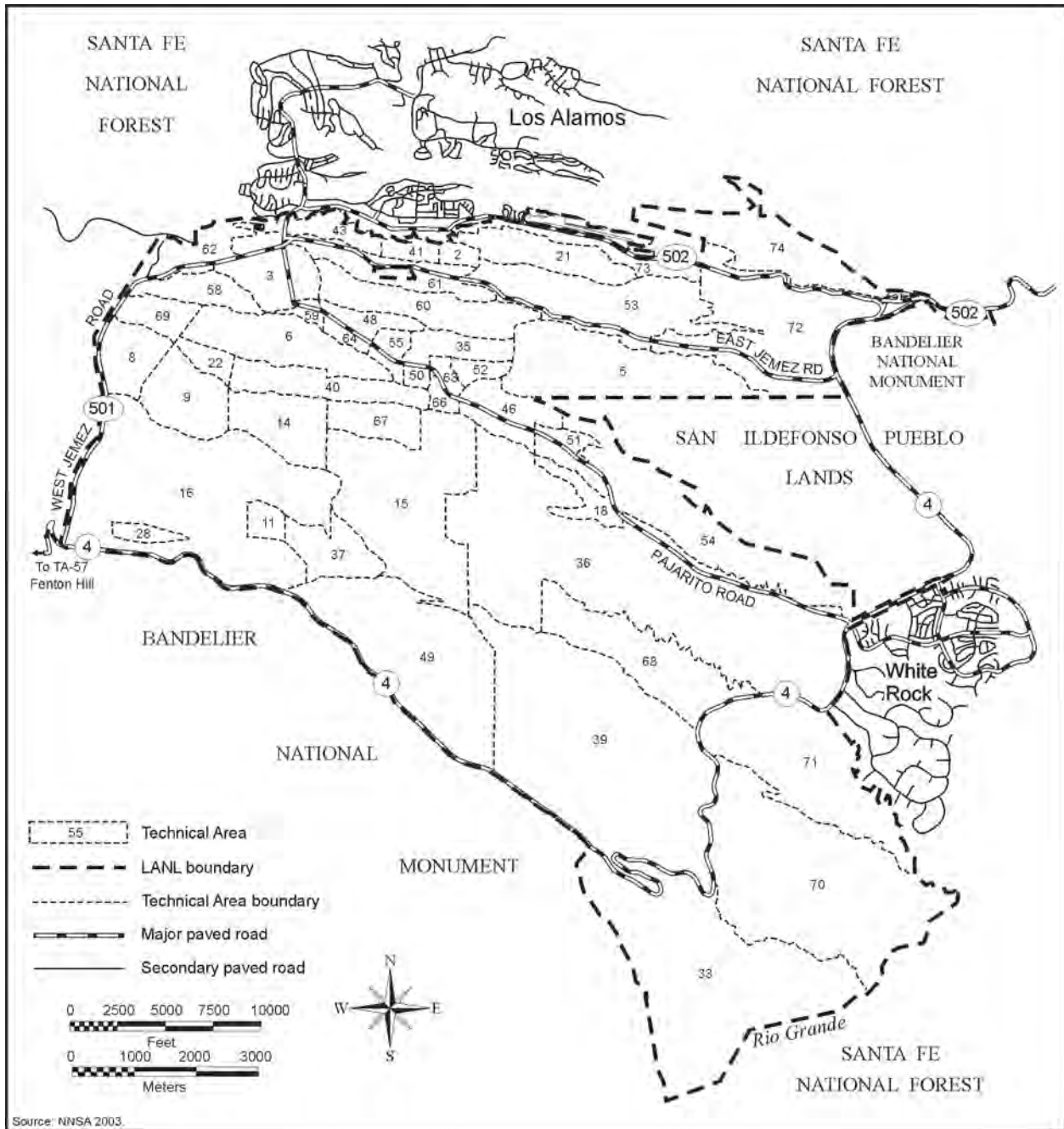


Figure I-1 Los Alamos National Laboratory Technical Area Locations

I.2.2.1 The Los Alamos National Laboratory Environmental Restoration Project Background

DOE and LANL employees must conduct activities in compliance with regulatory requirements derived from Federal and state statutes and Executive orders. Laws, regulations, agreements, and environmental protection orders applicable to LANL are presented in Chapter 6 of this SWEIS.

Operations involving radioactive materials have been historically conducted by DOE and its predecessors under Atomic Energy Act authority. However, during the last several decades, the

Congress enacted several major statutes addressing environmental protection, including RCRA, HSWA, and the Federal Facility Compliance Act. LANL currently operates under the regulatory authority of DOE, the U.S. Environmental Protection Agency (EPA), and the State of New Mexico. Under the Atomic Energy Act, DOE continues to have general landlord authority for protecting the public and environment, as well as specific authority for protecting workers, the public, and the environment from deleterious effects of radioactive and other toxic or hazardous materials. EPA has overall Federal regulatory authority for management of hazardous materials defined under RCRA and its amendments, particularly HSWA, as well as corrective actions taken pursuant to these statutes. EPA has authorized the State of New Mexico to implement this regulatory authority.

In 1989, DOE created the Office of Environmental Restoration and Waste Management; LANL's environmental restoration project was established the same year to undertake environmental restoration and decommissioning activities (LANL 2000b). In November 1989, the New Mexico Environmental Improvement Division (now NMED) issued LANL's Hazardous Waste Facility Permit. In March 1990, EPA issued Module VIII to the permit, setting forth procedural requirements for HSWA corrective actions and specifying development of an installation work plan. LANL's environmental restoration project identified 2,124 PRSs, consisting of 1,099 PRSs that EPA listed in the Hazardous Waste Facility Permit and 1,025 PRSs not listed in the permit. Through 1995, EPA had sole authority over HSWA corrective actions at LANL. In January 1996, EPA delegated this authority to NMED (LANL 2000b).

LANL staff grouped the PRSs into 24 operable units (LANL 2000b) and, in the early to mid-1990s, issued RCRA facility investigation (RFI) Work Plans describing the history of activities within each operable unit, potential contaminants and release pathways, and site investigation plans. Site investigations included: installation of borings and wells; sampling of surface soils, vegetation, drainage channel sediments; and subsurface material, including soil vapor; monitoring of surface water and groundwater; and measurement of external radiation and airborne contaminants. The investigations sampled and monitored for radionuclides and nonradiological contaminants, including polychlorinated biphenyls (PCBs), explosives, and organic and inorganic constituents (LANL 2000b).

In December 1997, LANL staff and NMED began to consolidate corrective action sites that were related by contaminant source, geographic location, and potential cumulative risk. In 1999, LANL staff began to use watersheds to identify discrete systems within which multiple, consolidated sites would be investigated, assessed, and remediated (LANL 2000b).

Phase I RFIs have been completed for most of the MDAs and many other PRSs. Additional investigations are ongoing. Since 1993, over 100 voluntary cleanup actions have been conducted (LANL 2002g). Through the end of 2005, 774 units had been approved for no further action, including 146 that had been removed from LANL's Hazardous Waste Facility Permit. Of these, 125 non-HSWA Module sites had previously been approved for no further action by DOE and, under the terms of the Consent Order, the no further action determinations will be re-evaluated by NMED. Based on prior no further action approvals and consolidation of geographically proximate sites, 829 sites remain within LANL's environmental restoration project (LANL 2006h).

I.2.2.2 Consent Order

On May 2, 2002, NMED issued a Determination of Imminent and Substantial Endangerment to Health and the Environment and a draft order compelling investigation and cleanup of environmental contamination. After receiving public comments, NMED revised its Determination and issued a final Compliance Order on November 26, 2002. On behalf of DOE, the U.S. Department of Justice filed a lawsuit challenging the final order. The University of California filed a separate lawsuit. NMED, DOE, the Justice Department, and the University of California entered settlement negotiations that led to a Consent Order to replace the November 2002 Compliance Order.

NMED issued a revised Consent Order for public comment on September 1, 2004. The comment period closed on October 1, 2004. NMED delayed issuance of the final Consent Order until surface water and watershed issues were addressed in a separate Federal Facility Compliance Agreement under the Clean Water Act. The agreement was signed on February 3, 2005. On March 1, 2005, the final Consent Order was entered into by NMED, the State of New Mexico Attorney General, DOE, and the University of California (NMED 2005).

The Consent Order requires LANL-wide investigation and cleanup pursuant to stipulated procedures and schedules (NMED 2004). (Schedules in the Consent Order may be adjusted to account for delays in NMED approvals; or to accommodate requests from DOE or its authorized contractor for time extensions.) Most PRSs contain constituents that are regulated under the Consent Order, as well as radionuclides that are regulated under the Atomic Energy Act. To avoid duplication of completed work, the Consent Order does not apply to those PRSs not listed in Module VIII that received No Further Action decisions from EPA when it had primary regulatory authority.

The Consent Order requires the installation of wells, piezometers, and other subsurface units to provide site characteristic or environmental information; the collection and investigation of sample data; and preparation and submittal of investigative reports for various PRSs. Following the investigation phase for a subject PRS, corrective measures are proposed, authorized, and implemented as needed. If NMED determines that a corrective measure evaluation is needed, a corrective measure evaluation report³ must be prepared that addresses alternative remedies. NMED will determine the remedy to be implemented, although DOE may propose a remedy. After completing the approved corrective measure, a remedy completion report must be prepared and sent to NMED for approval.

Investigations and PRSs addressed in the Consent Order are summarized in the following sections of this appendix:

- Section I.2.3: Firing Sites and Other PRSs within Testing Hazard Zones
- Section I.2.4: Canyons
- Section I.2.5: Technical Area Investigations

³ A corrective measure evaluation report essentially corresponds to a RCRA corrective measures study report.

- Section I.2.6: Other SWMUs and Areas of Concern (AOCs), Including Aggregate Areas
- Section I.2.7: Continuing Investigations

MDAs that are not specifically cited in the Consent Order but may be addressed as part of required aggregate area investigations are summarized in Section I.2.8.

I.2.3 Firing Sites and Other PRSs within Testing Hazard Zones

Consent Order Section IV.A.5 addresses firing sites and other PRSs within testing hazard zones. Consent Order Table IV-1 lists SWMUs and AOCs located within designated testing hazard zones. Investigations, and if appropriate, corrective actions must be performed for these SWMUs and AOCs. With some exceptions, investigation and corrective action may be deferred for any SWMU or AOC located within a testing hazard zone and identified in Consent Order Table IV-2. These SWMUs and AOCs need not be included in relevant aggregate area investigation work plans. The deferral may continue until the firing site used to delineate the relevant testing hazard zone is closed, or it is inactive and DOE determines that it is reasonably unlikely to be reactivated (NMED 2005). **Table I-5** lists the 107 nondeferred SWMUs and AOCs (Consent Order Table IV-1), and **Table I-6** lists the 45 deferred SWMUs and AOCs (Consent Order Table IV-2).

Each PRS listed in Table I-5 will be remediated in accordance with the schedule for the aggregate area containing the PRS (see Section I.2.6). Some PRSs listed in these tables may require a significant remediation effort. PRSs of particular interest for this appendix include two firing sites (Firing Sites E-F and R-44) and five MDAs (MDAs F, Z, AA, Y, and AB). Thumbnail descriptions of these PRSs are provided below.

I.2.3.1 Technical Area 15: Firing Site E-F

TA-15 (R Site) is in the center of LANL. Most of TA-15 is encompassed by Threemile Mesa, but Water Canyon transverses the southern site boundary and Potrillo Canyon intersects the main portion of Threemile Mesa, dividing the mesa into two areas (**Figure I-2**) (LANL 1993c).

TA-15 has been used since World War II for explosive testing of nuclear weapons components. Several early firing points are no longer used, and most of their structures have been decommissioned and dismantled (LANL 1993c). Firing Site G was in use by 1949, and is listed in the Consent Order as a deferred site (Table I-6). Areas R-40, R-183, and The Hollow contain office buildings. Firing Sites R-44 and R-45 were built in the 1950s (LANL 1993c). R-41 is a container storage area. The Pulsed High-Energy Radiographic Machine Emitting X-Rays (PHERMEX) facility was completed in the 1960s. A second radiographic machine, Ector, was installed in the early 1980s (LANL 1993c).⁴

⁴ A newer facility, the Dual-Axis Radiographic Hydrodynamic Test (DARHT) facility, is not shown on Figure I-2 but is located near PHERMEX.

Table I-5 Non-Deferred Sites Within Testing Hazard Zones

| <i>Site Identification</i> | <i>Description</i> | <i>Site Identification</i> | <i>Description</i> |
|----------------------------|--|----------------------------|--|
| 06-005 | Firing site pit | 15-009(e) | Septic system |
| 06-007(a) | MDA F | 15-009(g) | Septic system (active) |
| 06-007(b) | MDA F | 15-009(h) | Septic tank |
| 06-007(c) | MDA F | 15-009(i) | Septic tank |
| 06-007(d) | MDA F | 15-010(c) | Drain line |
| 06-007(e) | MDA F | 15-014(l) | Outfall (active) |
| 06-008 | Underground storage tank | C-15-001 | Surface disposal |
| 07-001(a) | Firing site | C-15-004 | Transformers |
| 07-007(b) | Firing site | C-15-011 | Former site of underground tank |
| 11-005(a) | Septic system | C-15-013 | Underground fuel tank |
| 11-005(b) | Septic system | 18-001(a) | Lagoon |
| 11-005(c) | Outfall | 27-002 | Firing sites |
| 11-006(a) | Sump | 27-003 | Bazooka impact area |
| 11-006(b) | Tank and/or associated equipment | 36-001 | MDA AA |
| 11-006(c) | Tank and/or associated equipment | 36-002 | Sump |
| 11-006(d) | Tank and/or associated equipment | 36-003(a) | Septic system |
| 11-011(a) | Industrial or sanitary wastewater treatment | 36-003(b) | Septic system |
| 11-011(b) | Industrial or sanitary wastewater treatment | 36-004(c) | Firing site – open detonation (active) |
| 11-011(d) | Industrial or sanitary wastewater treatment | 36-005 | Surface disposal site |
| C-11-002 | Footprint of former laboratory | 36-006 | Surface disposal site |
| C-12-001 | Footprint of former building | 36-008 | Surface disposal site |
| C-12-002 | Footprint of former building | C-36-003 | Storm drainages |
| C-12-003 | Footprint of former building | 37-001 | Septic system |
| C-12-004 | Footprint of former building | 39-001(b) | MDA Y |
| 14-001(g) | Firing site – Open burn/open detonation (active) | 39-002(b) | Storage area |
| 14-002(c) | Building | 39-002(c) | Storage area |
| 14-002(f) | Footprint of former junction box shelter | 39-002(d) | Storage area |
| 14-003 | Open burning ground | 39-002(f) | Storage area |
| 14-005 | Open burn site (active) | 39-004(c) | Firing Site 39-6 (active) – open detonation RCRA unit |
| 14-006 | Tank and/or associated equipment | 39-004(d) | Firing Site 39-57 (active) – open detonation RCRA unit |
| 14-007 | Septic system | 39-007(a) | Storage area |
| 14-009 | Surface disposal site | 39-007(d) | Storage area |
| 14-010 | Sump | 39-008 | Former building footprint (soil contamination) |
| C-14-001 | Footprint of former building | 39-010 | Excavated soil dump |
| C-14-003 | Footprint of former building | 40-001(b) | Septic system |
| C-14-004 | Footprint of former building | 40-001(c) | Septic system |
| C-14-005 | Footprint of former building | 40-003(a) | Scrap burn site/open detonation (completed RCRA closure) |
| C-14-006 | Footprint of former building | 40-003(b) | Burning area (completed RCRA closure) |
| C-14-007 | Footprint of former building | 40-004 | Operational release |
| C-14-008 | Footprint of former building | 40-005 | Sump |
| C-14-009 | Footprint of former building | 40-009 | Landfill |
| 15-001 | Surface disposal | 40-010 | Surface disposal site |
| 15-004(f) | Firing Site E-F | 49-001(a) | MDA AB |
| 15-004(h) | Firing Site H | 49-001(b) | MDA AB |
| 15-005(c) | Container storage area (R-41) | 49-001(c) | MDA AB |

| <i>Site Identification</i> | <i>Description</i> | <i>Site Identification</i> | <i>Description</i> |
|----------------------------|------------------------------|----------------------------|--------------------------------------|
| 15-007(b) | MDA Z | 49-001(d) | MDA AB |
| 15-007(c) | Firing site shaft | 49-001(e) | MDA AB |
| 15-007(d) | Firing site shaft | 49-001(g) | MDA AB |
| 15-008(a) | Surface disposal at E-F site | 49-002 | Underground chamber |
| 15-008(b) | Surface disposal | 49-003 | Leach field and small-shot area |
| 15-008(c) | Surface disposal | 49-005(a) | Landfill |
| 15-008(g) | Surface disposal | 49-006 | Sump |
| 15-009(b) | Septic system | 49-008(d) | Firing sites and underground chamber |
| 15-009(c) | Septic tank | | |

MDA = material disposal area, RCRA = Resource Conservation and Recovery Act.
Source: NMED 2005.

Table I-6 Deferred Sites in Testing Hazard Zones

| <i>Site Identification</i> | <i>Description</i> | <i>Site Identification</i> | <i>Description</i> |
|----------------------------|--------------------------------|----------------------------|-----------------------------|
| 06-003(a) | Firing site | 14-002(b) | Firing site |
| 06-003(h) | Firing site | 15-003 | Firing site |
| C-06-019 | Footprint of former structure | 15-004(a) | Firing site |
| 07-001(c) | Firing site | 15-004(g) | Firing site |
| 07-001(d) | Firing site | 15-006(a) | Firing site |
| 11-001(a) | Firing site | 15-006(b) | Firing site |
| 11-001(b) | Firing site | 15-006(c) | Firing site |
| 11-002 | Burn site | 15-006(d) | Firing site |
| 11-003(b) | Air gun | 15-008(f) | Firing site |
| 11-004(a) | Firing site | 36-004(a) | Firing site |
| 11-004(b) | Firing site | 36-004(b) | Firing site |
| 11-004(c) | Firing site | 36-004(d) | Firing site |
| 11-004(d) | Firing site | 36-004(e) | Firing site |
| 11-004(e) | Firing site | 39-004(a) | Firing site |
| 11-004(f) | Firing site | 39-004(b) | Firing site |
| 11-009 | MDA S | 39-004(e) | Firing site |
| 11-012(c) | Footprint of former building | 40-006(a) | Firing site |
| 11-012(d) | Footprint of former laboratory | 40-006(b) | Firing site |
| C-11-001 | Footprint of former laboratory | 40-006(c) | Firing site |
| 14-001(f) | Firing site | 49-008(a) | Soil contamination |
| 14-002(a) | Firing site | 49-008(b) | Soil contamination (Area 6) |
| 14-002(d) | Firing site | 49-008(c) | Soil contamination |
| 14-002(e) | Firing site | | |

MDA = material disposal area.
Source: NMED 2005.

The E-F Site (Consolidated Unit 15-004(f)-99) is north of Potrillo Canyon and southeast of Ector. It includes the firing site (SWMU 15-004(f)), a surface disposal area (SWMU 15-008(a)), a septic system (SWMU 15-009(e)), and the site of a removed transformer station (C-15-004) (LANL 1993c). The septic system has been recommended for no further action (LANL 2005c).

History of Firing Site E-F. Firing Site E-F was created in 1947, possibly from an earlier firing point. Firing Site E is larger and about 800 feet (244 meters) from Firing Site F. Firing Sites E and F were both connected to an underground, timbered, control room (Building TA-15-27, or R-27) 600 feet (183 meters) to the southwest of Firing Site E (LANL 1993c). The sites were used extensively through 1973 and were last used in 1981. Firing Sites E and F were once merely surface depressions. As testing progressed, soil was either regraded to the previous depression level or new gravel was imported to fill holes. Eventually, soil was mounded to the north and south to protect buildings from shrapnel. No major effort was made to remove the scattered materials, although, after each explosion, test debris and obvious pieces of uranium metal were recovered. Between 1945 and 1957, 95,000 pounds (43,000 kilograms) of natural uranium metal was expended. After 1957, 44,000 pounds (20,000 kilograms) of depleted uranium was expended (LANL 1993c).

Two small surface-disposal areas (SWMU 12-008), 200 feet (61 meters) apart, are south of Firing Site E-F. The areas contain mounded rubble (LANL 1993c).

Waste Inventory. Up to 139,000 pounds (63,000 kilograms) of natural and depleted uranium may have been expended. Shrapnel or other pieces of uranium may have scattered up to 3,500 feet (1,070 meters) from the firing site, although most debris deposited within 1,000 feet (305 meters). Much of the uranium has oxidized. About 705 pounds (320 kilograms) of beryllium metal was scattered, and much of this metal has oxidized. Other toxic metals include lead (about 220 pounds [100 kilograms]), mercury (less than 220 pounds [100 kilograms]), bismuth, copper, cobalt, nickel, tin, and thorium. Little high explosive (HE) probably survived the tests (LANL 1993c).

The two disposal areas south of Firing Site E-F include metal pieces, soil, plastic, rock, pebbles, electrical cable, electrical accessories, and miscellaneous debris. Potential contaminants include uranium, beryllium, lead, and mercury (LANL 2005c).

Site Investigations. Studies since the late 1970s have shown extensive uranium contamination, varying from concentrations exceeding 4,500 milligrams per kilogram at the firing point to less than 200 milligrams per kilogram 980 feet (300 meters) away. Soil samples collected in 1980 showed an order of magnitude decrease in uranium concentrations within the top 10 to 12 inches (25 to 30 centimeters) of soil, although the trend was not uniform (LANL 1993c). In 1994, numerous surface and subsurface samples were collected as part of a Phase I RFI. Contaminants included uranium, protactinium-234m, thorium-234, americium-241, cesium-137, barium, beryllium, cadmium, chromium, copper, lead, manganese, mercury, nickel, silver, vanadium, and zinc. Similar radionuclides and inorganic chemicals were found at the surface disposal site (LANL 2005c).

Current Configuration. Firing Site E-F is wooded. Scattered debris includes chunks of oxidized metal. The two piles of debris in the surface disposal area are each 8 feet (2.4 meters) in diameter and 2 feet (0.6 meters) high (LANL 2005c).

I.2.3.2 Firing Site R-44

Firing Site R-44 (Consolidated Unit 15-006(c)-99) is near Firing Site E-F (Figure I-2) (LANL 1993c, 2001f) and includes the firing site itself (SWMU 15-006(c)), the septic system associated with the R-44 site (SWMU 15-009(c)), and a surface disposal area (SWMU 15-008(b)). The firing site itself is listed as a deferred site (Table I-6).

History of Firing Site R-44. Named after the site control room, R-44 was built in 1951 and used from 1956 through 1978 for tests of weapons components. But since PHERMEX and Ector were put into operation, the site was used less and for small experiments. R-44 was last used in September 1992. From 1953 to 1978, 15,000 pounds (7,000 kilograms) of uranium (mostly depleted uranium), 770 pounds (350 kilograms) of beryllium, and 33 pounds (15 kilograms) of lead were expended. Debris scattered into the canyons on either side of the firing site. The surface disposal area comprises two small areas at the edge of Threemile Canyon containing pieces of metal and plastic, soil, rocks and pebbles, electrical cable, other electrical accessories, and other debris (LANL 1993c).

Waste Inventory. An aerial radiological survey suggested that in 1982, the amount of uranium in the soil at R-44 was about four percent of that at Firing Site E-F, or about 5,070 pounds (2,300 kilograms) (LANL 1993c). A 1991 land-based radiological survey found pieces of uranium near the firing site. The area was partially remediated. In 1987, samples were collected at four radial distances (10, 100, 250, and 450 feet [3, 30, 76, and 137 meters]) from the center of the firing site. High explosives were not detected. Concentrations of lead, beryllium, and uranium-238 at 450 feet (137 meters) were all more than a magnitude smaller than those in the center. Average soil background levels were 28.4 milligrams per kilogram for lead, 2.4 milligrams per kilogram for beryllium, and 3.4 milligrams per kilogram for uranium (LANL 1993c).

The 1993 RFI Work Plan for Operable Unit 1086 estimated that the volume of piled debris in the surface disposal area amounted to a few dump truck loads. At least 80 percent was contaminated with uranium, beryllium, and lead (LANL 1993c).

Site Investigations. The Phase I RFI for the firing site (June 1995 through March 1996) found uranium, beryllium, lead, arsenic, and hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX). The Phase I RFI for the surface disposal area found uranium and inorganic chemicals, including antimony, arsenic, beryllium, chromium, copper, lead, mercury, nickel, silver, and zinc (LANL 2005c).

Current Configuration. The Cerro Grande Fire damaged the firing site, which is wooded with ponderosa pine. Debris was exposed throughout the site, mainly toward the east. Within a year, straw wattles, rock check dams, and silt fencing were installed and the area was hydromulched. Sediment migration was minimal. A year after the fire, the site had a vegetative cover greater than 70 percent (LANL 2001f). Much of the exposed debris was recovered and disposed of.

I.2.3.3 Technical Area 6: Material Disposal Area F

TA-6 (Twomile Mesa Site) is on Twomile Mesa, which is bordered to the north by Twomile Canyon and to the south by Pajarito Canyon. During the Manhattan Project, TA-6 was used to test explosive detonators for the Fat Man weapon; to purify the explosive pentaerythritol tetranitrate (PETN), used to achieve implosion; and to destroy shaped explosive charges called lenses. After the war, MDA F was created to dispose of classified objects. Test firing continued at TA-6 until 1952. Explosives development, laser, chemical laboratory, and photographic operations continued through February 1976, and several small operations continued until the 1980s (LANL 1993g).

History of MDA F. MDA F is a small site to the north of Twomile Mesa Road. MDA F is at an elevation of 7,460 feet (2,274 meters). Runoff flows north to the southwest fork of Twomile Canyon, which is part of the Pajarito Canyon Watershed (LANL 1999b).

A May 15, 1946, memorandum from the Director of Los Alamos Scientific Laboratory, N. E. Bradbury, announced preparation of a pit for disposal of classified objects and shapes. The memorandum stated that the pit was located at TD Site, but a penciled correction indicated Twomile Mesa (Rogers 1977). A second pit was dug in 1947 in accordance with a July 16, 1947, memorandum from Bradbury. The locations of these two pits were not recorded on contemporary documents (LANL 1993g).

From 1949 through 1951, work orders were written for three smaller pits on Twomile Mesa (LANL 1993g):

- 1949 – A pit 40 by 20 by 10 feet deep (12 by 6.1 by 3.0 meters)
- 1950 – A pit 6 by 6 x 6 feet deep (1.8 by 1.8 by 1.8 meters)
- 1951 – A pit 2 by 2 by 4 feet deep (0.6 by 0.6 by 1.2 meters)

The locations of these pits are unknown, as are their as-built dimensions and contents.

From 1950 to 1952, three shafts may have been drilled to dispose of spark gaps containing cesium-137. None of the shafts correlates with archived job and work orders (LANL 1993g). Aerial photographs from 1954 show two large disturbed areas that may be the two pits referenced in the Bradbury memoranda (LANL 1993g). The two chain-link fences at MDA F were erected in 1981. The smaller fenced area basically corresponds to the disturbed areas on aerial photographs, but the larger fenced area is mostly north of the larger pits.

Waste Inventory. The inventory is poorly known. MDA F was used for disposal of classified items. Spark gaps containing cesium-137 were probably buried. In 1964, the total estimated amount of cesium-137 was 30 microcuries. Other hazardous materials may have been placed in the pits (LANL 1993g).

The pits may contain explosives. This concern was prompted by a statement from a person responsible for digging the 1946 pit that “large blocks of HE, Primacord, etc.” were placed in the pit (LANL 1993g). Yet later this individual stated that no hazardous materials were buried, and

that burial was not the accepted practice for disposal of explosives (LANL 1993g). The RFI Work Plan for Operable Unit 1111 found no primary sources stating that explosives were buried. All reports of squibs, detonators, depleted uranium, and strontium-90 buried in pits at MDA F were from secondary sources (LANL 1993g).

Current Configuration. MDA F comprises a small area encompassed by, and in the vicinity of, a pair of fenced areas (**Figure I-3**). Southeast of MDA F are depressions that may have resulted from explosive destruction of defective lenses for the Fat Man weapon in 1945 (LANL 1993g, 1999b). Some of these lenses contained Baratol, which contains barium nitrate and 2,4,6-trinitrotoluene (TNT) (LANL 1999b). West of MDA F is the “timbered pit” that may have been used for test firing Jumbino vessels.⁵ A 1944 progress report contains a photograph of a Jumbino in a pit, and a 1986 geophysical survey located an anomaly in this area (LANL 1993g). Aerial photography and satellite imagery in 2000 suggested two long, narrow trenches and six small pits in the vicinity of the two fenced areas (Pope et al. 2000). One pit may be the timbered pit.

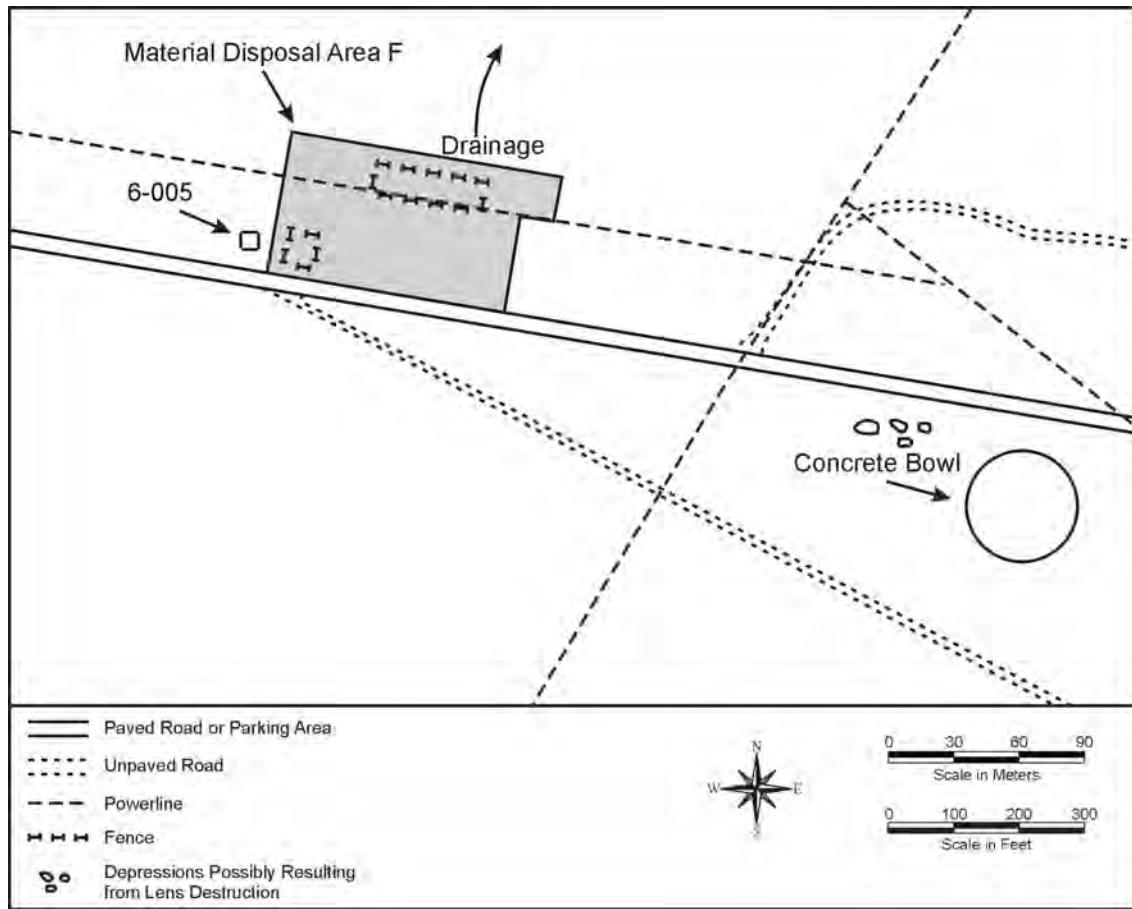


Figure I-3 Material Disposal Area F

⁵ A Jumbino is a stainless steel vessel used to test methods for containment and recovery of fissionable materials such as plutonium from explosives implosion tests. Recovery was needed because of the very limited supply of the fissionable materials. From 1944 tests involving Jumbino vessels, Los Alamos scientists constructed a much larger vessel called Jumbo for containment of the Trinity Test. Jumbo was never used for this purpose because by 1945 plutonium availability was much greater (LANL 1993b).

The site was contoured and reseeded with native grasses in 1996. The MDA vicinity is dotted with scrub oak (Pope et al. 2000). A power line crosses the site in an east-west direction.

Waste management units are:

- SWMU 6-005 – the timbered pit to the west of the smaller fenced area
- SWMU 6-007(a) – the pair of fenced areas
- SWMU 6-007(b) – the pit from the 1940s photographs
- SWMUs 6-007(c and d) – the two pits described by the 1946 and 1947 Bradbury memoranda
- SWMU 6-007(e) – additional pits that may exist at MDA F

Site Investigations. The areas inside the fences have been monitored for radioactivity since 1981. No readings above background have been observed (LANL 1999b). According to the 1993 RFI Work Plan for Operable Unit 1111 (LANL 1993g), vegetation at MDA F was sampled in 1981 and 1983 for radioactive contaminants; none were found. In 1986, a site survey was performed using ground-penetrating radar and magnetometry. Survey data were difficult to interpret. The Phase I RFI for MDA F was to determine: (1) pit boundaries, (2) whether contaminants of concern were present in media surrounding the pits, and (3) whether barium and TNT were in surface soils south and east of MDA F (LANL 1993g). Aerial photography and satellite imagery were conducted in 2000 to help locate the disposal unit positions.

I.2.3.4 Technical Area 15: Material Disposal Area Z

MDA Z (SWMU 15-007(b)) is south of the side road leading to Building TA-15-233 near Firing Site G. MDA Z is teardrop-shaped and measures 200 feet (60 meters) by 50 feet (15 meters) at its widest. The MDA was used between 1965 and 1981 for disposal of construction debris. The waste was placed in a natural depression. (Concrete-filled sandbags at the site were probably piled as a retaining wall.) One face of the MDA grades to native soil; the other face is exposed, standing 15 feet (4.6 meters) high. The debris on the exposed face was probably bulldozed from PHERMEX and includes metals from wire and blast mats, volatile organic compounds or semi-volatile organic compounds from charred wood, road and construction debris, and radioactive substances (LANL 1993c, 1999b). One reference states that chunks of uranium are visible (LANL 1999b), although a 1982 aerial radiological survey detected no radioactive contamination above background values (LANL 1993c).

A Phase I RFI conducted from June 1995 to March 1996 collected surface and subsurface samples. Inorganic chemicals found above background values were beryllium, copper, lead, mercury, and silver. Uranium was found with a maximum concentration of 349 milligrams per kilogram. Twelve organic chemicals were found. The RFI report recommended material removal following a baseline ecological risk assessment (LANL 2005c).

I.2.3.5 Technical Area 36: Material Disposal Area AA

Located in the southeastern portion of LANL, TA-36 (Kappa Site) has four active firing sites.

MDA AA (SWMU 36-001) is within Potrillo Canyon. MDA AA is near the active Lower Slobbovia firing range (SWMU 36-004(d)) and consists of two to four disposal trenches used to burn and dispose of debris and sand from firing sites. The trenches likely contain wood, nails, and sand contaminated with barium, uranium, other inorganic chemicals, plastics, and possibly high explosive. When a trench became filled with waste, it was covered with 4 feet (1.2 meters) of soil. The first trench was dug in the mid-1960s, and the site was closed in 1989 in accordance with New Mexico solid waste regulations.⁶ The MDA AA trench area was graded to lessen the potential for stormwater runoff. Samples taken from the last active trench in 1987 and 1988 showed elevated levels of cadmium and uranium (LANL 1993a, 1999b, 2005c).

A Phase I RFI was conducted from 1993 through 1995. Two trenches were identified: the northern trench is 80 by 40 by 8 to 13 feet deep (24 by 12 by 2.4 to 4.0 meters deep); the southern trench is 120 by 20 to 30 by 3 to 12 feet deep (37 by 6.1 to 9.1 by 0.9 to 3.7 meters deep). Boreholes into the trenches were sampled for inorganic and organic chemicals and radionuclides. The RFI report recommended no further action. NMED disagreed. A Phase II sampling and analysis program was planned. In 1996, an interim action stabilized erosion gullies using wire mesh and cobbles (LANL 2005c).

I.2.3.6 Technical Area 39: Material Disposal Area Y

TA-39 (Ancho Canyon Site) is at the bottom of Ancho Canyon between Los Alamos and White Rock. MDA Y (SWMU 39-001(b)) is part of Consolidated Unit 39-001(b)-00 consisting of SWMUs 39-008 and 39-001(b) (LANL 1999b, 2005c).

SWMU 39-008 is a former firing range. Testing began in 1960, continued until 1975, was suspended for 13 years, and resumed in 1988. Building 39-137 housed a gun using gas to fire projectiles at targets on a cliff face. Most debris from this and other gas gun experiments lies in an area west of the building, but projectiles and target fragments occasionally hit the cliff face 200 feet (61 meters) west of Building 39-56. The area between the buildings and the cliff was leveled and surface materials pushed into a mound. A 1977 RFI report, later withdrawn, recommended deferring action on SWMU 39-008 because it was still active. However, SWMU 39-008 is a nondeferred site in the Consent Order, where it is described as soil contamination associated with a former building footprint (see Table I-5) (LANL 2005c).

SWMU 39-001(b) (MDA Y) consists of three pits that, beginning in the late 1960s, received debris from the firing range (SWMU 39-008), empty chemical containers, and office waste (LANL 1999b, 2005c). The RFI Work Plan for Operable Unit 1132 indicates that the first pit measured 148 by 20 by 12 feet deep (45 by 6.1 by 3.7 meters deep); the second pit next to and west of the first pit had the same dimensions, and the third pit was south of the other pits (LANL 1993b). Figure 5-3 of this reference suggests that the first two pits were 40 feet (12 meters) apart. The third pit is depicted as being about twice as long as the first two pits but

⁶ A permitted burn area west of MDA AA is still used to burn combustible firing site debris (LANL 1999a).

about as wide. Pit 1 may have been surveyed and dug in 1973; Pit 2 was in use from about 1976 to 1981; and Pit 3 from 1981 to 1989 (LANL 1993b).

The most probable locations of the pits were estimated from geophysical surveys, historical information, and radiation surveys. In 1994, two separate field activities investigated whether waste constituents had migrated from the pits. The 1994 field activities guided RFI sampling conducted in 1996. Test pits were trenched to below 12 feet (3.7 meters), the approximate depth of waste burial. The 1994 and 1996 field activity results were summarized in an RFI report that was later withdrawn (LANL 2005c).

I.2.3.7 Technical Area 49: Material Disposal Area AB

PRSs associated with MDA AB are addressed in Section I.2.5.3.

I.2.4 Canyons

The Consent Order requires investigations within canyon watersheds in accordance with approved work plans.⁷ The Consent Order requires construction of new wells, abandonment of some existing wells, and environmental sampling. Newly constructed wells must include alluvial, intermediate, and regional aquifer wells in the following watersheds (NMED 2005):

- Los Alamos/Pueblo Canyons Watershed
- Mortandad Canyon Watershed
- Water Canyon/Cañon de Valle Watershed
- Pajarito Canyon Watershed
- Sandia Canyon Watershed
- Other canyons (Ancho, Chaquehui, Indio, Potrillo, Fence, and North Canyons [Bayo, Guaje, Barrancas, and Rendija])

These wells would supplement existing wells. The numbers and locations of the wells, however, will be defined in approved work plans and may be different from numbers and locations identified in the Consent Order.

Canyon investigations implemented in 2005 focused primarily on Mortandad Canyon, and involved the characterization of sediment, biota, and groundwater to determine the nature and extent of contamination in media and to collect sufficient data to perform human and ecological risk assessments. Additional investigations in Pajarito Canyon were focused on sediment characterization to evaluate the nature and extent of contamination and the distribution of contaminant inventory (LANL 2006h).

⁷ At the time of Consent Order issuance, some canyon work plans had already been submitted to NMED while others were still under development.

The canyon investigation results may lead, as approved by NMED, to corrective measure programs. The scope of any remediation program for any watershed cannot be fully defined at this time. However, potential remediation alternatives could range from no action to more significant activities such as installation of additional shallow and deep groundwater monitoring wells, vadose zone monitoring systems, in situ bioremediation, permeable reactive barriers, or groundwater pump-and-treat systems. The more complex and involved remedies might require staging areas and moderate augmentation of infrastructure (such as plumbing for extracted water or other wastes) to support remedy operational aspects.

I.2.5 Technical Area Investigations

Requirements for TAs are typically prescribed for individual MDAs. (An exception is the investigative program prescribed for the Bayo Canyon Site, which consists of several PRSs but no MDAs.) Investigations for each MDA must be conducted in accordance with approved work plans and may include disposal unit surveys, drilling explorations, soil and rock sampling, sediment sampling, vapor monitoring and sampling (if present or discovered), intermediate and regional aquifer groundwater well installation, and groundwater monitoring.

I.2.5.1 Technical Area 10: Bayo Canyon Site

The Bayo Canyon Site (former TA-10) is in Bayo Canyon next to the western boundary of TA-74 and 4 miles (6.4 kilometers) west of the intersection of Bayo and Los Alamos Canyons. From 1943 to 1961, tests were conducted for nuclear weapons development. The Radiochemistry Laboratory, Building TA-10-1, prepared radiation sources for blast diagnostics. Explosives dispersed aerosols and debris containing uranium, lanthanum, and strontium-90. Liquid wastes were discharged to Bayo Canyon (NMED 2005). Bayo Canyon PRSs were investigated in accordance with the RFI Work Plan for Operable Unit 1079 (LANL 1992d). They include: (1) Consolidated Unit 10-001(a)-99; (2) Consolidated Unit 10-002(a)-99; (3) SWMU 10-004(a); (4) SWMU 10-006; and (5) AOC 10-009. The Consent Order requires additional investigations in accordance with the Bayo Canyon Aggregate Area Investigation Work Plan (NMED 2005). The work plan was submitted to NMED by the July 30, 2005, deadline, as was the required Historical Investigation Report for Bayo Canyon (LANL 2005m).

I.2.5.2 Technical Area 21: Material Disposal Areas A, B, T, and U

TA-21 (DP Site) is on DP Mesa east-southeast of the Los Alamos township. From 1945 to 1978, TA-21 was used for chemical research and for plutonium and uranium metal production (LANL 1999b, 2002a). DP West was used for radioactive-materials processing. Operations ceased in the 1980s, although process buildings remained until decommissioning began in the 1990s. DP East includes the Tritium Science and Fabrication Facility and the Tritium Systems Test Assembly (DOE 1999a). Operations will be relocated and structures decommissioned as addressed in Appendix H, Section H.2, of this SWEIS.

MDAs A, B, T, U, and V within TA-21 are shown in **Figure I-4** (LANL 2005b). The complex of structures to the east of MDA A is DP East, while the complex of structures to the west of MDA A is DP West. MDA V within TA-21 has been removed.

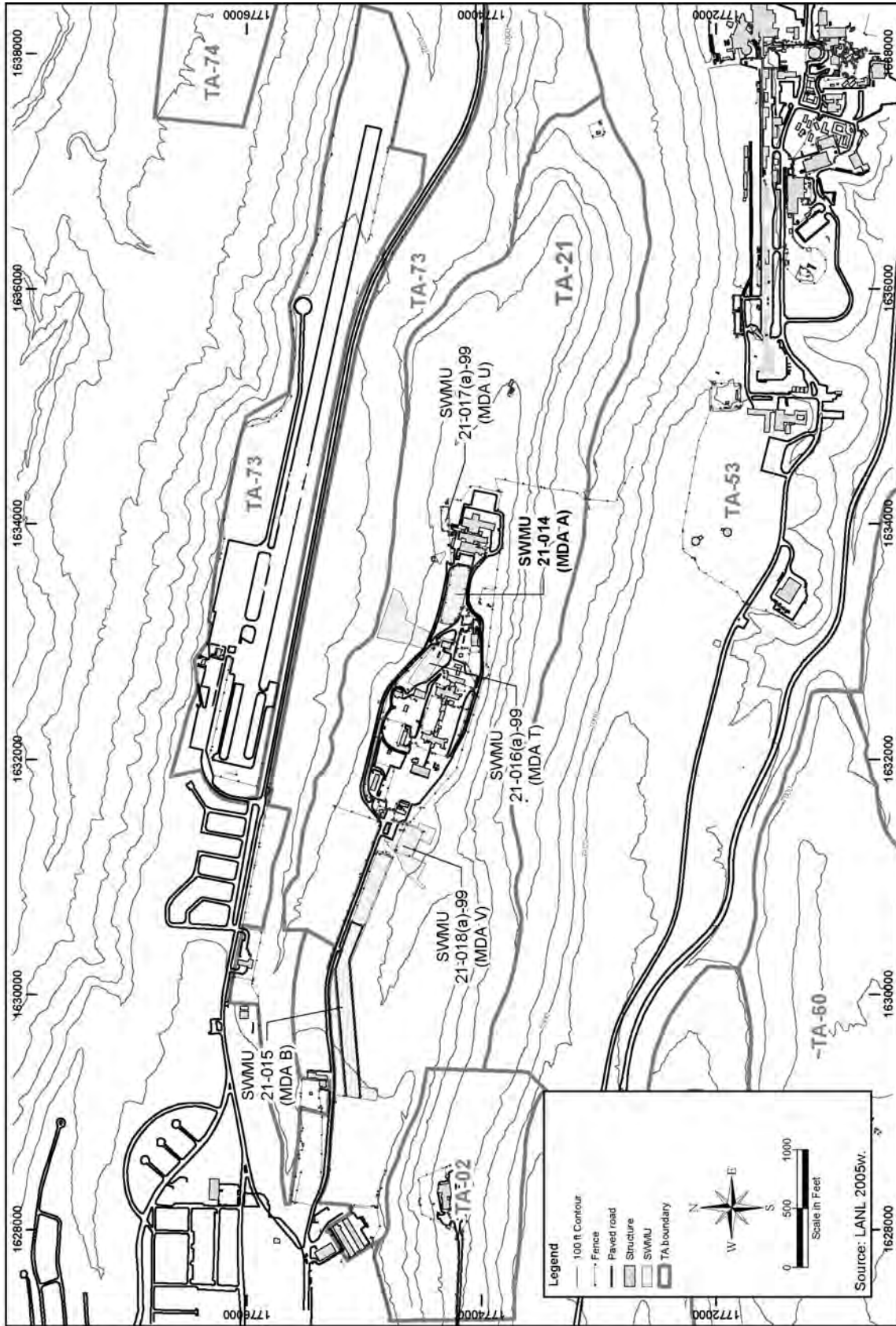


Figure I-4 MDAs A, B, T, U, and V within TA-21

I.2.5.2.1 Material Disposal Area A

MDA A (SWMU 21-014) is on a site covering 1.25 acres (0.51 hectare) between DP West and DP East.

History of MDA A. In 1945, two disposal pits were dug at the east end of the MDA, and two underground tanks (“General’s Tanks”) for liquid waste storage were emplaced at the west end. During 1969, a large pit in the center of the MDA was dug for demolition debris (**Figure I-5**) (LANL 1991).

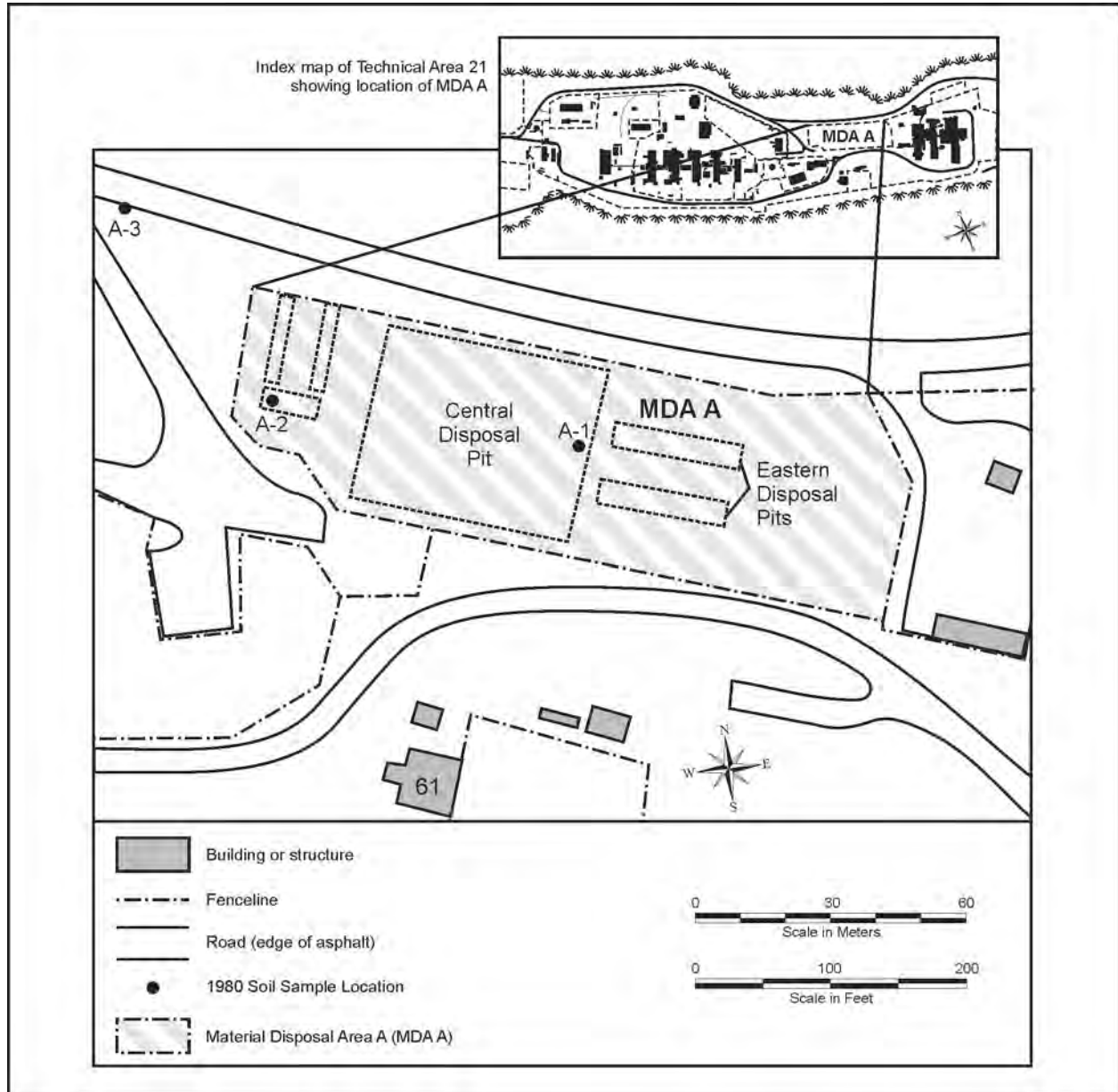


Figure I-5 Material Disposal Area A

Eastern Pits. Contemporary engineering drawings depict four pits. Yet only two pits were built, based on later engineering drawings showing pits roughly 15 feet (4.6 meters) wide at the top and 12 feet (3.7 meters) deep, as well as other documentation (Rogers 1977, LANL 1991). The MDA Core Document (LANL 1999b) states that the pits were 13 feet (4 meters) deep and received 36,000 cubic feet (1,020 cubic meters) of “solid wastes with alpha contamination accompanied by small amounts of beta and gamma” (Rogers 1977). The work plan for TA-21 states that the pits received “laboratory equipment, building construction material, paper, rubber gloves, filters from air cleaning systems, and contaminated or toxic chemicals.” The possibility exists that “plutonium, polonium, uranium, americium, curium, Radium-Lanthanum [sic], actinium, and waste products from the Water Boiler” were present in the waste. “Polonium and plutonium-239 and plutonium-240 were also thought to be the major contaminants in the waste” (LANL 1991).

During the early 1950s, several 55-gallon (208-liter) drums were stored at the east end of the MDA containing a solution of sodium hydroxide and stable iodine used to scrub ventilation air containing plutonium and possibly uranium. The liquid volume and its chemical content are unknown. Drum corrosion released some of the solution to surface soil. The drums were removed in 1960 and the storage area paved (LANL 1999b).

General’s Tanks. In 1945, two 50,000-gallon (189,000-liter) steel tanks (named after General Leslie Groves) were buried on the west end of the MDA to store solutions containing plutonium-239 and plutonium-240 (LANL 1999b). The tanks are shown in **Figure I-6** and described below (Rogers 1977):

The tanks are 12 feet (3.7 meters) in diameter and 62 feet-10 inches (19.1 meters) long. They were placed 20 feet (6.1 meters) apart in pits 12 feet (3.7 meters) deep, 15 feet (4.6 meters) wide, and probably 86 feet 10 inches (21.0 meters) long on four concrete piers. Each pier was 4 feet-10 inches (1.5 meters) high, with the bottom 2 feet (0.6 meters) below the bottom of the pit. Each tank rested on piers 1 foot (0.3 meters) above the bottom of the pit. Sand was placed in the bottom of the pit up to the top of the piers—a depth of 1 foot-10 inches (0.5 meters). Thoroughly packed earth filled the area between the tank and most of the rest of the pit. Directly above the tanks, loose dirt fill was specified. A concrete slab 8 inches (20.3 centimeters) thick, 56 feet (17.1 meters) wide, and 68 feet 10 inches (21 meters) long was poured 1.5 feet (0.5 meters) above the tanks. Approximately 5 feet (1.5 meters) of earth fill was placed above the concrete slab. This final earth fill formed a mound 2.25 to 5.75 feet (0.7 to 1.8 meters) above grade. On the north end of each tank, a vent extended 15 feet (4.6 meters) above the mound. On the south end of each tank, the fill pipe is enclosed in a concrete box with outside dimensions 2 feet-10 inches (0.9 meters) high, 2 feet-10 inches (0.9 meters) wide, and 4 feet-4 inches (1.3 meters) long. The box extended 1 foot (0.3 meter) above the mound.

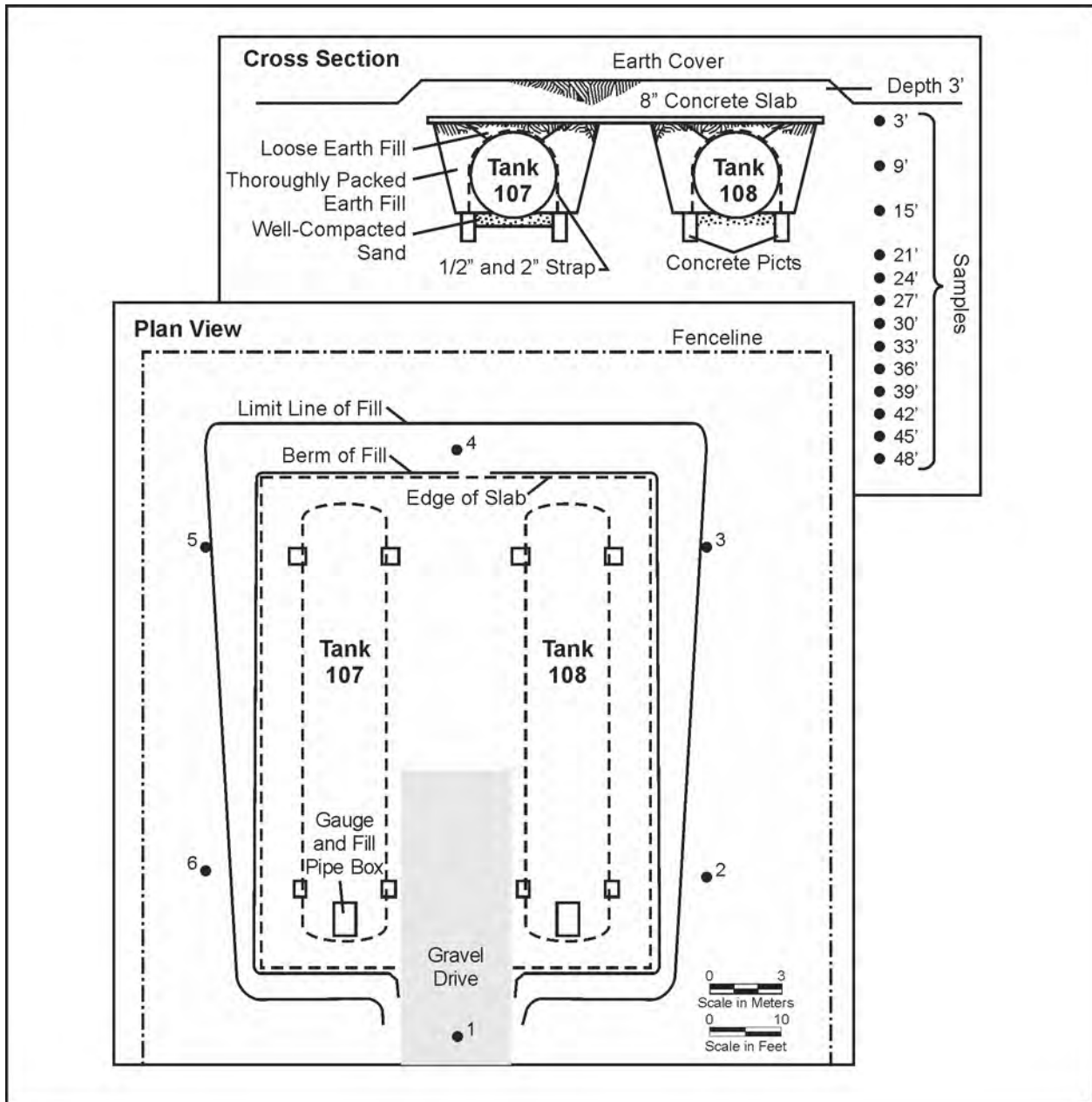


Figure I-6 General's Tanks within Material Disposal Area A

Solutions containing plutonium-239 and plutonium-240 in sodium hydroxide were to be stored until the plutonium could be extracted (LANL 1991, 1999b). But in 1975, the solution was removed, solidified in cement, and buried in MDA A, leaving a residual sludge within the tanks. The solidified waste was subsequently moved to Pit 29 in MDA G, where it is being stored (LANL 1999b). Evidence of rain water entry into the tanks led to the sealing of openings in the top of the tanks in 1985 (LANL 1991).

Central Pit. In 1969, a pit was dug in the center of MDA A to a depth of 22 feet (6.7 meters), leading to a waste capacity of 4,885 cubic yards (3,735 cubic meters). The pit received waste from operations in TA-21. In 1972, the pit was enlarged (but not deepened) to a total capacity of

18,736 cubic yards (14,325 cubic meters). The pit received plutonium-contaminated debris from demolition of a frame and masonry building. Demolition was finished in 1974, after which the remaining portions of the pit were filled with waste. A soil cover was emplaced in May 1978. Radionuclides included plutonium-238, plutonium-239, plutonium-240, uranium-235, depleted uranium, and other isotopes (LANL 1989, 1991).

Waste Inventory. Documentation about waste inventory is limited.

Eastern Pits. Memoranda and other information suggest that the dominant radionuclide contaminants were plutonium-239, plutonium-240, and polonium. The pit may contain small quantities of uranium, americium-241, and other isotopes. The pit and its surroundings may contain residues from the leaking drums of iodine in a sodium hydroxide solution (LANL 1991).

General's Tanks. The 1991 work plan for TA-21 estimated the total tank inventory to be 12 to 25 curies, mostly plutonium-239 and plutonium-240, but including plutonium-241 and americium-241 (LANL 1991).⁸ It was estimated that one-third of the activity was americium-241 (Rogers 1977). A more recent report estimates 54.3 curies of plutonium-239, 78.9 curies of plutonium-241, 6.07 curies of americium-241, and small quantities of uranium-235 and plutonium-238 (LANL 2004). The tanks probably contain metals and solvents (LANL 1991).

Central Pit. This pit probably contains plutonium-238, plutonium-239, plutonium-240, uranium-235, depleted uranium, and other isotopes (Rogers 1977). It is unknown whether the pit contains chemically hazardous wastes (LANL 1991).

Current Configuration. MDA A consists of a fenced grassy area between DP East and DP West, bordered to the north and south by paved roads. Photographs suggest that about 10 to 20 percent of the MDA is paved with asphalt.

Site Investigations. Historical site investigations included surface and subsurface sampling in 1980 and 1984 and a geophysical investigation in 1989. Four test holes were drilled next to the General's Tanks in 1974 and six holes in 1983. Surface soil samples found uranium and plutonium-238, plutonium-239, plutonium-240, above background levels in most of the area over and near the General's Tanks. Limited data suggested elevated uranium levels in vegetation. This contamination was covered after site remediation in 1985 and 1987. Subsurface samples collected in 1974 and 1983 near the General's Tanks to 30-foot (9.1-meter) depths found uranium and plutonium-238, plutonium-239, and plutonium-240, above background levels in most sampling intervals (LANL 1991). The 1989 geophysical investigation used several remote sensing techniques (magnetics, electromagnetics, resistivity, radar, and self-potential) to improve knowledge of pit and trench geometries and to locate other buried material (LANL 1989).

The MDA A Investigation Work Plan required by the Consent Order was submitted to NMED by the January 31, 2005 due date (LANL 2005m, 2005b). The MDA A Investigation Report was completed and submitted to NMED on November 9, 2006.

⁸ Having a 13-year half-life, plutonium-241 is formed along with plutonium-239/240 in a nuclear reactor and is essentially inseparable from it. Plutonium-241 decays to americium-241, an isotope having a 458-year half-life (LANL 1991).

I.2.5.2.2 Material Disposal Area B

MDA B (SWMU 21-015) is the largest MDA in TA-21. It is within a narrow site covering 6 acres (2.4 hectares) south of and parallel to DP Road west of MDA V (**Figure I-7**).

History of MDA B. MDA B operated from 1945 to 1948 (LANL 1999b) and received waste from DP East and DP West, including laboratory waste and debris, and probably limited volumes of liquid wastes (LANL 2004d). It also received waste from other areas of LANL. Unlike the practice at other MDAs of layering waste within disposal pits (see MDA C in Section I.2.5.4), the depth and width of the MDA B pits were filled with waste before backfilling. This disposal practice used pit capacity efficiently but led to cover subsidence. After MDA B was closed following a 1948 pit fire⁹, subsidence craters were filled with noncontaminated concrete and soil from construction sites (LANL 1991).

The 1948 pit fire was probably caused by spontaneous combustion of mixed chemicals in waste. The fire was intense, lasted an estimated 2 hours, and covered an area of 2,500 square feet (232 square meters) (LANL 1991). MDA B was closed and another disposal site was developed (probably MDA C) that was farther from living and working areas (Rogers 1977). In 1966, the western two-thirds of the MDA was fenced, paved, and leased to Los Alamos County for trailer storage. The storage park has since been closed (LANL 1991).

Work performed in 1982 to stabilize the eastern end of MDA B included moving the fence, decontaminating surfaces, removing vegetation, and covering the area with soil that was compacted and seeded (LANL 1991). In 1984, the eastern portion of MDA B was resurfaced using several different experimental cover systems. The experimental program included field studies of barriers against biological intrusion and erosion (LANL 1986). The current cover features several variations of a nominal 3-foot-thick (1-meter-thick) crushed-tuff cover placed over the original cover (LANL 1999b).

Waste Inventory. Inventory information is largely anecdotal. The following description is from the Historical Investigation Report for the 2004 MDA B Investigation Work Plan (LANL 2004d):

The principal radioactive contaminants consist of the types of radioactive materials used at the time: plutonium, polonium, uranium, americium, curium, radioactive lanthanum, actinium, and waste products from the water boiler reactor. However, approximately 90 percent of the waste consisted of radioactively contaminated paper, rags, paper gloves, glassware, and small metal apparatuses placed in cardboard boxes by the waste originator and sealed with masking tape. The remainder of the material consisted of metal, including air ducts and large metal apparatuses. The latter type of material was placed in wood boxes or wrapped with paper. At least one truck, contaminated with fission products from the Trinity test, is buried in MDA B.

Limited volumes of liquid waste are believed to have been emplaced in at least one chemical trench in the eastern end of the MDA (LANL 2004d).

⁹ A chemical fire also occurred in 1946 that lasted about two hours and was extinguished by bulldozing dirt over the affected area (LANL 2006f).

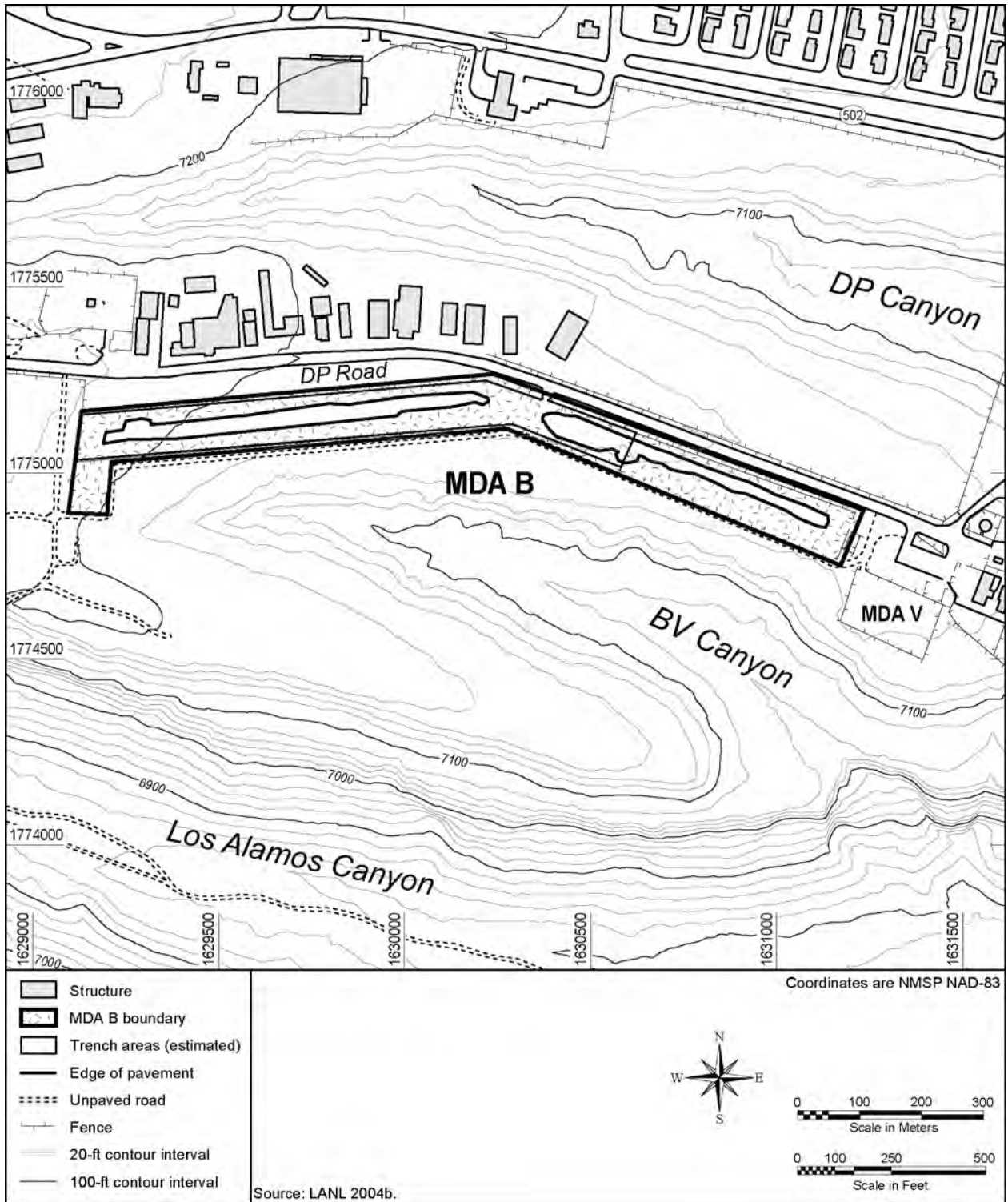


Figure I-7 Material Disposal Area B Incorporating 1998 Geophysical Survey Information

The 1977 report by Rogers (Rogers 1977) references a January 4, 1971, memorandum:

The total volume of the pits, after deducting the three foot of cover materials, is 28,000 cubic yards. These pits actually contain very little plutonium. At the time they were in use, plutonium was scarce and only that which was present as contamination was buried. (It is estimated) that the entire pit contains no more than 100 grams (6.13 curies) of plutonium-239.

The following summary of nonradioactive wastes is from the MDA B Historical Work Plan (LANL 2004d):

There are some indications hazardous chemicals may be present at MDA B. Drager, commenting on the 1948 fire, reported there was some evidence chemicals had been disposed of in the dump in an unauthorized manner; that is, in cardboard containers used for the regular disposal of common laboratory waste. In the fire, several cartons of waste caused minor explosions, and on one occasion, a cloud of pink gas arose from the debris in the dump. Documented employee interviews stated chemical disposal occurred at the east end of MDA B. Chemicals disposed of included old bottles of organic chemicals, including perchlorate, ethers, and solvents. The 1987 DOE document also stated lecture bottles, mixtures of spent chemicals, old chemicals, and corrosive gases may be in trench(es) at the east end of MDA B.

Current Configuration. The number of disposal units is uncertain (LANL 1991). A 1977 report estimated at least five pits (Rogers 1977). This reference suggests that four disposal pits were dug parallel to the fence along DP Road and that two pits were dug in the MDA at its western end (Rogers 1977). The RFI Work Plan for TA-21 references a 1964 memorandum stating that a covered shallow trench was at the extreme eastern end of the MDA. Another source indicated that several small slit trenches were dug in the eastern end of the MDA for chemical disposal (LANL 1991). The RFI Work Plan for TA-21 concluded that the MDA likely contained a minimum of four pits plus at least one chemical trench (LANL 1991). The 1991 RFI Work Plan estimated that the disposal trench surface area was 1.1 acres (0.46 hectare), covering 27,780 cubic yards (21,240 cubic meters) of buried waste (LANL 1991).

Geophysical surveys conducted in 1998 (LANL 2004d) found a single primary trench in the eastern leg of MDA B, and one to three trenches in the western leg (Figure I-7). The eastern trench is 800 feet (244 meters) long and varies from 25 to 60 feet (7.6 to 1.8 meters) wide. The western trench may contain one continuous trench or three trenches excavated end to end. The total length is 1,000 feet (305 meters)—or 300 to 400 feet (91 to 122 meters) per trench if three trenches—and its width is about 40 feet (12.2 meters). Trench depths appear to be 11 to 15 feet (3.4 to 4.6 meters) beneath the current ground surface. Depths from the top of the ground surface to the top of the waste (estimated to occur at the locations of numerous metal objects) range from 1.3 to 7.2 feet (0.4 to 2.2 meters) (mean 4.1 feet [1.2 meters]) (LANL 2004d). The MDA B Investigation Work Plan estimates that the disposal trench surface area is 2.4 acres (0.97 hectare), and the volume is 47,910 cubic yards (36,630 cubic meters) (LANL 2004d).

The investigations were not able to distinguish the slit trenches for chemical wastes reputed to be at the eastern end of MDA B. The investigations did suggest that several small chemical pits

may be in the area of these slit trenches. The investigations were not able to distinguish the short trenches reputedly excavated in the western portion of the MDA, although buried metal objects were found. The area occupied by buried objects appears to extend beyond the fence to the west and south. Their calculated depths range from 0.1 to 6.8 feet (0.03 to 2.1 meters). Partially exposed buried objects were seen (LANL 2004d).

In 2004, workshops were conducted wherein subject matter experts concluded that for purposes of a planned program of investigation and remediation, MDA B could be best envisioned as comprising two sections containing chemical slit trenches, a section that may contain slit trenches or disposal pits, five sections containing debris pits, and two sections of suspected chemical waste discharge (LANL 2005p). The investigation and remediation program for MDA B is addressed in Section I.3.3.2.7.

MDA B contains no structures. The site is surrounded by a galvanized steel chain-link fence and consists of (LANL 2004d):

- a soil-covered, unpaved area covering 15,750 square feet (1,463 square meters) (105 by 150 feet [32 by 46 meters]) at the western end of MDA B
- an asphalt-paved area comprising the long western leg and the central portion of the site (1,500 by 120 feet [457 by 37 meters])
- an unpaved area comprising the eastern leg of the site (600 by 150 feet [183 by 46 meters])

Vegetation has penetrated through cracks in the asphalt, and portions of the northern and southern boundaries of the site are lined with trees (LANL 2004d).

North of the MDA and south of DP Road is an unpaved area used by businesses for parking and deliveries. Commercial buildings occupy the paved area alongside and north of DP Road. West of MDA B is a vacant lot. An abandoned underground radioactive liquid waste line that ran outside the fence along the southern boundary of the site was removed in 2007. Buried water and communication lines are beneath the area between DP Road and the north fence. A water hydrant is inside the northwest corner of the fence, and air monitoring stations are located on the northern and northeastern sides of the fence along DP Road (LANL 2004d, 2006a, 2006i).

Site Investigations. Numerous investigations have occurred since 1948. Pre-RFI investigations are summarized in the Operable Unit RFI Work Plan for TA-21, the Investigation Work Plan for MDA B, and Revision 1 of the Investigation/Remediation Work Plan for MDA B (LANL 1991, 2004d, 2006i). RFI investigations are summarized below:

Surface investigations from 1966 to 2001 have included surface soil sampling and surface flux measurements of volatile organic compounds. Americium-241, cesium-137, plutonium-238, plutonium-239, and tritium were detected consistently across the surface of MDA B. Organic chemicals were detected very infrequently at the surface of MDA B. Lead and zinc were detected above background values consistently across MDA B. Other inorganic chemicals were also detected (LANL 2006i).

Three subsurface investigation campaigns occurred in 1966, 1983, and 1998. The 1966 and 1983 investigations included vertical boreholes drilled alongside the MDA boundary. The 1983 investigations indicated potential tritium contamination at depth. The 1998 investigations included seven angled boreholes drilled beneath the disposal trenches. Lead was found at several depths in one borehole in the west end of the MDA, and in one sample from a borehole in the central portion of the MDA. Aluminum, arsenic, cadmium, mercury, and zinc were also detected. Tritium was found above background in six of seven boreholes. The tritium concentration in the borehole beneath the assumed location of the chemical trench increased slightly over the length of the boring, but decreased in concentration in the deepest sample. Hence, tritium may have been released from the disposal trenches to the subsurface tuff. Tritium sample results over all of DP Mesa may also have been affected by the operation of the Tritium Systems Test Assembly and Tritium Systems Fabrication Facility. In 1983, both of these facilities had atmospheric releases of tritium that would have been noted over all of DP Mesa (LANL 2006a). Americium-241 and strontium-90 were found in this borehole in concentrations that decreased with depth. In a different borehole, uranium-234, uranium-235, and uranium-238 were found above background in one sample (LANL 2006i).

Pore-gas sampling from the angled boreholes found trace levels of several volatile organic compounds, primarily trichloroethene (TCE) and 1,1,1-trichloroethane (TCA), in the parts-per-billion-by volume range (LANL 2006i).

The average moisture content in soils beneath the asphalt at MDA B (10.6 weight-percent) is elevated compared with surrounding surface soils (5.1 weight percent) and subsurface materials (5.6 weight percent) (LANL 2006i).

The objectives of Revision 1 of the Investigation/Remediation Work Plan are to characterize the types and quantities of waste contained in the historical disposal trenches at MDA B; to remove and properly dispose of the waste in these trenches; to collect confirmation samples to characterize the radiological, organic chemical, and inorganic chemical concentrations in the soil and rock next to the disposal trench sides and bottoms and in the deeper subsurface beneath the site; and to obtain data needed to prepare a sampling and analysis plan to support the evaluation of any potential residual risk to human health and the environment after the waste is removed (LANL 2006i). In January 2007, the work plan was approved with modifications by NMED (NMED 2007b). Additional information about the investigation/remediation program for MDA B is in Section I.3.3.2.7.

I.2.5.2.3 Material Disposal Area T

MDA T is on a site covering 2.2 acres (0.9 hectare) (**Figure I-8**). MDA T comprises Consolidated Unit 21-016(a)-99, consisting of SWMUs 21-007, 21-010(a-h), 21-011(a), 21-011(c-g, i, j), and 21-01g(a-c); and AOCs 21-001, 21-011(h), 21-028(a), C-21-009, and C-21-012 (LANL 2005c). It includes four absorption beds, more than 60 shafts, an area once used for solidified waste storage, two industrial wastewater treatment plants, associated buried piping, and various surface features that may have been impacted by facility operations (LANL 2005c).

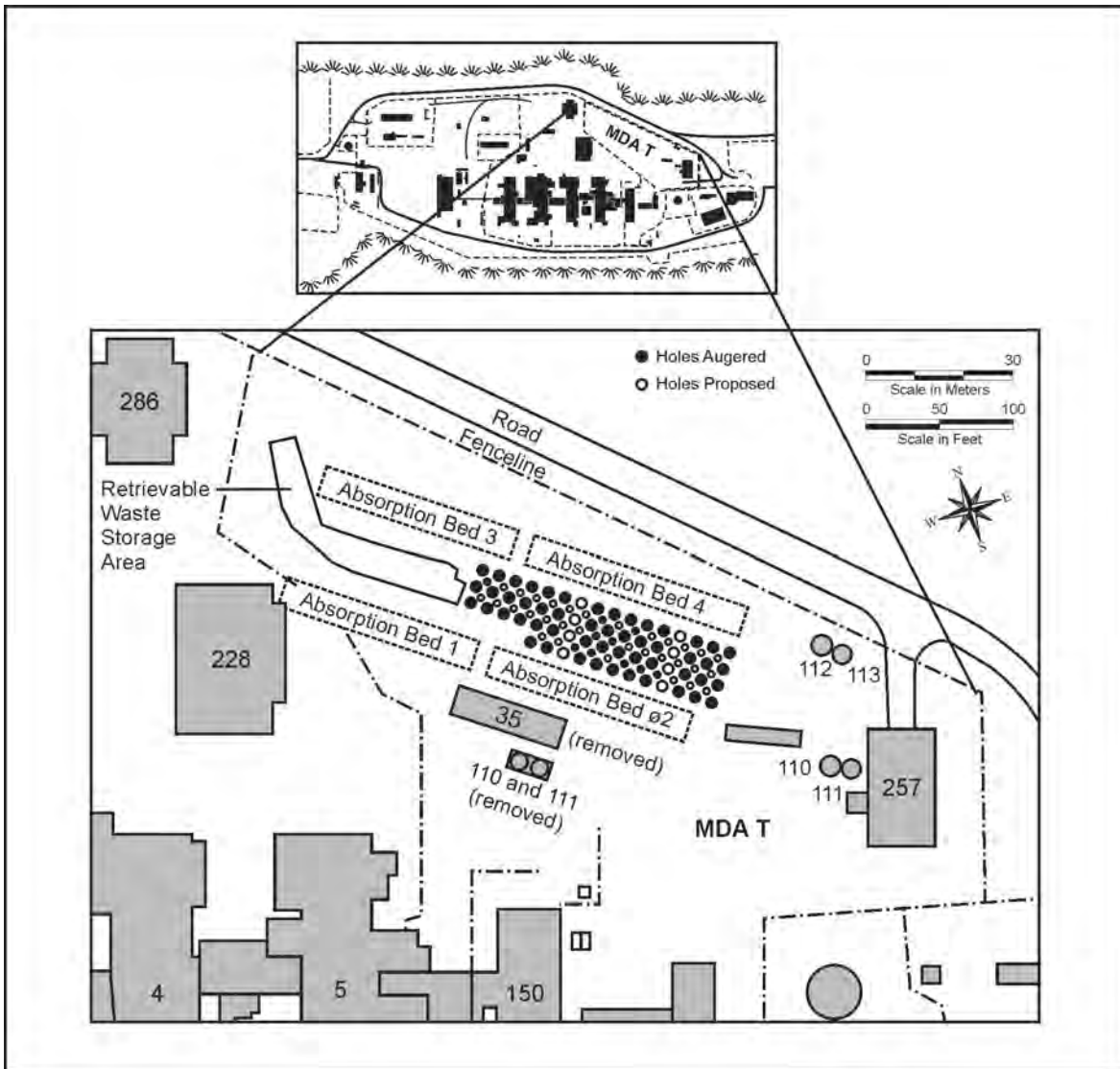


Figure I-8 Material Disposal Area T

History of MDA T. From 1945 to 1952, the absorption beds received liquids from the TA-21 plutonium laboratories. After 1952, when a liquid waste treatment plant was installed in Building 035, the beds were used only occasionally, receiving small quantities of liquid effluent until 1967, when a new liquid waste treatment process began operating in Building 257. The shafts were used between 1968 and 1983 for disposal of liquids combined into a cement paste as well as some solid wastes (LANL 1991, 2004a).

Absorption Beds. The four absorption beds (SWMU 21-016(a)) were built “about 1945” (LANL 1991).¹⁰ The four absorption beds were each 120 by 20 by 6 feet deep (36.6 by 6.1 by 1.8 meters deep).¹¹ The distance between the centers of Beds 1 and 3 and Beds 2 and 4 is 80 feet (24.4 meters) (Rogers 1977). The beds are shown in cross section in **Figure I-9** (LANL 1991).

¹⁰ MDA T may have received wastes as early as 1943 (LANL 1991).

¹¹ The beds were 4 feet (1.2 meters) deep, the bottoms of the beds were cut level, and the east and west sides of each bed were sloped so that only the center 100 feet (30.5 meters) of each bed had a depth of 4 feet (1.2 meters) (Rogers 1977).

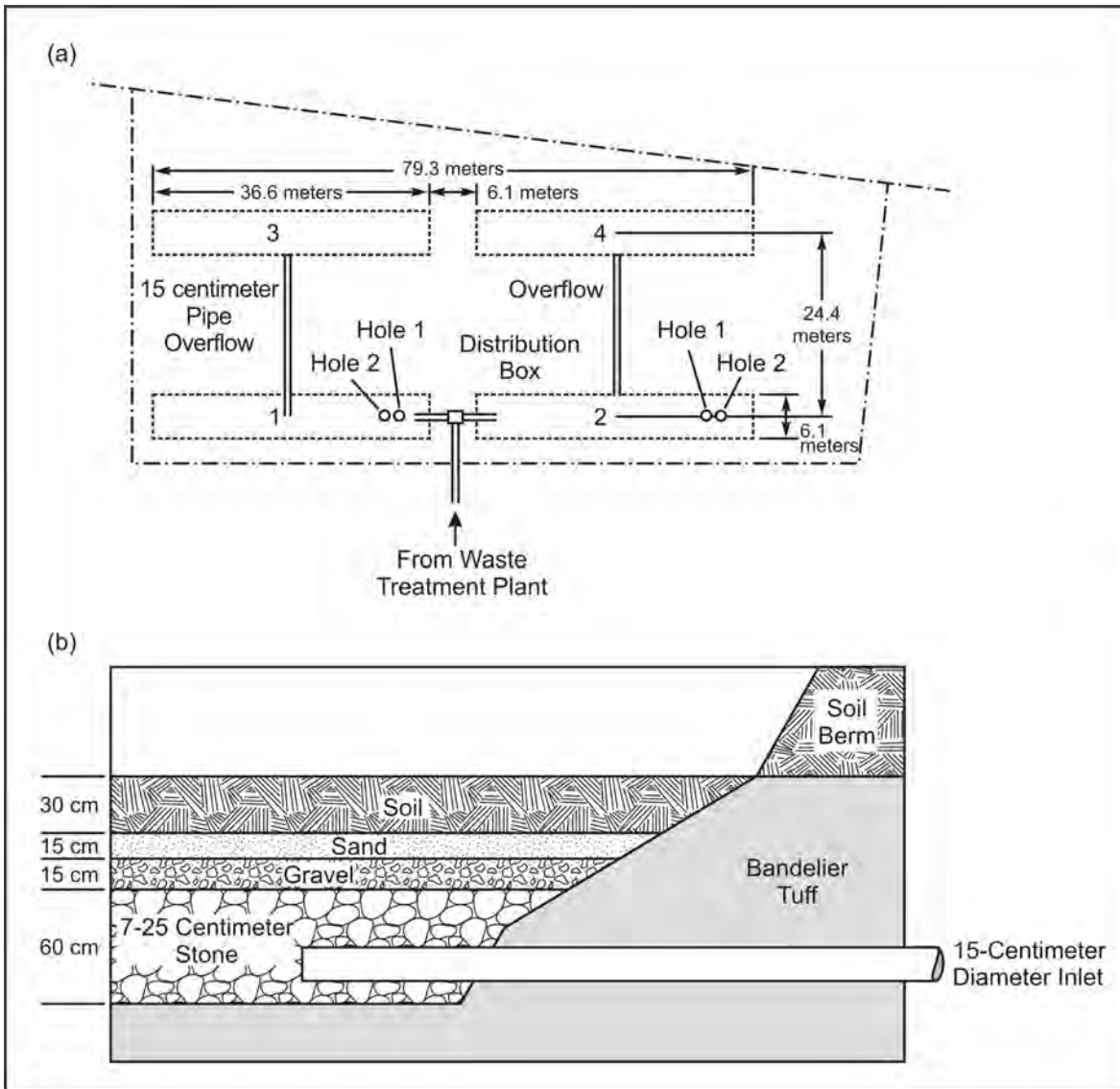


Figure I-9 Absorption Bed and Distribution Pipe Cross-Section

The two sources for liquid waste from DP West were (**Figure I-10**) (LANL 1991, Rogers 1977):

- Effluent from sumps in Buildings 2, 3, 4, and 5 that was piped to a distribution box located between Beds 1 and 2
- Effluent from the Building 12¹² floor drain that was piped directly to Bed 1

The concrete distribution box (SWMU 21-011(c)) has dimensions of 4 by 3 by 4 feet (1.2 by 0.9 by 1.2 meters) with 6-inch-thick (15.2-centimeter-thick) walls. Overflow pipes connect Bed 1 with Bed 3 and Bed 2 with Bed 4 (Rogers 1977).

¹² This building was removed in 1973 (Rogers 1977).

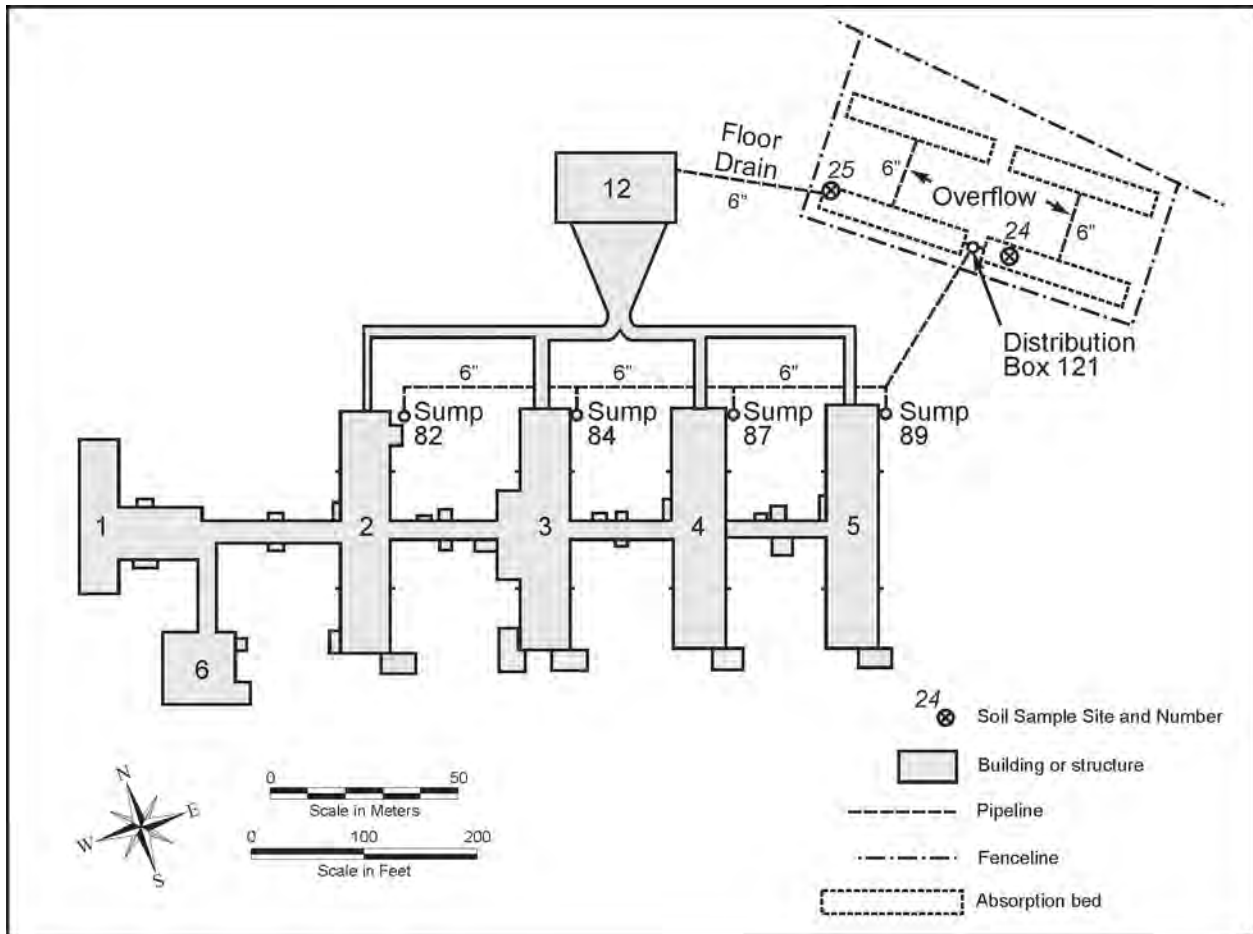


Figure I-10 Location of Lines Discharging to Absorption Beds at Material Disposal Area T Before 1952

The absorption beds occasionally became saturated and overflowed northward toward DP Canyon (Rogers 1977). Overflow associated with operational use of the beds, release of effluents from outfalls, and possibly from experimental studies has contributed to contamination in soils north of the site. The western end of the MDA has experienced erosion (LANL 1993h).

Disposal Shafts. Starting on May 1, 1968, more than 60 disposal shafts (SWMU 21-016) were augured (**Table I-7**), mostly between Beds 2 and 4 and, after being lined with asphalt, used mostly to dispose of cement paste from liquid waste treatment at Building 257 (LANL 1991). The larger shafts (numbers 1 through 60) are on 12-foot (3.7-meter) centers. (There are gaps in the sequencing of the shafts because several shafts were not augured.) The smaller shafts (shafts 70 through 100) were placed between the surface matrices of the larger shafts (Rogers 1977).

Wastes in Retrievable Storage. In 1974, a pit 30 by 60 by 20 feet deep (9 by 18 by 6 meters deep) was dug between Absorption Beds 1 and 3 for storage of liquid wastes cemented into corrugated metal pipes. These pipes were moved to MDA G in the 1980s (LANL 1991). The excavation (SWMU 21-016(b)) was backfilled (LANL 2004a).

Table I-7 Material Disposal Area T Waste Disposal Shaft Depths and Diameters

| Shaft | Diameter (feet) | Depth (feet) | Shaft | Diameter (feet) | Depth (feet) |
|-------|-----------------|--------------|-------|-----------------|--------------|
| 1 | 8 | 61 | 42 | 8 | 21 |
| 2 | 8 | 21 | 43 | 8 | 62 |
| 3 | 8 | 27 | 44 | 8 | 63 |
| 5 | 8 | 29 | 46 | 8 | 66 |
| 6 | 8 | 27 | 47 | 8 | 25 |
| 8 | 8 | 67 | 48 | 8 | 63 |
| 9 | 8 | 63 | 49 | 8 | 67 |
| 10 | 8 | 23 | 50 | 8 | 65 |
| 11 | 8 | 28 | 51 | 8 | 30 |
| 13 | 8 | 65 | 52 | 8 | 23 |
| 17 | 8 | 50 | 53 | 8 | 52 |
| 18 | 8 | 59 | 54 | 8 | 63 |
| 19 | 8 | 65 | 55 | 8 | 69 |
| 20 | 8 | 63 | 56 | 8 | 62 |
| 21 | 8 | 62 | 57 | 8 | 25 |
| 22 | 8 | 64 | 58 | 8 | 22 |
| 23 | 8 | 63 | 59 | 8 | 54 |
| 24 | 8 | 61 | 60 | 8 | 63 |
| 25 | 8 | 16 | 70 | 6 | 68 |
| 26 | 8 | 15 | 75 | 6 | 67 |
| 27 | 8 | 58 | 76 | 6 | 67 |
| 28 | 8 | 67 | 78 | 6 | 65 |
| 29 | 8 | 61 | 80 | 6 | 66 |
| 30 | 8 | 62 | 82 | 6 | 64 |
| 31 | 8 | 18 | 83 | 6 | 24 |
| 32 | 8 | 15 | 84 | 6 | 50 |
| 33 | 8 | 64 | 87 | 6 | 66 |
| 34 | 8 | 60 | 91 | 6 | 26 |
| 35 | 8 | 62 | 92 | 6 | 27 |
| 36 | 8 | 61 | 94 | 6 | 22 |
| 41 | 8 | 62 | 95 | 6 | 16 |
| - | - | - | 100 | 6 | 66 |

Note: The citations in the source for this table (LANL 1991) are in meters. To convert feet to meters, multiply by 0.3048.
Source: LANL 1991.

Additional Facilities and PRSs. Numerous additional facilities and PRSs are associated with MDA T (Consolidated Unit 21-016(a)-99), including:

- Building 035 (SWMU 21-010(a)). Construction on this industrial liquid waste treatment plant began in 1949 and was completed in 1952. It operated until 1967. It was decontaminated and decommissioned in 1967, and the building and some associated tanks and piping were removed and disposed of; other tanks were relocated (LANL 2005c). A septic tank and leach field were abandoned in place (LANL 2004a).
- Building 257 (SWMU 21-011(a)). This treatment plant treated and prepared wastes for disposal at MDA T and included an outfall (SWMU 21-011(k)) that discharged to

DP Canyon.¹³ The treatment plant includes a clarifier-flocculator, aboveground storage tanks and pumps, and a cement silo. Tanks associated with Building 257 include a 13,500-gallon (51,103-liter) acid holding tank (SWMU 21-011(d)), effluent holding tanks (SWMUs 21-011(f) and 21-011(g)), the Pug Mill Tank (AOC 21-011(h)), a sodium-hydroxide storage tank (SWMU 21-011(i)), and an americium raffinate storage tank (SWMU 21-011(j)) (LANL 2005c).

- SWMU 21-007. This SWMU represents airborne releases from salamanders (incinerators for waste oils and organics). The incinerators were used between 1964 and 1972 and were located atop MDA T (LANL 2005c).
- AOC 21-018(a). This former surface storage area within the MDA T fence was the location for temporary storage of alcohol, acetone, and freon (LANL 2005c).

Waste Inventory

Absorption beds. Between 1945 and 1952, the beds received 14 million gallons (53 million liters) of untreated wastewater containing plutonium and fluoride. In addition, from June 1951 to July 1952, 10,450 gallons (40,000 liters) of ammonium citrate effluent were released containing plutonium and fluoride. From 1953 through 1967, 4.3 million gallons (16 million liters) of effluent were discharged (LANL 2004a). As of January 1973, the absorption beds had received 4 curies of tritium and 10 curies of plutonium-239, plutonium-240 (94 weight-percent plutonium-239 and 6 weight-percent plutonium-240). The beds also received plutonium-238, uranium-235, and americium-241. Wastewater discharged to the beds contained fluorine, iodine, cadmium, beryllium, lead, mercury, sodium, nitrates, and chorine. It probably contained solvents and other organic chemicals (LANL 2004a).

Shafts. Radioactive wastes included cement-stabilized americium, alkaline fluoride, and plant sludge. Some shafts temporarily held wastewater. Personal protective equipment and other contaminated items were also disposed of, including (LANL 2004a):

- Shafts 3, 17, 18, 19, and 26 contain 3-foot diameter (0.9-meter-diameter) “bathyspheres” containing plutonium-239 and plutonium-240 and other mixed fission products. **Table I–8** presents the plutonium-239 inventory contributed by the bathyspheres.
- Shaft 17 contains six drums of cyanide salts fixed in asphalt.

Table I–8 Plutonium-239 Disposed of in Material Disposal Area T Shaft Bathyspheres

| <i>Shaft Number</i> | <i>Plutonium-239 Bathysphere Inventory (grams)</i> |
|---------------------|--|
| 3 | 290 |
| 17 | 342 |
| 18 | 134 |
| 19 | 245 |
| 20 | 210 |

Note: To convert grams to ounces, multiply by 0.035274.

¹³ Remediation of the outfall SWMU (21-011k) has been completed (see Section I.2.7.6).

- Shafts 50 and 54 contain demolition debris from Filter Building 012.
- Shafts 52 and 58 together contain four drums of uranium-233.

Shaft-specific inventories (as of 2004) of plutonium-239, plutonium-238, plutonium-240, americium-241, uranium-233, and uranium-235 are listed in **Table I-9**, along with volumes of the plutonium cement pastes. The shafts also contain mixed fission products (LANL 2004a).¹⁴

Table I-9 Radionuclide Inventories and Cement Paste Volume by Shaft

| Shaft | Cement Paste Volume (liters) | Pu-239 (grams) | Pu-238 (grams) | Pu-240 (grams) | Am-241 (grams) | U-233 (grams) | U-235 (grams) |
|-------|------------------------------|----------------|----------------|----------------|----------------|---------------|---------------|
| 1 | 67,440 | 20.8 | 0.025 | 1.2 | 21 | – | – |
| 2 | 23,920 | 3.7 | 0.004 | 0.2 | 2.5 | – | – |
| 3 | 10,750 | 300.2 | 0.012 | 18 | 5.3 | – | – |
| 5 | 87,200 | 12 | 0.014 | 0.7 | 24.1 | – | – |
| 9 | 88,780 | 25 | 0.029 | 1.5 | 23.3 | – | – |
| 10 | 18,660 | 4 | 0.005 | 0.2 | 4.2 | – | – |
| 11 | 18,950 | 3.2 | 0.004 | 0.2 | 2.6 | – | – |
| 13 | 85,500 | 39.6 | 0.047 | 2.4 | 34.6 | – | – |
| 17 | 87,240 | 373.9 | 0.038 | 22.42 | 16.6 | – | – |
| 18 | 83,440 | 152.8 | 0.022 | 9.14 | 17.1 | – | – |
| 19 | 80,280 | 261.3 | 0.019 | 15.7 | 6.2 | – | – |
| 20 | 89,540 | 11.6 | 0.014 | 0.7 | 26.4 | – | – |
| 21 | 87,290 | 13.3 | 0.016 | 0.8 | 22.6 | – | – |
| 22 | 88,760 | 18.8 | 0.022 | 1.1 | 20 | – | – |
| 23 | 80,700 | 20.4 | 0.024 | 1.2 | 31.4 | – | – |
| 24 | 84,100 | 17.4 | 0.021 | 1 | 25 | – | – |
| 25 | 23,460 | 7.2 | 0.009 | 0.4 | 10 | – | – |
| 26 | 21,310 | 214.5 | 0.005 | 12.9 | 5.6 | – | – |
| 27 | 82,770 | 32.5 | 0.038 | 2 | 18.1 | – | – |
| 28 | 89,880 | 40.4 | 0.048 | 2.4 | 33.5 | – | – |
| 29 | 87,850 | 4.2 | 0.005 | 0.3 | 9.8 | – | – |
| 30 | 87,090 | 14 | 0.017 | 0.8 | 18.8 | – | – |
| 31 | 25,900 | 3 | 0.003 | 0.2 | 2.9 | – | – |
| 32 | 22,510 | 5.4 | 0.006 | 0.3 | 9.4 | – | – |
| 33 | 90,490 | 24.8 | 0.029 | 1.5 | 20.5 | – | – |
| 34 | 89,270 | 11.4 | 0.013 | 0.7 | 21.3 | – | – |
| 35 | 87,730 | 16 | 0.019 | 1 | 25.3 | – | – |
| 36 | 89,410 | 12.4 | 0.015 | 0.7 | 25.9 | – | – |
| 41 | 68,600 | 20.5 | 0.024 | 1.2 | 18.1 | – | – |
| 42 | 32,730 | 4.2 | 0.005 | 0.3 | 2.5 | – | – |
| 43 | 89,000 | 28.1 | 0.033 | 1.7 | 29.5 | – | – |
| 44 | 87,890 | 14.5 | 0.017 | 0.9 | 21.2 | – | – |
| 46 | 82,540 | 33 | 0.039 | 2 | 35.6 | – | – |

¹⁴ In July 1976, the shafts were estimated to contain 7 curies of uranium-235, 47 of plutonium-238, 191 of plutonium-239, 3,761 of americium-241, and 3 of mixed fission products (LANL 2004a).

| Shaft | Cement Paste Volume (liters) | Pu-239 (grams) | Pu-238 (grams) | Pu-240 (grams) | Am-241 (grams) | U-233 (grams) | U-235 (grams) |
|--------------------------------------|------------------------------|----------------|----------------|----------------|----------------|---------------|---------------|
| 47 | 35,100 | 16.6 | 0.02 | 1 | 15.5 | – | – |
| 48 | 65,760 | 21.7 | 0.026 | 1.3 | 23.4 | – | – |
| 49 | 92,800 | 62.2 | 0.073 | 3.7 | 49.4 | – | – |
| 50 | 72,290 | 18.5 | 0.022 | 1.1 | 21.2 | – | – |
| 51 | 38,620 | 11.4 | 0.013 | 0.7 | 11.7 | – | – |
| 53 | 71,610 | 28.7 | 0.034 | 1.7 | 33.9 | – | – |
| 55 | 90,600 | 45.9 | 0.054 | 2.8 | 26.7 | – | – |
| 56 | 83,870 | 23.9 | 0.028 | 1.4 | 32.6 | – | – |
| 57 | 37,200 | 19.1 | 0.023 | 1.1 | 11.9 | – | – |
| 59 | 77,400 | 44.2 | 0.052 | 2.7 | 31.1 | – | – |
| 60 | 90,460 | 38.2 | 0.045 | 2.3 | 33 | – | – |
| 70 | 52,400 | 79.9 | 0.094 | 4.8 | 29.8 | – | – |
| 75 | 52,800 | 32.9 | 0.039 | 2 | 35.4 | – | – |
| 76 | 52,600 | 56.7 | 0.067 | 3.4 | 53.1 | – | – |
| 78 | 49,800 | 7.6 | 0.009 | 0.5 | 0.8 | – | – |
| 80 | 56,300 | 20 | 0.024 | 1.2 | 4 | – | – |
| 82 | | 8.9 | 0.01 | 0.5 | 2.4 | – | – |
| 83 | 18,000 | 19.6 | 0.023 | 1.2 | 4.8 | – | – |
| 84 | 37,700 | 9.5 | 0.011 | 0.6 | 0.3 | – | – |
| 87 | | 7.7 | 0.009 | 0.5 | 0.4 | – | – |
| Complex B (52, 58) | 64,690 | 34.2 | 0.04 | 2.1 | 20.1 | 713 | – |
| Complex A (6, 8, 54, 90, 91, 92, 94) | 125,630 | 99.8 | 0.118 | 6 | 79.6 | – | 713 |
| Total (grams): | – | 2,471 | 1.5 | 148 | 1,112 | 713 | 713 |

Pu = plutonium, Am = americium, U = uranium.

Note: To convert liters to gallons, multiply by 0.26418; grams to ounces, multiply by 0.035274.

Source: LANL 2004a.

Current Configuration. The absorption beds and shafts are enclosed by a chain-link fence (except the southwest corner of Absorption Bed 1). The surface is vegetated with weeds, grasses, chamisa bushes, and two young ponderosa pine trees (LANL 2004a). MDA T has a downward slope from south to north. Backfilling and grading have added 5 to 6 feet (1.5 to 1.8 meters) of soil to the original surface of the beds, shafts, and the retrievable waste storage area. The bottoms of the absorption beds are about 9 feet (2.7 meters) below current ground surface (LANL 2004a).

MDA T is a complex site containing or contingent to several SWMUs, some active and some not. In addition to buried and abandoned piping and lines from utilities and waste treatment and transfer operations, complex groupings of utility lines and corridors pass through MDA T. A corridor of acid waste lines runs underground from the northwest corner of Building 257 to the southwest of former Building 035. Waste drain lines also run from the northwest corner of Building 257 north to effluent tanks 112 and 113. An acid waste line runs southeast from former Building 035 before angling northeast to the effluent tanks. An acid waste line also runs from the southwest corner of former Building 035, under Building 257, and east out of MDA T. A natural gas line runs east-west under Building 257 and along the south side of former Building

035. Main water lines run just south of the MDA T fence lines, with feeder lines north to former Building 035 and Building 257. Aboveground electrical lines run just north of the MDA T fence line, splitting to the south between former Building 035 and Building 257, and to the east over tanks 112 and 113 and along the north side of Building 257. Underground electrical lines run between former Building 035 and Building 247 (LANL 2004a).

Site Investigations. Pre-RFI site investigations at MDA T are summarized in the Operable Unit RFI Work Plan for TA-21 and in the February 2004 Investigation Work Plan for MDA T (LANL 1991, 2004a). Pre-RFI investigations occurred in 1946, 1947, and 1948. In 1953, the U.S. Geological Survey concluded that no appreciable horizontal migration of contamination had occurred. From 1959 to 1961, the U.S. Army Corps of Engineers dug a test pit (caisson) next to Absorption Bed 1 and drilled six angled boreholes under the bed. In 1960 and 1961, infiltration studies were performed by adding large quantities of raw liquid waste and ordinary tap water to Absorption Bed 1 (LANL 2004a).

Additional boreholes were drilled in 1967 and 1974 to measure tuff moisture content. Paleochannels at depths of 15 to 25 feet (4.6 to 7.6 meters) were found. Moisture migration studies occurred in 1978, and shallow soil sampling and radiological characterizations occurred in 1984 and 1986 (LANL 2004a). Results of the field study initiated in 1978 showed plutonium and americium-241 at depths to 100 feet (30 meters) below ground surface (LANL 1984).

Phase I RFIs collected surface soil samples in 1992, 1994, 1995, 1996, and 1997, as well as tuff samples from boreholes. The following contaminants were found (LANL 2004a):

- In the surface soil and shallow subsurface extending to DP Canyon, americium-241, plutonium-238, and plutonium-239 were elevated compared with background values.
- In soil and subsurface soil and tuff samples from boreholes, several metals were detected above background values. Levels of cadmium, copper, and nickel above background values were found near the influent line for Building 035 and at a nearby location.

Additional work was proposed in the 2004 MDA T Investigation Work Plan: a site-wide radiation mapping survey; sampling of drainage channels; borings to characterize release from the absorption beds and the possible presence of perched water and bedrock fractures; and further characterization of the area surrounding former Building 035 and existing Building 257 (LANL 2004a). The Investigation Report for MDA T was completed and submitted to NMED on September 18, 2006. In October 2007, DOE issued a proposed subsurface vapor monitoring plan for MDA T that included installation of three wells for quarterly sampling of tritium and volatile organic compounds (LANL 2007f).

I.2.5.2.4 Material Disposal Area U

MDA U is within a fenced, 0.2-acre (0.08-hectare) site north of Buildings 21-152 and 21-153 in DP East (**Figure I-11**). It contains two absorption beds (SWMUs 21-017(a) and (b)).

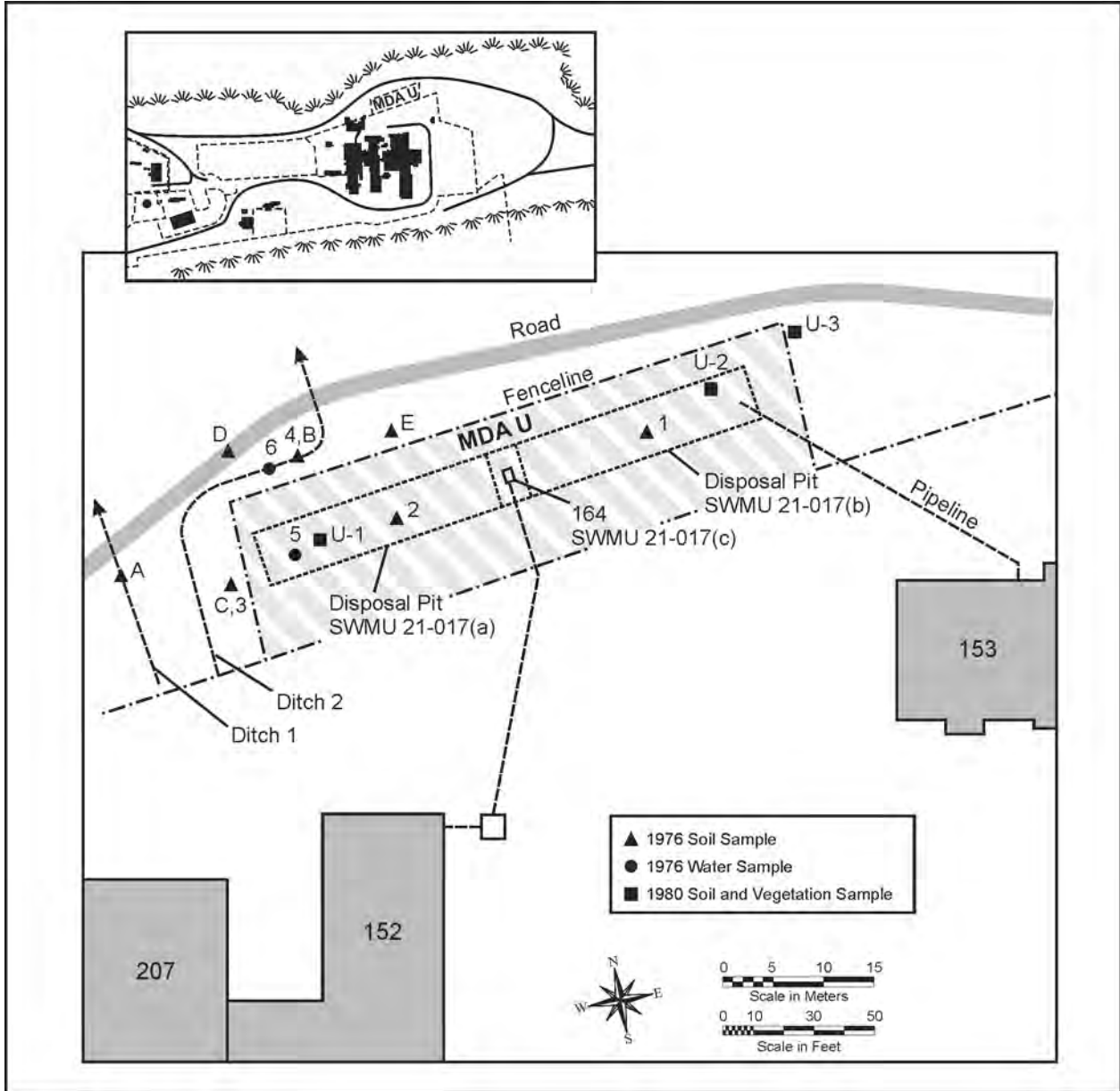


Figure I-11 Material Disposal Area U Showing Pipelines for Liquid Effluents

History of MDA U. The absorption beds were used from 1948 to 1968 for disposal of liquid wastes (LANL 1991). Each bed was 80 by 20 by 6 feet (24 by 6.1 by 1.8 meters) (LANL 2004k). The beds were filled with 24 inches (61 centimeters) of cobbles and overlain by 6 inches (15 centimeters) of gravel and 6 inches (15 centimeters) of sand. Covering the sand was 12 inches (30 centimeters) of soil (LANL 2004k). Between the two beds was a distribution box (SWMU 21-017(c)) with lines leading to the beds (LANL 1999b). Liquid waste included effluent from Buildings 21-152 and 21-153, and from 21-155, the Tritium Systems Test Assembly¹⁵ (LANL 2004k).

Effluent from Buildings 21-152 and 21-153 was received until 1968 (LANL 2004k). Effluent discharge from Building 21-155 presumably ceased at the same time. In addition, until 1976 the west bed received water from a cooling tower for Building 21-155 (LANL 1991, 2004k). MDA U also received oil from precipitrons¹⁶ and from Building 21-152 floor drains (LANL 2004k).

In 1985, the distribution box and lines were removed (LANL 1991), as was a portion of the line from the cooling tower (LANL 2004k). A trench 20 feet (6.1 meters) wide, 100 feet (30 meters) long, and 4 to 13 feet (1.2 to 4.0 meters) deep was dug, and some, but not all, contaminated soil was removed. After a plastic liner was placed in the trench to denote the excavation boundary, the trench was filled with soil. The excavated area was covered with 6 inches (15 centimeters) of topsoil and drainage problems were remedied (LANL 1991).

In 1987, ditches were placed along the south fence to prevent runoff; additional topsoil, gravel mulch, and seeds were deposited inside the fence; and brass markers were placed at the corners of the site. Additional collection ditches were excavated in 1990 to prevent runoff from the surrounding area from flowing across MDA U (LANL 1991).

In 2001, exploratory trenches were dug across each absorption bed to find the plastic liner placed over the excavated areas when the drain line and absorption bed material were removed in 1985. Black plastic was found in the west absorption bed at a depth of 3.5 to 4 feet (1.1 to 1.2 meters). Cobbles up to 20 inches (0.5 meters) in diameter were seen under the plastic. In the east absorption bed, a clear liner was found at about 3 feet (0.9 meter) below ground surface and a black liner at 7 feet (2.1 meters), above a cobble layer (LANL 2006g).

Waste Inventory. Between 1945 and 1968, the beds received 135,000 gallons (511,000 liters) of liquid. The primary radionuclide was polonium-210.¹⁷ The beds also received actinium-227, plutonium, and tritium. About 2.5 curies of actinium-227 were discharged in 1953, mainly from Building 21-153.¹⁸ A 1946 memorandum referenced in the MDA U Investigation Work Plan states that plutonium and polonium were measured in effluent discharged to the beds. The beds probably received inorganic materials, organic chemicals, acids, and oils (LANL 2004k).

Much of the contamination discharged to the beds has been removed.

¹⁵ Building 21-155 (Tritium Systems Test Assembly) is not shown in Figure I-11.

¹⁶ Precipitrons were air filters installed in the filter building, Building 21-153, and used to filter air exhausted from Building 21-152 (LANL 1991).

¹⁷ Because polonium-210 has a half-life of 138.4 days, current inventories of polonium-210 are effectively nonexistent. Polonium-210 decays to stable lead.

¹⁸ A filter building decommissioned in 1978.

Current Configuration. MDA U is a grassy area, fenced to the north, east, and west by a security fence, and to the south by an industrial site. Building 21-153 was unused after March 1970 and demolished in 1978. The effluent pipeline from Building 21-153 has been removed, along with the pipeline from Sump 173 at Building 21-152. Sump 173 remains (LANL 2004k).

Site Investigations. Early site investigations included effluent sampling in 1946; surface soil and water sampling in 1976; an investigation of soil, vegetation, and tar in 1980; a subsurface investigation in 1983; and soil and vegetation sampling in 1984. RFIs were conducted in 1992, 1994, 1998, and 2001. Samples of soil and sediment found americium-241, plutonium-238, plutonium-239, tritium, chromium, lead, mercury, uranium, and zinc in concentrations above background values. Organic chemicals were infrequently found in low concentrations (LANL 2004k).

The 1998 and 2001 investigations sampled fill from the beds. Tritium and uranium-234 were found in levels above background values, and actinium-227 progeny were found in the eastern beds. The 1998 investigations found uranium-234, uranium-235, actinium-227 progeny, and tritium in boreholes. Subsurface samples found aluminum, arsenic, barium, beryllium, chromium, copper, lead, manganese, and mercury at levels above background values. Subsurface pore-gas samples showed numerous low-level detections of organic chemicals (LANL 2004k).

Field investigations in 2005 included characterization drilling and logging of nine boreholes, continuous core sampling in 5-foot (1.5-meter) intervals, field screening for radiation and volatile organic compounds, collecting surface and subsurface samples for chemical characterization, and collecting subsurface samples for geotechnical characterization.

In the 2006 Investigation Report for MDA U, LANL staff concluded that the nature and extent of contamination in surface and subsurface media had been defined, and that no perched saturation zones existed under the site. LANL staff also concluded that neither additional corrective action nor further characterization was warranted. LANL staff recommended that the three SWMUs within the MDA U boundary be designated as “complete with controls,” the controls being the maintenance of the land use as industrial (LANL 2006g). On September 28, 2006, NMED approved the Investigation Report and issued a Corrective Action Complete with Controls certification of completion for SWMUs 21-017(a-c) and 21-022(f) pursuant to the Consent Order (NMED 2006b).

I.2.5.3 Technical Area 49: Material Disposal Area AB

Created in 1959 from TA-15, TA-49 is on the southwestern edge of LANL (see Figure I-1). MDA AB is on Frijoles Mesa.

History. Beginning in the fall of 1959, underground hydronuclear experiments were conducted to investigate the possibility of a nuclear yield from accidental detonation of a nuclear weapon's high explosive component. Experiments were conducted through August 1961 (LANL 1992b), mainly in four underground shaft areas (Areas 1-4) to which Areas 2A and 2B were added. (These six areas, plus an area of surface contamination, compose MDA AB.) A site diagram (**Figure I-12**) shows the areas containing the hydronuclear shafts, central control area, supporting areas, and other nearby PRSs and site features (LANL 1992b), including:¹⁹

- Areas 1, 2, 2A, 2B, 3, and 4: SWMUs 49-001(a-f)
- Surface contamination, particularly in Area 2: SWMU 49-001(g)
- Area 5, central control area: SWMU 49-008(a), soil contamination; SWMU 49-005(b), a small landfill; and SWMU 49-006, a sump
- Area 6, open burning/landfill area: SWMU 49-004
- Area 10, underground experimental area: SWMU 49-002, the experimental area; and SWMU 49-005(a), a small nearby landfill
- Area 11, radiochemistry and small-scale shot area: SWMU 49-008(c), soil contamination; and SWMU 49-003, inactive leach field and drain lines
- Area 12, Bottle House Area: SWMU 49-008(d), soil contamination

Areas 1, 2, 2A, 2B, 3, and 4. Between January 1960 and August 1961, about 4 dozen hydronuclear, calibration, and equation of state experiments were conducted. At least 23 additional underground containment, equipment development, and mockup experiments were conducted using high explosives, and, in a few cases, small quantities of uranium-238 or radioactive tracer. The experiments caused explosive dispersal of uranium-235, plutonium-239, lead, beryllium, and uranium-238 at the bottoms of backfilled shafts that varied in depth from 31 to 142 feet (9.4 to 43 meters) (LANL 1992b). Some experiments used radioactive tracers, and many experiments with and without special nuclear material used uranium-238. The maximum fission energy released in any experiment equaled only a few tenths of a pound of high explosive (LANL 1992b). Less than 10 millicuries of fission products probably remain, and only a few curies of tritium were expended. Special nuclear material was never used in Area 3 (LANL 1992b).

Essentially all of the contamination is deep underground. Most contaminants are confined to within maximum radii of 10 to 15 feet (3.0 to 4.6 meters) from detonation points. Small levels of surface contamination in Area 2 resulted from inadvertent drilling into a subsurface region contaminated from a previous experiment (LANL 1992b).

¹⁹ Also shown on Figure I-12 is the Hazardous Devices Team training area (HDT Area). Remediation of SWMU 49-007(b) is administratively complete (LANL 2005a).

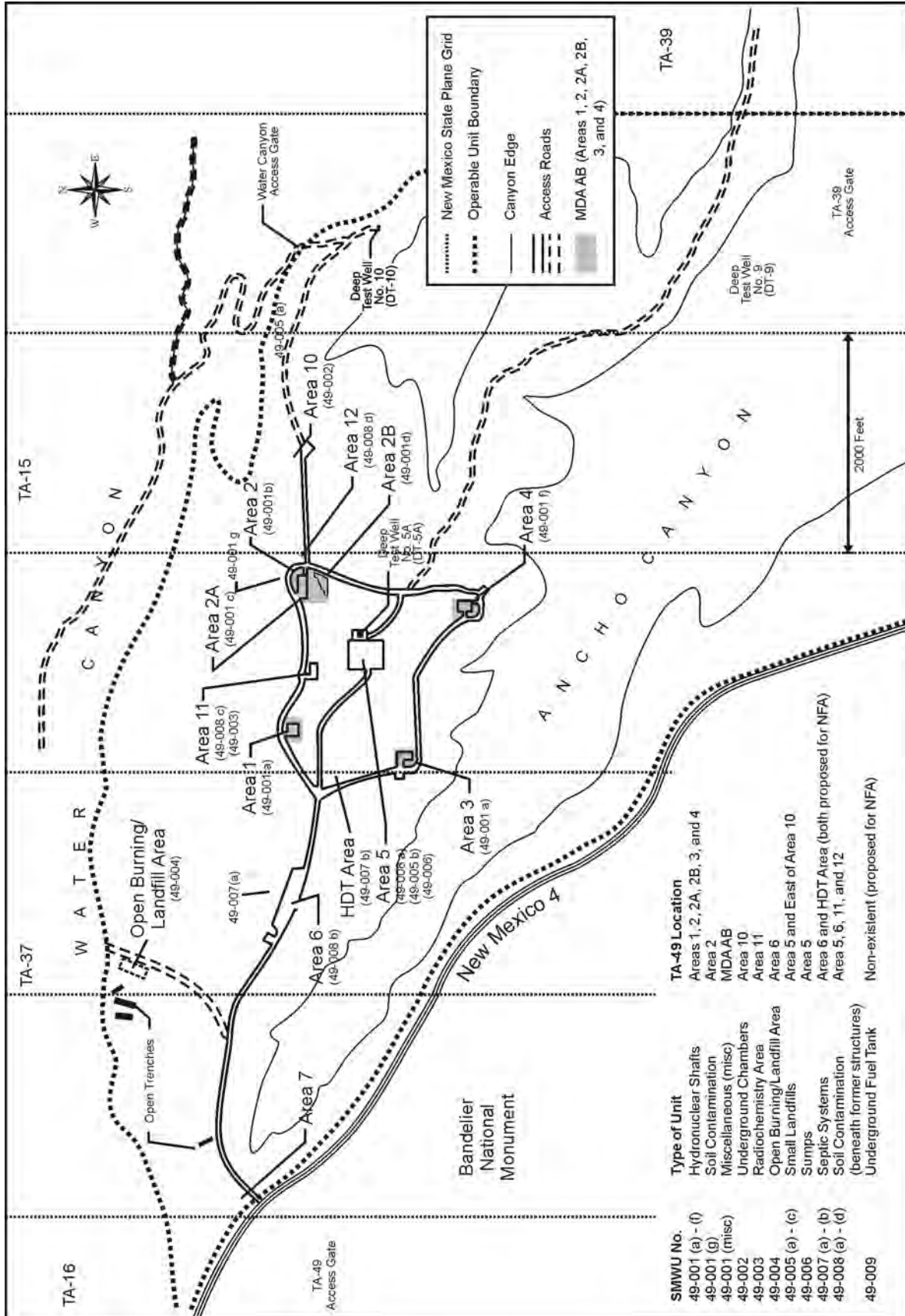


Figure I-12 Technical Area 49 Shaft Areas and Other Solid Waste Management Units

Before the experiments began, deep test wells were drilled into the main aquifer to determine the thickness of the tuff and volcanic sediments, hydrologic characteristics of the main aquifer, and presence of perched water (none was found). Two other deep boreholes were drilled that did not penetrate the aquifer. Four boreholes were drilled to depths from 300 to 500 feet (91 to 152 meters) to map the geologic and hydrologic characteristics of the underlying tuff (Core Holes 1 through 4). These holes are used for subsurface monitoring. A large but unquantified volume of drilling fluid was lost in Core Hole 2. Perhaps several million gallons of fluids were also lost in deep test well DT-5A below a level of 285 feet (87 meters) (LANL 1992b).

Before the underground experiments were conducted, containment experiments using “quarter-scale” quantities of high explosive occurred in Area 11. Subsequently, “full-scale” containment experiments occurred in Areas 1, 2, 3, and 4 using much larger quantities of high explosive than those in ensuing experiments (LANL 1992b).²⁰

Experimental holes in Areas 1, 2, 3, and 4 were spaced at 25-foot (7.6-meter) intervals on 100-foot (30-meter) square grid patterns. Areas 2A and 2B have irregular shapes. Experimental holes were typically 6 feet (1.8 meters) in diameter and ranged in depth from 31 to 142 feet (9.4 to 43 meters). Experimental holes were not drilled at all grid locations. Some of the holes were backfilled without further use and some were used to bury contaminated debris (LANL 1992b).

Associated with many experimental holes were small-diameter holes containing pipes leading from the shafts to steel boxes near the ground surface. The boxes collected samples of radioactive particles entrained in explosive gases. Recovery of sample collection devices from the boxes occasionally caused localized surface contamination that was cleaned to field detection limits or covered with soil. Pipes connected the boxes to large-diameter gas expansion holes. Each gas expansion hole served several experimental holes (LANL 1992b).

Researchers typically placed an experimental configuration in the bottom of a hole, installed instrument cables leading to the surface, and backfilled the hole with sand and crushed tuff. The down-hole package usually included substantial amounts of metallic lead. After completing measurements and sample collection, researchers severed the cables and backfilled hole subsidence. Holes containing special nuclear material were capped with concrete. The steel sampling boxes were usually filled with concrete and left in place. Researchers usually disconnected the sampling pipes from the sampling box and expansion hole and then reused or buried them in pipe dump holes, 3 feet (0.9 meters) in diameter by 30 feet (9.1 meters) deep, around the experimental area. At least four dump holes were drilled in Area 2B. Similar holes may exist in other areas (LANL 1992b).

Large concrete shields were used to minimize radiation exposure from a pulsing neutron source. The shields may have been activated with short-lived radionuclides. Monitoring with routine field instrumentation has found no detectable levels of surface contamination. Approximately 10 of these shields remain (LANL 1992b).

²⁰ *Containment experiments characterized the extent to which the detonations would fracture the tuff in the vicinity of the detonation points (LANL 1992b).*

The most significant contamination incident occurred in 1960 during the drilling of Hole 2-M in Area 2. After contamination was found, equipment that could not be decontaminated, or was of little value was placed in Hole 2-M along with contaminated surface soil. Other contaminated items were disposed of (LANL 1992b).

In January 1961, all open holes were filled with sand and crushed tuff, and the surface of Area 2 was capped with compacted clay and gravel. Historical estimates of the fill thickness in Area 2 range from 1 to 6 feet (0.3 to 1.8 meters), and a field inspection suggested a maximum fill thickness of 6 feet (1.8 meters). The cap was extended 12.5 feet (3.8 meters) beyond the outermost shafts and, in September 1961, paved with asphalt. Near-surface contamination was left beneath the asphalt. In 1977, the La Mesa forest fire burned over most of TA-49, destroying essentially all remaining combustible structures at the site (LANL 1992b).

In March 1975, collapse of asphalt over backfilled Hole 2-M left a hole 6 by 3 by 4 feet deep (1.8 by 0.9 by 1.2 meters deep) in the asphalt and underlying fill. This opening may have caused the 50 feet (15 meters) of standing water seen in 1975 in Core Hole 2. In September 1976, the opening over Hole 2-M was filled and the pad covering Area 2 was repaved with additional asphalt. Samples of water bailed from Core Hole 2 in 1977 and 1978 showed plutonium-239 in concentrations of 1.7 to 3.1 picocuries per gram, indicating that water in Core Hole 2 had contacted contamination beneath Area 2. The contaminated water presumably moved through fractures to the Core Hole 2 borehole and traveled down the annular spacing between the casing and the borehole. Alternatively, the enhanced infiltration caused by the collapsed hole created saturated soil conditions that extended laterally to the Core Hole 2 borehole and then traveled down the annular spacing between the casing and the borehole.

About 150 feet (46 meters) of standing water was measured in Core Hole 2 on several occasions in 1979 and 1980. Water from several levels was bailed from Core Hole 2 and plutonium was found in concentrations of from 0.1 to 5.5 picocuries per liter in filtered water samples, and from 0.54 to 0.72 picocuries per gram in suspended sediment samples. Core Hole 2 was bailed dry in June 1980 and from 1980 through 1987, Core Holes 1 through 4 were checked annually for standing water. No standing water was found. In 1981, the upper 2 feet (0.6 meters) of sand in the sand-filled shafts in Areas 2A and 2B was replaced with concrete. In May 1991, when vegetation was seen growing through cracks in the asphalt, Core Hole 2 contained 100 feet (30 meters) of standing water. In November 1991, cracks in the asphalt were resealed, and through the summer and fall of 1991 and spring of 1992, the water level in Core Hole 2 was measured on about a monthly basis. The water level during this time remained fairly stable. In December 1991, a transducer was installed in Core Hole 2 for continuous monitoring of the water level, which remained stable through April 1992. This water level stability suggested that the response to the summer 1991 rainfall and spring 1992 snowmelt was sluggish. Water analyses for a bailed sample from Core Hole 2 in May 1991 showed low but measurable concentrations of plutonium (LANL 1992b).

In 1998 and 1999, LANL performed an interim action at Areas 2, 2A, and 2B to: (1) plug and abandon Core Hole 2 and two other boreholes; (2) remove asphalt from Area 2; (3) install an evapotranspiration cover consisting of a layer of clean, crushed tuff, topsoil, shallow-rooted grass, and gravel for erosion protection; (4) cover part of the site and vicinity with a biointrusion barrier; (5) install a silt fence surrounding the new evapotranspiration cover; and (6) install a

run-on diversion channel (LANL 1998a, 1999a, 1999c). In February 2000, a moisture monitoring system was installed to monitor the new evapotranspiration cover at Area 2. Moisture monitoring continues as required by the Consent Order.

In May 2000, the Cerro Grande forest fire burned the western and northern edges of TA-49, but did not burn vegetation or structures at MDA AB or Area 11.

Area 5. As the main control area, Area 5 contained several structures that were removed or destroyed between 1961 and 1984, including the tower. Other structures were destroyed in June 1977 by the La Mesa forest fire (LANL 1992b). Some of the debris collected during the 1984 cleanup of Area 5 was likely disposed of in a pit 10 by 10 by 10 feet deep (3 by 3 by 3 meters deep) in Area 5 (SWMU 49-005(b)) (LANL 2005c).

Area 6. Area 6 occupies a 150- by 700-foot (46- by 213-meter) area. Area 6 included storage and office structures, although all structures were removed by 1977. In addition, a 400-square-foot (37-square-meter) “boneyard” stored lumber, fencing, and steel. Some materials may have been radioactively contaminated. AOC 49-008(b) consists of contaminated surface soil (LANL 2005c).

The landfill in Area 6 (SWMU 49-004) was used from late 1959 to mid-1961 to burn construction wastes and to bury uncontaminated residues. The landfill was reopened in 1971 and 1984. A trench 30 by 100 by 15 feet deep (9.1 by 30 by 4.5 meters deep) was dug for burial of uncontaminated debris. Assessments of surface contamination in the landfill have found transuranic isotopes as well as lead and beryllium. A 1991 geophysical survey indicated a landfill surface area of 35 by 200 feet (11 by 61 meters). The survey found several magnetic and electromagnetic anomalies. The survey suggested that the buried objects were covered by 4 feet (1.2 meters) of overburden (LANL 1992b).

Area 10. Used for calibration tests, Area 10 contains an inactive underground experimental chamber and two shafts (AOC 49-002), each 6 to 7 feet (1.8 to 2.1 meters) in diameter and 64 feet (20 meters) deep and connected at the bottom by a tunnel. One shaft contains an elevator. In the other shaft, a pulsed neutron source irradiated calibration samples placed within a 14-foot (4.3 meter-diameter) by 10-foot high (3.0-meter-high) room lined with reinforced concrete faced with steel plate. A hydraulic lift platform at the bottom of the calibration room connects to a hydraulic oil reservoir at the surface. A concrete pad at the tops of both shafts provides a foundation for the elevator building and shielding wall (LANL 2005c).

East of Area 10 is an inactive landfill (SWMU 49-005(a)). The landfill is 50 to 100 feet (15 to 30 meters) northeast of the Area 10 experimental chamber and shafts. The landfill was built in 1984 as a disposal area for debris from the 1984 general surface cleanup of TA-49. The wastes were primarily wood and small pieces of metal (LANL 2005c).

Area 11. Area 11 is a 220- by 300-foot (67- by 91-meter) area, 700 feet (213 meters) west of the main MDA AB shafts, where radiochemistry and small-scale containment experiments took place (LANL 2005c). Containment experiments took place at the bottoms of thirteen 10-inch (25-centimeter-diameter) by 12-foot-deep (3.7-meter-deep) vertical holes encased in steel and backfilled with sand. Some of the shots used irradiated uranium-238 as a tracer. A maximum of

10.5 grams (0.4 ounces) of uranium was used, and the irradiated samples contained microcurie levels of neptunium-239. Some holes may have contained lead and some holes were partially backfilled with concrete. Ten-inch-diameter (25-centimeter-diameter) casing from two capped holes extends above the ground surface (LANL 1992b).

Area 12. Area 12 historically featured confinement experiments where high explosive was detonated in sealed metal “bottles” (up to 5 feet [1.5 meters] in diameter by 16 feet [4.9 meters] long) placed in a shaft 30 feet (9.1 meters) deep. The Bottle House, one of two remaining surface structures, surrounded the shaft. Roughly 26 experiments used a few kilograms of uranium-238. Six used a few microcuries of irradiated uranium tracer. Area 12 then supported operations at the nearby Cable Pull Test Facility, built in the early 1960s. The Bottle House shaft was backfilled with crushed tuff (LANL 1992b).

Waste Inventory

Areas 1, 2, 2A, 2B, 3, and 4. Inventories of plutonium and uranium in each of the experimental areas (as of 1992) are summarized in **Table I–10**. The experimental areas may also contain small quantities of fission products (less than 10 millicuries) and ingrown americium-241 (about 0.33 pounds [0.15 kilograms] in 1992). The experimental shafts contain approximately 24 pounds (11 kilograms) of beryllium and possibly more than 198,000 pounds (90,000 kilograms) of lead (LANL 1992b).

Table I–10 Material Disposal Area AB Principal Radionuclides Inventories

| <i>MDA AB Area</i> | <i>SWMU Number</i> ^a | <i>Plutonium</i> ^b (kilograms) | <i>Uranium-235</i> (kilograms) | <i>Uranium-238</i> (kilograms) |
|--------------------|---------------------------------|--|-----------------------------------|-----------------------------------|
| Area 1 | 49-001(a) | 1.06 | 0.00 | 62.3 |
| Area 2 | 49-001(b) | 12.62 | 47.4 | 52.5 |
| Area 2A | 49-001(c) | 3.75 | 9.8 | 10.6 |
| Area 2B | 49-001(d) | 5.67 | 6.4 | 14.7 |
| Area 3 | 49-001(e) | 0.00 | 0.005 | 0.030 |
| Area 4 | 49-001(f) | 17.04 | 29.4 | 29.0 |
| Total | | 40.14 | 93.0 | 169.1 |

MDA = material disposal area, SWMU = solid waste management unit.

^a SWMU 49-001(g) comprises surface contamination at the experimental areas.

^b Plutonium isotopic composition in weight-percent: plutonium-239 (93.5 - 94.2 percent); plutonium-240 (5.30 - 6.05 percent); plutonium-241 (0.458 - 0.563 percent). Plutonium-241 decays to americium-241.

Note: To convert kilograms to pounds, multiply by 2.2046.

Source: LANL 1992b.

The Hole 2-M incident probably caused the radionuclides seen in surface soils around the Area 2 pad and just outside the Area 2 exclusionary fence (SWMU 49-001(g)). About 0.8 acre (0.3 hectare) may be contaminated with plutonium and americium (LANL 1992b).

Area 5. Only small amounts of hazardous or radioactive materials could have been released to soil. A few hundred gallons of photographic solutions may have been released to sumps or nearby soil (LANL 1992b).

Area 6. The landfill may contain lead or beryllium but probably contains little radioactive material (LANL 2002g).

Area 10. Materials used in calibration tests included uranium, beryllium, and lead shielding. Milligram quantities of enriched uranium were occasionally released, albeit generally recovered. The pulsed neutron source may have activated surrounding soils and structures, but activation products should be significantly decayed. The hydraulic oil in the lift system was not reported to contain PCBs. After 1961, hazardous materials were not used. Materials disposed of in the nearby landfill (SWMU 49-005(a)) were mainly wood and metal (LANL 2005c).

Area 11. Elevated levels of radioactivity have been measured near the east end of the former radiochemistry building. Small levels of radioactivity may be in the vicinity of the leach field. A 1991 geophysical survey suggested near-surface piping and electrically conductive areas possibly related to subsurface chemical contamination or elevated moisture levels. Buried metal was found in the small-shot area (LANL 1992b).

Area 12. Surface contaminants are at low levels and have discontinuous distributions (LANL 1992b).

Current Configuration

Areas 1, 2, 2A, 2B, 3, and 4. All six areas are covered with native soil and vegetation. Few aboveground structures remain. All areas except Area 3 are fenced. Aboveground pipes exist in Area 3, as do exposed patches of concrete. Piping to a gas expansion hole remains in Area 4 (LANL 1992b). Pipe interiors are contaminated (LANL 1992b).

Depths of MDA AB test and support shafts are shown in **Table I-11**. The shafts include shot holes, pipe dump holes, gas expression holes, and unused holes (either backfilled or proposed, but not excavated). This table does not list all possible subsurface contamination such as pipe dump holes, buried pipes, and sampling boxes. The individual down-hole assemblies in the experimental shafts weighed as much as 8 tons (7.3 metric tons) and consisted of cable, steel, iron, aluminum, and other structural materials (LANL 1992b).

A crushed-tuff evapotranspiration cover has been installed at Areas 2, 2A, and 2B. During February and March 2000, the LANL environmental restoration project installed three new shallow neutron access holes and two time-domain-reflectometry arrays in the cover and initiated monthly moisture monitoring to track the cover performance (LANL 2000a).

Area 5. The only surface structures now in Area 5 are the observation well enclosure and the concrete pads from the former transformer station and the photographic tower. Small amounts of metallic debris and lead bricks remain (LANL 1992b).

Area 6. A 1991 geophysical survey showed the footprint of the landfill trench to be 35 by 330 feet (11 by 101 meters). The RFI Work Plan describes four open trenches that are west and southwest of the landfill trench (SWMU 49-004). These previously undocumented trenches may predate activities at TA-49. The trenches are 10 feet wide by 4 to 6 feet deep by 50 to 100 feet long (3.0 by 1.2 to 1.8 by 15 to 30 meters). One trench had been backfilled and one passes through prehistoric ruins (LANL 2005c). Area 6 currently supports microwave research.

Table I–11 Material Disposal Area AB Test and Support Shaft Depths

| <i>Area 1</i> | <i>Area 2</i> | <i>Area 2A</i> | <i>Area 2B</i> | <i>Area 3</i> | <i>Area 4</i> |
|---------------------|---------------|----------------|----------------|---------------|---------------|
| 1-A 58 ^a | 2-A 54 | 2A-E 58 | 2B-A 58 | 3-A 87 | 4-A 88 |
| 1-B 31 | 2-B 54 | 2A-J 58 | 2B-B 58 | 3-B 57 | 4-B 101 |
| 1-C 51 | 2-C 30 | 2A-O 58 | 2B-C 57 | 3-C 88 | 4-C 58 |
| 1-D 31 | 2-D 57 | 2A-T 58 | 2B-D | 3-D 88 | 4-D 108 |
| 1-E 50 | 2-E 53 | 2A-Y 58 | 2B-E | 3-E 88 | 4-E 78 |
| 1-F 50 | 2-F 57 | 2A-Z 57 | 2B-F | 3-F 88 | 4-F 78 |
| 1-G 31 | 2-G | – | 2B-G | 3-G 142 | 4-G |
| 1-H | 2-H 57 | – | 2B-H 58 | 3-H | 4-H 88 |
| 1-I 31 | 2-I 57 | – | 2B-I | 3-I | 4-I |
| 1-J 58 | 2-J 57 | – | 2B-J 57 | 3-J 142 | 4-J 88 |
| 1-K 85 | 2-K 68 | – | 2B-K | 3-K 142 | 4-K 88 |
| 1-L 31 | 2-L 57 | – | 2B-L 58 | 3-L | 4-L |
| 1-M 31 | 2-M 58 | – | 2B-M | 3-M | 4-M 88 |
| 1-N 31 | 2-N 57 | – | 2B-N | 3-N | 4-N |
| 1-O 85 | 2-O 57 | – | 2B-O | 3-O | 4-O 84 |
| 1-P 58 | 2-P 57 | – | 2B-P | 3-P | 4-P 88 |
| 1-Q 31 | 2-Q 57 | – | 2B-Q | 3-Q | 4-Q |
| 1-R 31 | 2-R | – | 2B-R | 3-R | 4-R 78 |
| 1-S 31 | 2-S 57 | – | 2B-S | 3-S | 4-S |
| 1-T 58 | 2-T 57 | – | 2B-T 78 | 3-T | 4-T 78 |
| 1-U 58 | 2-U 52 | – | 2B-U | 3-U 88 | 4-U 108 |
| 1-V | 2-V 57 | – | 2B-V 58 | 3-V 88 | 4-V |
| 1-W 58 | 2-W 57 | – | 2B-W | 3-W | 4-W 78 |
| 1-X | 2-X 57 | – | 2B-X 78 | 3-X | 4-X |
| 1-Y 80 | 2-Y 78 | – | 2B-Y 58 | 3-Y 108 | 4-Y 78 |
| – | – | – | 2B-Z 60 | – | 4-Z 70 |

^a Notation: The first set (1-A) identifies the shaft. The second set is the nominal shaft depth in feet.
 Note: To convert feet to meters, multiply by 0.3048.

Area 10. The elevator building has been removed. The concrete pad remains, as do concrete radiation shields at the top of the calibration shaft. The entrances to both shafts are covered with concrete blocks. The elevator shaft is open and the calibration shaft has been backfilled. The hydraulic oil reservoir has been removed (LANL 2005c).

Area 11. In 1970 and 1971, radiochemistry structures were decontaminated, demolished, and removed. The subsurface leach field and drain line remain (LANL 1992b).

Area 12. All structures have been removed except for the Bottle House and the Cable Pull Test Facility. Current use of Area 12 is limited to air monitoring and occasional use of portable microwave experimental equipment in the roadway between Areas 10 and 12 (LANL 1992b).

Site Investigations. Site characterization and monitoring began in 1959. Early studies analyzed information from boreholes drilled in and near the experimental areas and from the three observation holes. A 1987 survey found surface contamination at Areas 1, 3, and 4 and in the northeast corner of the Area 2 pad. The contamination was apparently caused by exhumation of contaminated soil by gophers. A 1991 geophysical study in Area 4 was limited by interference from the chain-link perimeter fence and from buried metallic debris. Additional site investigations have been conducted for Areas 5, 6, 11, and 12 up to the early 1990s as summarized in the RFI Work Plan for Operable Unit 1144 (LANL 1992b).

More recent site investigations are summarized below.

Areas 1, 2, 2A, 2B, 3, and 4. The Phase I RFIs in 1993 and 1994 included installation and sampling of four shallow and three deep boreholes and collection of surface samples at Area 2. In 1999, an interim measure and best management practices program was conducted at Areas 2, 2A, and 2B and the contaminated area northeast of Area 2 (LANL 2005c).

Area 5. A 1995 Phase I RFI was conducted at AOC 49-008(a). The RFI report recommended no further action, although it indicated that the site would be evaluated for ecological risks. In 1997, EPA Region 6 nonconcurred with the recommendation and recommended additional characterization. During 1995, a Phase I RFI was conducted at the Area 5 sump (SWMU 49-006). Based on a human health risk-based screening assessment, the RFI report recommended no further action, although it indicated that the site would be evaluated for ecological risks. EPA concurred with the recommendation. In 2002, a Supplemental Sampling and Analysis Plan for Areas 5, 6, and 10 was prepared (LANL 2005c).

Area 6. In 1995, a Phase I RFI was conducted at the open burning/landfill area (SWMU 49-004). The RFI report recommended no further action, although it indicated that the site would be evaluated for ecological risks. EPA Region 6 nonconcurred with the recommendation and called for Phase II sampling. In 1996, a Phase I RFI was conducted for AOC 49-008(b) (LANL 2005c).

Area 10. In 1995, a Phase I RFI was conducted at the experimental chamber and shaft (AOC 49-002). The RFI report recommended no further action, although it indicated that the site would be evaluated for ecological risks. EPA Region 6 concurred with the recommendation (LANL 2005c). Regarding the nearby landfill (SWMU 49-005(a)), a Phase I RFI was conducted during 1995 and 1996 (LANL 2005c).

Area 11. A 1995 Phase I RFI for the area of soil contamination (AOC 49-008(c)) performed radiation surveys and collected surface and subsurface samples. No further action was recommended, although the RFI report indicated that the site would be evaluated for ecological risks. EPA Region 6 nonconcurred with the recommendation (LANL 2005c). Regarding the leach field (SWMU 49-003), 13 shallow subsurface samples were collected during a 1995 Phase I RFI (LANL 2005c).

Area 12. In 1995, Phase I RFI sampling found radiation levels above background values at four survey points around the Bottle House. Copper and silver were found above background values in soil samples. Radionuclides were found above background values and uranium was present above screening action levels. Five organic chemicals were found. In 1997, a voluntary

corrective action was conducted to remove the soils around the Bottle House. Additional soil removal occurred in 1998 (LANL 2005c).

I.2.5.4 Technical Area 50: Material Disposal Area C

TA-50 is on Mesita del Buey. TA-50 was developed for waste management activities because of limitations in disposal capacity in other areas, because of a plan to develop LANL to the south, and because of the 1948 fire in MDA B (see Section I.2.5.2.2). TA-50 includes inactive MDA C (**Figure I-13**) (DOE 1999a, LANL 1999b, 2006k).

History of MDA C. MDA C is adjacent to waste management facilities to the north, while Ten Site Canyon is to the northeast.

MDA C was used from 1948 to 1965. In 1963, the Radioactive Liquid Waste Treatment Facility (Building 50-1) was built to the north of MDA C. Additional facilities near MDA C include the Waste Characterization, Reduction, and Repackaging Facility (Building 50-69), built in 1983.²¹ Liquid wastes from these facilities are piped to the Radioactive Liquid Waste Treatment Facility (LANL 1992c).

MDA C (SWMU 50-009) comprises seven pits, including one chemical pit, and 108 shafts. The disposal units are within a site covering 11.8 acres (4.8 hectares) (LANL 1999b). All pits and shafts were dug into the overlying soil and the Tshirege Member of the Bandelier Tuff (LANL 2003k). The MDA C disposal unit dimensions and periods of operation are shown in **Table I-12** (LANL 2003k). Except for 10 shafts, all disposal units are unlined. The shafts were placed in three groups. The first group of 12 shafts was dug between and parallel to Pits 4 and 5; the second group of 55 shafts was dug between and parallel to Pits 1 and 3; the third group of 40 shafts was dug in two lines perpendicular to the western ends of Pits 1 through 5. The strontium-90 disposal shaft was dug at the southwest corner of Pit 1 (LANL 2003k). (Shaft designation numbers do not reflect their sequence of use.)

Limited disposals may have been made following 1966. The last mention of MDA C in quarterly and annual waste disposal reports was in 1968. The last shaft (Shaft 89) was plugged on April 8, 1974 (Rogers 1977).

The pits were filled with wastes arriving in a variety of containers (Rogers 1977). Routine radioactive trash consisted of cardboard boxes, 5-mil plastic bags from chemistry laboratories, and 55-gallon (0.21-cubic-meter) barrels of sludge from wastewater treatment plants in TA-21 and TA-45 (LANL 2003k). Nonroutine waste included debris from the demolition of the Bayo Site and TA-1, classified materials, and tuballoy (a uranium alloy) chips (LANL 2003k). Hazardous constituents and uncontaminated classified material were buried with radioactive waste. A 1959 memorandum complains that much of the waste in one of the pits (probably Pit 6) was outdated technical badges and safety film. Chemicals were commonly burned in the chemical pit (Rogers 1977).

²¹ Not shown in Figure I-13 is the Radioactive Materials Research, Operations, and Demonstration Facility (Building 50-37), built in 1975. The facility is now called the Actinide Research and Teaching Integration Center.

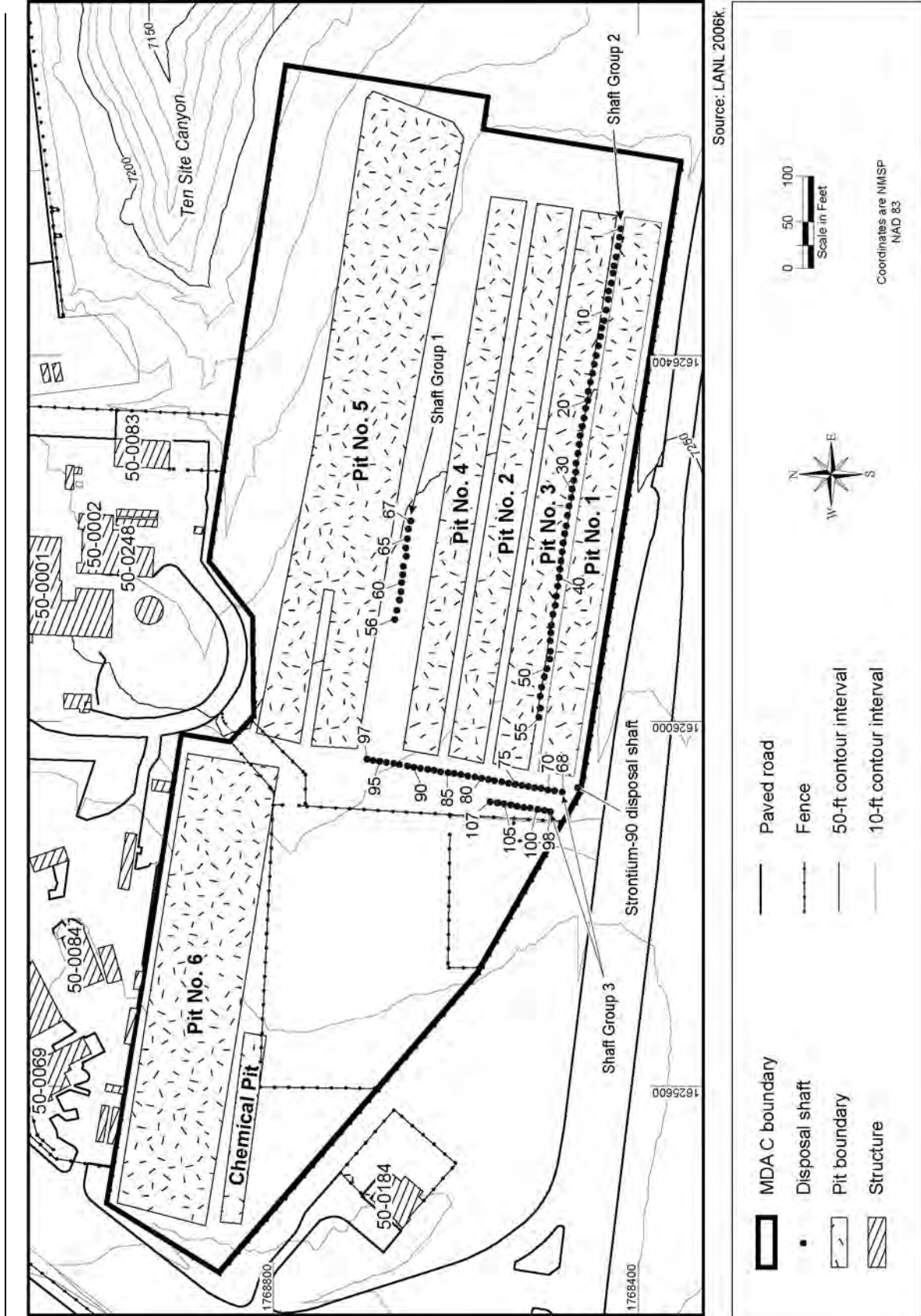


Figure I-13 Locations of Pits and Shafts at Material Disposal Area C

Table I–12 Approximate Dimensions of Material Disposal Area C Disposal Units

| <i>Disposal Unit</i> | <i>Dimensions (feet)^a</i> | <i>Period of Operation</i> |
|---|--------------------------------------|----------------------------|
| Pit 1 | 610 × 40 × 25 | 1948 to 1951 |
| Pit 2 | 610 × 40 × 25 | 1950 to 1951 |
| Pit 3 | 610 × 40 × 25 | 1951 to 1953 |
| Pit 4 | 610 × 40 × 25 | 1951 to 1955 |
| Pit 5 | 705 × 110 × 18 | 1953 to 1959 |
| Pit 6 | 505 × 100 × 25 | 1956 to 1959 |
| Chemical Pit | 180 × 25 × 12 | 1960 to 1964 |
| Shaft Group 1 (12 shafts; numbers 56-67) | 2 × 10 | 1959 |
| Shaft Group 2 (55 shafts; numbers 1-55) | 2 × 15 | 1959 to 1967 |
| Shaft Group 3 (40 shafts; numbers 68-107) | 1-2 × 20-25 ^b | 1962 to 1966 |
| Shaft 108 (strontium-90 disposal shaft) | Unknown | 1950s or 1960s |

^a Pit dimensions are length by width by depth; shaft dimensions are diameter by depth. Dimensions are approximate.

^b Shafts 98-107 are 1 foot in diameter and are lined with 12-inch thick concrete. Shafts 68-97 are 2 feet in diameter and are unlined.

Note: To convert feet to meters, multiply by 0.3048.

Source: LANL 2003k.

At first, the waste was covered once a week to reduce the danger of fire, but operating practices were changed in 1957. Wastes were then backfilled when a single layer of waste covered about half the width of the pit, reducing the risk of fire as well as the amount of waste that could be placed in a pit (Rogers 1977). The MDA C Investigation Work Plan references a 1959 memorandum stating that Pit 6 received 10,000 cubic yards (7,645 cubic meters) of waste and 24,000 cubic yards (18,300 cubic meters) of fill, for an approximate ratio of 2.5 cubic yards (1.9 cubic meters) of fill to 1 cubic yard (0.76 cubic meters) of waste (LANL 2003k).

The shafts were used for disposal of “beta-gamma waste,” mostly from the Chemical Metallurgy Research Building at TA-3 (Rogers 1977, LANL 2003k). Before February 1958, when the first shafts were drilled, beta-gamma waste was taken to a disposal pit where the waste was placed in a hole dug into the bottom of the pit and covered. After the shafts were opened, containers of waste were transported to the disposal area in lead transfer casks and dropped into the disposal shafts. By 1967, filled disposal shafts were routinely topped with concrete (Rogers 1977).

Five fires occurred at MDA C between 1950 and 1958. The first, in November 1950, involved material that had been placed in one of the pits. The second, in June 1952, involved one box as it was being unloaded. The third, in March 1953, involved containers that had been placed in the pit prior to being covered with backfill. The fourth, in April 1953, involved a single, smoking box from Sigma Building. The final fire, in November 1958 involved two boxes; the suspected cause was the presence of a volatile, flammable chemical such as acetone (Rogers 1977).

In 1974, most of the MDA C surface was covered with crushed tuff and fill, and the new surface was recontoured and seeded with grass. Localized surface subsidence on the north boundary of Pit 6 was seen in 2002. The subsidence produced a hole along an asphalt drainage carrying runoff to Ten Site Canyon and may have promoted infiltration of stormwater into Pit 6. The subsidence was mitigated (LANL 2003k).

Waste Inventory. Table I-13 lists the wastes that were placed into each of the pits and three shaft groups, based—except for the chemical pit—on Los Alamos Scientific Laboratory logbooks (LANL 2003k). No information is available for the strontium-90 shaft.

Table I-13 Los Alamos Scientific Laboratory Logbook Citations of Wastes Placed in Pits and Shafts

| | |
|-------------------------------|---|
| Pit 1 | Trichloroethylene, boron, sulfuric acid, graphite, medical laboratory solutions, contaminated materials and trash, tritium, americium-241, uranium, classified material, plutonium, cyanide, radium-226, acids, lead, and waste oil. |
| Pit 2 | Trichloroethylene and contaminated materials and trash, boron, tritium, americium-241, uranium, sulfuric acid, biological waste, graphite, classified material, plutonium, cyanide, mercury, radium-226, acids, lead, and waste oil. |
| Pit 3 | Mercury teplers, tritium-contaminated glassware, cyanide solutions, contaminated materials and trash, trichloroethylene, boron, americium-241, uranium, sulfuric acid, biological waste, graphite, classified material, plutonium, radium-226, acids, lead, waste oil, and beryllium. |
| Pit 4 | Tritium-contaminated glassware and boxes, tritium contaminated urine samples, mercury teplers, actinium-227, vials of radium-226, cyanide and cyanide solutions, a 5-gallon can of actinium waste, empty bottles, contaminated materials and trash, trichloroethylene; boron, americium-241, uranium, sulfuric acid, biological waste, graphite, classified material, plutonium, acids, lead, waste oil, silver, and beryllium. |
| Pit 5 | Batteries (acids and lead), a 5-gallon can of actinium-227 waste, lead bricks, vials of radium-226, zirconium shavings, cyanide and cyanide solutions, radionuclide-contaminated boxes and urine samples, contaminated materials and trash, trichloroethylene, boron, americium-241, uranium, sulfuric acid, biological waste; graphite, classified material, and plutonium. |
| Pit 6 | Radionuclide-contaminated oil, tritium-contaminated oil, copper sheets, cobalt chips, bottles of cadmium-boron tungstate, tritium-contaminated boxes and cans, a can of oil, about 100 curies of cobalt-60, a lanthanum source, 10 bottles of platinum chloride, beryllium chips, carbon-14-contaminated graphite, a plutonium slug, contaminated materials and trash, classified material, mercury, actinium-227, radium-226, acids, and lead. |
| Chemical Pit | No logbook entries were made. A 1964 memorandum provides this summary: "...A variety of chemicals, pyrophoric metals, hydrides and powders, sealed vessels containing sodium-potassium alloy or compressed gasses, and equipment not suitable for salvage, public dump or the contaminated dump have been placed in the pit. No high explosives have ever been disposed of in this pit. Natural uranium powders and hydrides have been disposed of in this pit. Inadvertently, some plutonium-contaminated objects were placed in the pit but have long since been covered. Because of the uranium disposed it should be assumed that the pit is mildly alpha contaminated" (Rogers 1977). |
| Shaft Group 1 (Shafts 56-67) | Barium, tritium, radium, lanthanum-140, strontium-89 and -90, tantalum, cerium waste, two cerium sources, fission products, one lanthanum-140 static source, phosphoric acid, depleted uranium, a charcoal trap, and polonium-beryllium-fluorine compounds. |
| Shaft Group 2 (Shafts 1-55) | Barium-140, lanthanum-140, fission products from the Omega reactor, uranyl phosphate, graphite slugs, a cobalt-60 capsule, radioactive graphite, radioactive tantalum, 1 gram of irradiated plutonium, thallium, irradiated uranium, graphite, lead-beryllium sources, thorium, cesium, strontium, plasma thermocouples, fuel elements (rods), cobalt-60 slugs and sources, sulfuric acid solution, zirconium carbide, a copper sphere, two "rabbit" tubes ^a of beryllium, reactor seals, alpha emitters in solution, acid solutions, actinium components, various uranium isotopes, depleted uranium, cerium-141, yttrium, silver-110, sodium-22, cesium-137, cesium-144, plutonium waste, oralloy (enriched uranium from Oak Ridge), benzene, isopropyl alcohol, neptunium-237, contaminated materials and trash, americium-241, biological waste, classified material, radium-226, lead, silver, and "induced activity" (activation products, usually from a linear accelerator). |
| Shaft Group 3 (Shafts 68-107) | Plutonium-contaminated trash, fission products, aluminum sheets and tubes, acids, cesium-137, sodium, cobalt-60, antimony, lanthanum-140, cobalt-60 sources, polonium, beryllium, vacuum pump oil, empty glass bottles, graphite, plutonium, boron, fuel element end caps, thermocouples, acetone, uranium, zirconium carbide, zinc and aluminum residues, barium, irradiated tantalum, tuballoy (a uranium alloy), shell waste, yttrium-91, radioactive chemicals and organic solutions, hydrochloric acid waste, plutonium in ether solution, zinc and mercury solutions, depleted uranium chips, miscellaneous sources, oralloy solution, iridium-192, tantalum, indium-114, animal tissues, solvents, a LAMPRE (Los Alamos Molten Plutonium Reactor Experiment) rod assembly, waste oil, detonator components, NRX (Navy experiment) reactor parts, trinitrotoluene (TNT) element samples, americium-242, aluminum-105 (sic), zinc-65, neptunium-237, contaminated materials and trash, americium-241, classified material, actinium-227, radium-226, lead, silver, strontium-90, and "induced activity." |

^a Rabbits are containers placed in a reactor neutron flux to irradiate the contents.

Note: To convert gallons to liters, multiply by 3.7854; grams to ounces, multiply by 0.03527.

Data are as stated in the source document.

Source: LANL 2003k.

Radionuclide inventories estimated for the pits and shafts, decay corrected to January 1989, are listed in **Table I–14** (LANL 1992c). These inventories are derived from information in (Rogers 1977). Table I–14 (LANL 1992c) does not list any citation for transuranic isotopes in the MDA C shafts, although a 1999 DOE database on buried transuranic waste (DOE 1999g) estimates 57 curies of plutonium-239 in MDA C shafts.

Table I–14 Material Disposal Area C Estimated Radionuclide Inventories as of January 1989

| <i>Disposal Unit</i> | <i>Radionuclide</i> | <i>Activity (curies)</i> |
|----------------------|----------------------------------|--------------------------|
| Pits | Uranium-234, -235, -236, -238 | 25 |
| | Plutonium-239 | 26 |
| | Americium-241 | 145 |
| | Total | 196 |
| Shafts | Tritium | 20,000 |
| | Sodium-22 | 0.58 |
| | Cobalt-60 | 2.4 |
| | Strontium-90/Yttrium-90 | 21 |
| | Radium-226 | 1 |
| | Uranium-233 | 5 |
| | Uranium-234, -235, -236, -238 | <0.1 |
| | Fission products ^a | 50 |
| | Activation products ^a | 200 |
| | Total | 20,280 |

^a Uncorrected because exact compositions are unknown.

Source: LANL 1992c.

Current Configuration. The topography slopes from west to northeast, becoming steeper across the northeast quadrant of the site toward Ten Site Canyon. The site is vegetated by grass established after the 1984 addition of fill and topsoil over the disposal units (LANL 2003k).

The area south of Pit 6 and west of Pits 1 through 6 is covered with asphalt, as is much of the ground north of the MDA not occupied by buildings. The MDA is fenced. Many of the buildings and structures north of MDA C are SWMUs. Underground utilities run along and outside the fence line (LANL 2003k), including a water line along Pajarito Road and a radioactive liquid waste line along the west half of the northern site boundary. A new pump house and effluent storage facility is being built 30 feet (9.1 meters) north of the MDA boundary between TA-50 and TA-35 (Stephens 2005).

Geophysical surveys were conducted in 1994, 2001, and 2002. All seven pits probably extend beyond the boundaries shown on historical maps. Pits 1 through 4 extends farther to the east, and Pit 6 possibly extends to the fence on the north side of MDA C.²² Shafts 98 through 107 were found to correlate with historical data. Neither the other two shaft fields nor the strontium-90 shaft were identified (LANL 2003k).

The 2001 geophysical survey found east-west trending conductivity anomalies that generally coincided with expected pit locations. No anomalies could be positively attributed to the shafts. The cover thicknesses over Pits 1 through 6 ranged from about 2.5 feet (0.8 meters) to about 8 feet (2.4 meters). The depth of cover over Shaft Groups 2 and 3, the western ends of Pits 1 through 4, and the chemical pit was less than 1 foot (0.3 meters)²³ (LANL 2003k).

Site Investigations. Radiation surveys of site soils and vegetation occurred from 1976 through 1984. Additional field surveys and laboratory analyses followed the 1984 placement of crushed tuff and cover material (LANL 1992c, 2003k). The Phase I RFI (1995 through 2003) sampled surface soil, subsurface tuff, and pore gas. A 2003 study obtained samples from 29 ant mounds and small-mammal burrow spoils and from 16 trees growing on the site. All trees were removed. The Phase I site investigations concluded (LANL 2003k):

- Historical releases of radionuclides to surface soils had been largely covered with crushed tuff. Elevated concentrations of americium-241 and isotopic plutonium in surface soils in the northeast area of MDA C were likely from releases from MDA C before placement of the crushed tuff in 1984.
- The only metals detected in concentrations above their respective background values in surface soil were lead and silver. There were sporadic detections of semivolatile organic compounds and Aroclor-1254 and -1260, but no defined pattern was found nor evidence for widespread release of organic chemicals.
- Specific metals (including barium, copper, and lead) and radionuclides (strontium-90 and americium-241) were found in tuff beneath the disposal pits. The extent of this subsurface contamination was not sufficiently defined.
- Subsurface pore gas contains tritium and volatile organic compounds (mainly trichloroethylene, tetrachloroethene, and 1,1,1-trichloroethane). The vertical and horizontal extent of contamination was not sufficiently defined.
- Surface flux of volatile organic compounds and near-surface tritium soil gas concentrations indicated localized areas where releases to the atmosphere were occurring.

²² The 1994 survey indicated that Pit 6 may possibly extend beyond the fence at the east end of the pit (LANL 2003a). However, a photograph confirms the proximity of the northern edge of Pit 6 to the north perimeter fence (Rogers 1977).

²³ A map showing the variable thickness of cover across MDA C is available in the Investigation Work Plan for MDA C (LANL 2003a) and in a survey of source materials for capping the MDAs (Stephens 2005).

Further work was proposed in the 2003 MDA C Investigative Work Plan to determine: (1) the extent of metals, cyanide, and radionuclide contamination in tuff beneath Pit 6; (2) the concentrations and spatial extent of volatile organic compounds and vapor phase tritium in the subsurface tuff; (3) the nature and extent of potential releases of metals, cyanide, and radionuclides beneath pits and shafts; (4) the extent of radionuclide contamination in surface soil on the eastern boundary of MDA C; (5) the presence of perchlorate, nitrate, dioxin, and furan in tuff; (6) the presence of perched groundwater beneath MDA C; and (7) information on hydrogeologic properties and fracture characteristics (LANL 2003k). The MDA C Investigation Report (LANL 2006k) was completed and submitted to NMED on December 6, 2006. Additional work is ongoing.

I.2.5.5 Technical Area 54: Material Disposal Areas G, H, and L

TA-54 is on Mesita del Buey, which spans the boundary of the Cañada del Buey and Pajarito Canyon Watersheds. The northern border is the boundary between LANL and the San Ildefonso Pueblo; its southeastern boundary borders White Rock (LANL 1999b). The primary function of TA-54 is management of radioactive and hazardous chemical wastes. It contains more than 100 structures (DOE 1999a). The facilities at TA-54 are grouped in different areas according to the types of waste managed (see **Figure I-14**). Areas and MDAs in TA-54 include:

- *Area G.* The current Area G footprint comprises a 63-acre (25.5-hectare) site used since 1957 (LANL 2005h). It includes MDA G, a site having numerous subsurface disposal pits and shafts that are the subject to Consent Order investigations, as well as active low-level radioactive waste disposal operations. It includes above- and belowground transuranic waste storage areas; a facility for decontaminating radioactive waste containers; compactors for transuranic and low-level radioactive waste; an administrative support building; and numerous other structures. Because of space and regulatory consideration, low-level waste disposal operations will be expanded into Zones 4 and 6 at Area G (64 *Federal Register* [FR] 50797); other waste management activities will be transferred to other LANL locations.
- *TA-54 West.* TA-54-West is the site of the Radioassay and Nondestructive Testing Facility, used to determine characteristics of containerized transuranic waste and to prepare the containers for shipment to WIPP.
- *Area L.* This 2.6-acre (1.1-hectare) area is LANL's chemical waste management area. Area L includes MDA L, a site formerly used for subsurface disposal of chemical wastes, and currently subject to Consent Order investigations.
- *MDA H.* This MDA consists of nine inactive shafts used until 1986 for disposal of classified radioactive wastes. The area is being remediated pursuant to the Consent Order.
- *MDA J.* This 2.65-acre (1.1-hectare) MDA was used from 1961 until 2001 for disposal of solid wastes. The six pits at MDA J are covered with clean fill and all four shafts are capped. An asbestos transfer station has been removed. MDA J has undergone closure under the New Mexico Solid Waste Act of 1990, and is under postclosure monitoring.

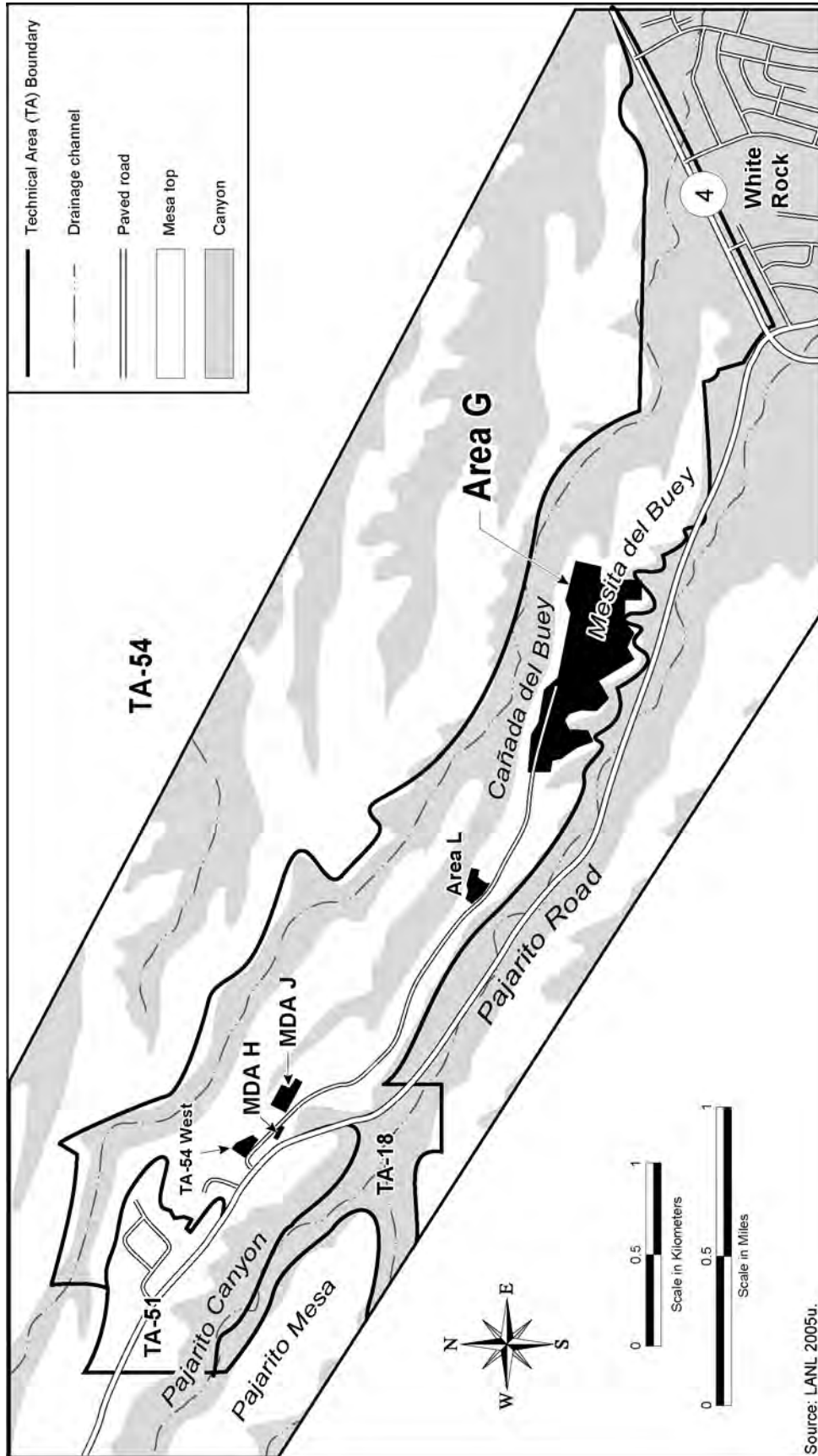


Figure I-14 Area and Material Disposal Area Locations of Technical Area 54

I.2.5.5.1 Material Disposal Area G

Within Area G, MDA G includes subsurface disposal units containing radionuclides and hazardous constituents under RCRA, and subsurface storage units for transuranic waste. The Investigation Work Plan for MDA G identified 32 pits, four trenches, and 194 shafts having depths ranging from 10 to 65 feet (3 to 20 meters) below the ground surface (LANL 2004c). **Figure I–15** shows existing waste areas within the existing Area G footprint (LANL 2005h).



Figure I–15 Waste Management Areas within the Existing Area G Footprint in Technical Area 54

History of MDA G. Disposal began during the 1950s. Up until the early 1970s, some of the waste disposed of at Area G contained transuranic isotopes in concentrations exceeding 10 nanocuries per gram, and some contained nonradioactive hazardous constituents. After DOE began retrievably storing wastes suspected of containing transuranic isotopes exceeding 10 nanocuries per gram, low-level radioactive waste disposed of in Area G contained significantly smaller quantities of transuranic isotopes,²⁴ but, until July 1986, still contained nonradioactive hazardous constituents (LANL 1997). Thereafter, disposal of mixed low-level radioactive waste was discontinued, but low-level radioactive waste and radioactively contaminated PCB waste continued to be disposed of in Area G (LANL 2004c). MDA G comprises those disposal units of Area G that are subject to corrective action under the Hazardous and Solid Waste Amendments to the Resource Conservation and Recovery Act.

²⁴ The transuranic limit for DOE disposal of low-level radioactive waste was revised in the early 1980s from 10 to 100 nanocuries per gram.

Tables I-15 and I-16 describe the dimensions, operational periods, and wastes placed into MDA G pits and trenches (LANL 2004c). **Table I-17** summarizes information about the shafts (LANL 1992a).²⁵ The trenches are used for retrievable storage of contact-handled transuranic waste. The shaft diameters range from 1 to 6 feet (0.3 to 1.8 meters) (LANL 2004c).

Table I-15 Material Disposal Area G Pits

| <i>Pit Number</i> | <i>Operational Period</i> | <i>Dimensions (feet) (length by width by depth)</i> | <i>Pit Volume^a (cubic yards)</i> | <i>Waste Volume^a (cubic yards)</i> | <i>Waste Description</i> |
|-------------------|---------------------------|---|---|---|---|
| 1 | 1/59-4/61 | 616 × 113 × 20 | 37,080 | 5,529 | Wing tanks from Kirtland Air Force Base, dry boxes, "normal trash." Pit used to burn combustibles. |
| 2 | 4/61-7/63 | 618 × 104 × 26 | 42,911 | 6,407 | Classified Bendix waste, 55-gallon drums, property numbers, D-38, hot dirt. |
| 3 | 6/63-3/66 | 655 × 115 × 33 | 56,759 | 9,473 | Misc. material, lumber, pipe, 55-gallon drums, D&D, D-38, Bendix classified waste, soil from TA-10/Bayo Canyon. |
| 4 | 1/66-12/67 | 600 × 110 × 34 | 44,950 | 8,212 | D&D, graphite, wooden boxes, D-38, 55-gallon drums, classified Bendix waste, property numbers. Burning trench along south wall of pit. |
| 5 | 1/67-3/74 | 600 × 100 × 29 | 41,258 | 6,624 | Scrap material, D&D, graphite hoppers, sludge drums (possibly aqueous solution from TA-50), property numbers. |
| 6 | 1/70-8/72 | 600 × 113 × 26 | 43,933 | 6,696 | Misc. scrap, wood, D&D. Covered with topsoil from TA-1 with up to 20 picocuries per gram plutonium contamination. |
| 7 | 3/74-10/75 | 600 × 50 × 30 | 17,101 | 4,343 | Low-level transuranic waste. Replaced Pit 17 for low-level transuranic waste in 1974. Covered with topsoil from TA-1 with up to 20 picocuries per gram plutonium contamination. |
| 8 | 9/71-5/74 | 400 × 25 × 25 | 6,528 | 2,311 | 55-gallon drums of sludge from H-7 and nonretrievable transuranic waste. Also drums from TA-50 (aqueous and nonretrievable transuranic waste). |
| 9 ^b | 11/74-11/79 | 400 × 30 × 20 | 9,027 | (b) | Drums and fiberglassed crates containing retrievable transuranic wastes (>10 nanocuries per gram plutonium-239 or uranium-233 or >100 nanocuries per gram plutonium-238). |
| 10 | 5/79-3/80 | 380 × 57 × 27 | 15,549 | 4,016 | Building debris, lab wastes, sludge drums (from TA-50 dewatering, possibly aqueous). |
| 12 | 9/71-12/75 | 400 × 25 × 25 | 7,303 | 2,363 | Transuranic-contaminated residual material. Originally contained retrievable transuranic waste that was transferred to Pit 9. |
| 13 | 11/76- 9/77 | 400 × 42 × 28 | 12,107 | 1,931 | Uranium, mixed fission and activation products. Uranium fission products and induced-activity wastes. |
| 16 | 9/71-8/75 | 400 × 25 × 25 | 8,081 | 2,235 | Crates and drums containing uranium-contaminated wastes. |
| 17 | 8/72-3/74 | 600 × 46 × 24 | 17,399 | 4,962 | Low-level plutonium transuranic waste, <10 microcuries per gram. Miscellaneous scrap wastes, crates, filter plenums. |
| 18 | 2/78-8/79 | 600 × 75 × 40 | 46,685 | 12,358 | Contaminated dirt, lab wastes, noncompactible waste, D&D, drums. |

²⁵ Additional shaft information is available in Table B-3 in the Investigation Work Plan for MDA G (LANL 2004c).

| Pit Number | Operational Period | Dimensions (feet) (length by width by depth) | Pit Volume^a (cubic yards) | Waste Volume^a (cubic yards) | Waste Description |
|-------------------|---------------------------|---|---|---|---|
| 19 | 11/75-8/79 | 153 × 30 × 18 | 1,371 | (c) | Asbestos and carcinogens, plastic layer placed in bottom. |
| 20 | 11/75-10/77 | 600 × 71 × 36 | 37,454 | 14,899 | Lab waste, oil, sludge drums, trash, contaminated dirt. |
| 21 | 8/72-12/74 | 402 × 56 × 26 | 13,328 | 3,607 | Uranium, classified material, boxes, drums, scrap metal. |
| 22 | 9/76-3/78 | 413 × 56 × 33 | 17,690 | 3,744 | Filter plenum, sludge drums (possibly aqueous from TA-50), lab waste, graphite fuel rods, contaminated dirt. |
| 24 | 5/75-11/76 | 600 × 58 × 30 | 23,388 | 7,327 | Graphite, lab wastes, 22 truck loads of soil. Uranium, tritium, mixed fission and activation products. |
| 25 | 1/80-5/81 | 395 × 103 × 39 | 47,000 | 6,530 | Reactor control rods, D&D, scrap drums, lab wastes, test drums, PCB-contaminated waste forms. |
| 26 | 2/84-2/85 | 310 × 100 × 36 | 22,209 | 4,312 | Building debris, transuranic waste culverts, asbestos, alpha box soil, lumber, PCBs. |
| 27 | 5/81-/82 | 400 × 80 × 46 | 26,946 | 7,441 | Lab waste, contaminated soil and pipe, D&D, PCBs, and unknown chemical waste. |
| 28 | 12/81-4/83 | 330 × 83 × 40 | 21,381 | 4,422 | Barium nitrate, PCB soil, lab waste, property numbers, transformers, clay pipes, building debris, uranium graphite. |
| 29 ^d | 10/84-10/86 | 658 × 80 × 50 | 45,795 | 9,784 | Retrievable transuranic-waste-contaminated cement paste, D&D soil, gloveboxes, plywood boxes, asbestos, PCBs, and unknown chemical waste. |
| 30 | 10/88-6/90 | 568 × 39 × 35 | 42,843 | 13,464 | Asbestos, PCBs, and unknown chemical waste. |
| 31 | 6/90-3/03 | 280 × 52 × 25 | (c) | 2,702 | Asbestos, mixed fission and activation products. |
| 32 | 11/85-8/87 | 518 × 74 × 51 | 36,364 | 5,367 | PCB asphalt, transformers, building debris, contaminated soil, gloveboxes, plywood boxes, capacitors. |
| 33 | 11/82-7/84 | 425 × 115 × 40 | 59,930 | 7,776 | Beryllium in stainless steel, lab waste, building debris, asbestos, noncompactible trash, PCBs, and unknown chemical waste. |
| 35 | 6/87-2/88 | 363 × 83 × 40 | 20,957 | 3,361 | Trash, plywood boxes, asbestos, lab waste, PCBs, and unknown chemical waste. |
| 36 | 1/88-12/88 | 435 × 83 × 43 | 28,057 | 4,491 | Plywood boxes, compactible N.N. trash, rubble, building waste, beryllium, and PCB-contaminated soil (less than 200 parts per million). |
| 37 | 4/90-4/97 | 731 × 83 × 61 | 57,213 | 24,299 | UHTREX reactor vessel and stack, asbestos, PCBs, and unknown chemical waste. |
| Total | | | 902,668 | 200,997 | – |

D-38 = depleted uranium, D&D = decontamination and decommissioning, TA = technical area, PCB = polychlorinated biphenyl, UHTREX = ultra-high-temperature reactor experiment.

^a Pit Volume = pit volume as field measured; Waste Volume = approximate volume of waste placed in pit.

^b Pit 9 contains disposed waste and 55,090 cubic feet of contact-handled transuranic waste stored above the pit under a soil cover.

^c No information available.

^d Stored above Pit 29 under a soil cover is contact-handled transuranic waste.

Note: To convert cubic feet to cubic meters, multiply by 0.028317, cubic yards to cubic meters, multiply by 0.76456; feet to meters, multiply by 0.3048; gallons to liters, multiply by 3.7854.

Source: LANL 2004c.

Table I-16 Material Disposal Area G Trench Information

| <i>Trench Number</i> | <i>Operational Period</i> | <i>Dimensions (feet) (length by width by depth)</i> | <i>Waste Description</i> |
|----------------------|---------------------------|---|--|
| A | 1974 | 262.5 × 12.75 × 8 | Heat sources containing plutonium (80 percent plutonium-238) and disposed of in casks. Average of 18 grams plutonium-238 per cask, with a maximum of 40 grams. |
| B | 1974 to 1976 | 218.75 × 12.75 × 8 | |
| C | No information | 218.75 × 12.75 × 10 (estimate) | |
| D | No information | 250 × 12.75 × 10 (estimate) | |

Note: To convert feet to meters, multiply by 0.3048; grams to ounces, multiply by 0.035274.

Source: LANL 2004c.

Table I-17 Material Disposal Area G Summary Shaft Information

| <i>Data Status</i> | <i>Shaft Number</i> |
|---|--|
| High tritium | 6, 7, 15, 16, 39, 50, 59, 61, 136, 137, 150-159 |
| Unknown tritium inventory | 3, 4, 8-11, 22, 30, 32, 60, 81, 104, 121, 132 |
| High cobalt-60 inventory | 22, 23, 97, 102, 108, 122 |
| Unknown cobalt-60 inventory | 95, 128 |
| High MAP-MFP ^a inventory | 1, 2, 28, 58, 94, 98, 100, 107, 110, 114, 120, 126, 139, 141, 189-192, 196 |
| Generally unknown values of radionuclides | 34, 37, 39, 56, 57, 70, 82, 84, 85, 118, 135, 138, 140 |
| Generally high radionuclide activity | 129, 133 |
| Generally unknown activity (less than 150 curies) | 12, 13, 14, 24, 25, 27, 36, 40-42, 45, 47, 52-55, 68, 69, 72, 74, 75, 77, 78, 79, 80, 83, 87, 93, 103, 106, 112, 115, 124, 134 |
| Activity generally known (less than 20 curies) | 5, 17-21, 26, 29, 31, 33, 35, 38, 43, 44, 46, 48, 49, 51, 62-67, 71, 76, 86, 88-92, 96, 99, 101, 105, 109, 111, 119, 123, 125, 127, 130, 131, 160, 206 |
| Polychlorinated-biphenyl-contaminated oil | C1-C13 |
| Transuranic waste storage | 200-232, 235-243, 246-253, 262-266, 302-306 |

^a MAP-MFP: mixed activation products or mixed fission products.

Source: LANL 1992a.

Table I-18 organizes the disposal units by their SWMU groupings (LANL 2004c).

Table I-18 Material Disposal Area G Solid Waste Management Unit Groupings

| <i>Subsurface Disposal and Storage Units</i> | <i>SWMU</i> | <i>Description</i> |
|--|-------------|--|
| Pit 9 | 54-014(b) | Pit with retrievably placed transuranic waste |
| 19 pits | 54-017 | Pits 1-8, 10, 12, 13, 16-22, 24 |
| 12 pits | 54-018 | Pits 25-33, 35-37 |
| Above Pit 19 | 54-013(b) | Truck decontamination operations that occurred on surface of Pit 19 |
| 4 trenches | 54-014(d) | Trenches A, B, C, D with retrievably stored transuranic waste |
| 68 shafts | 54-020 | Shafts C1-C10, C12, C13, 22, 35-37, 93-95, 99-108, 114, 115, 118-136, 138-140, 151-160, 189-192, 196 |
| 92 shafts | 54-019 | Shafts 1-20, 24-34, 38-92, 96, 109-112, 150 |
| 34 shafts | 54-014(c) | Shafts 200-233 |
| Above Pit 29 | 54-015(k) | Transuranic waste mound |

SWMU = solid waste management unit.

Source: LANL 2004c.

SWMU 54-014(b) is Pit 9. It received retrievable transuranic and mixed transuranic waste from 1974 to 1978. The filled pit was covered with 3.3 feet (1 meter) of crushed and compacted tuff and 4 inches (10 centimeters) of topsoil and reseeded with native grass (LANL 2004c).

SWMU 54-017 and SWMU 54-018 are two sets of pits. Pits comprising SWMU 54-017 are inactive. All but Pit 29 in SWMU 54-018 are inactive. (Although no longer in use, Pit 29 is an active regulated unit until RCRA closure is certified by NMED.) Both sets of pits received a variety of wastes. The filled pits were covered with 3.3 feet (1 meter) of crushed, compacted tuff, covered with 4 inches (10 centimeters) of topsoil, and reseeded with grass (LANL 2004c). Portions of several pits have been covered with concrete and used for purposes such as aboveground transuranic waste storage.

SWMU 54-13(b) was a vehicle monitoring and decontamination area on the surface of Pit 19 in the center of Area G. The area is no longer used (LANL 2004c).

SWMU 54-014(d) consists of four transuranic waste storage trenches. Beginning in 1974, the trenches received transuranic wastes in 30-gallon (0.11-cubic-meter) containers inside concrete casks. The trenches were backfilled with 3.3 feet (1 meter) of crushed tuff, covered with 4 inches (10 centimeters) of topsoil, and reseeded with grass (LANL 2004c).

SWMU 54-020 consists of 68 disposal shafts. Shaft 124 is an active regulated unit pending RCRA closure certification and NMED approval. The shafts contain PCB residues, low-level radioactive waste, and hazardous and mixed wastes. The shafts were filled with waste to within 3 feet (0.9 meters) of the ground surface, backfilled with crushed tuff, and capped with concrete (LANL 2004c).

SWMU 54-019 consists of 92 disposal shafts. The shafts received low-level radioactive waste, chemical and mixed wastes. Disposal shafts were filled with waste to within 3 feet (0.9 meters) of the ground surface, backfilled with crushed tuff, and covered with concrete domes (LANL 2004c).

SWMU 54-014(c) comprises 34 1-foot-diameter (0.3-meter-diameter), 18-foot-deep (5.5-meters-deep), shafts lined with concrete. The SWMU 54-014(c) shafts, now inactive, were used from 1979 to 1987 for transuranic waste. The shafts contain wastes requiring special packaging (mainly tritium), special handling (e.g., high surface-exposure rates), or segregation by activity. The shafts were filled with waste to within 3 feet (0.9 meters) of the ground surface, backfilled, and covered with concrete domes (LANL 2004c).

SWMU 54-015(k) is a layer of retrievable transuranic waste in cement-filled sections of corrugated metal pipes inside a mound of fill above Pit 29 (LANL 2004c). This waste was once stored in MDA T, as discussed in Section I.2.5.2.3.

Disposal units were generally dug, filled, and capped sequentially from the east end of the site to the west. Temporary spring-dome structures on concrete or asphalt pads have been placed over many of the disposal units to support waste operations (LANL 2004c).

Waste Inventory. The performance assessment and composite analysis for Area G contains disposed radionuclide inventories on a pit-by-pit basis and also inventories for groups of shafts in Area G (LANL 1997). **Table I-19** summarizes the hazardous chemical inventories within MDA G as summarized in the MDA G Investigation Work Plan (LANL 2004c).

Table I-19 Material Disposal Area G Hazardous Chemical Inventories

| <i>Hazardous Constituent</i> | <i>Pre-1971 Waste (kilograms)</i> | <i>1971 to 1990 Waste (kilograms)</i> |
|------------------------------|-----------------------------------|---------------------------------------|
| Aluminum | 0 | 480,000 |
| Arsenic | 2.2 | 380 |
| Barium | 520 | 430 |
| Beryllium | 0 | 19,000 |
| Cadmium | 12 | 1,900 |
| Chromium | 96 | 1,900 |
| Lead | 16 | 230,000 |
| Mercury | 1.3 | 380 |
| Nickel | 850 | 690 |
| Selenium | 3.6 | 3.0 |
| Silver | 22 | 18 |
| Acoclor-1260 | 0 | 200 |

Note: To convert kilograms to pounds, multiply by 2.2046.

Source: LANL 2004c.

Current Configuration. MDA G is within Area G, which, in addition to being the only active low-level radioactive waste disposal facility at LANL, is the focus of several other operations involving radioactive waste, including storage, characterization, and processing by compaction or repackaging of transuranic waste destined for disposal at WIPP; characterization and compaction of low-level radioactive waste before disposal; and storage of mixed low-level radioactive waste destined for offsite treatment or disposal. Portions of the MDA G disposal units are covered with concrete to support Area G waste management activities. Surface runoff from the site is controlled, discharging into drainages to the north to Cañada del Buey, and to the south to Pajarito Canyon. Stormwater and sediment monitoring stations are distributed throughout Area G and in the drainages around Area G (LANL 2006h).

The 63-acre portion of Area G shown in Figure I-15 will be closed to meet the Consent Order deadline for closure of MDA G. The closure approach must integrate and accommodate all applicable regulatory requirements. All storage and disposal units are subject to DOE requirements under the Atomic Energy Act. Many disposal units in Area G are SWMUs and AOCs that comprise MDA G and are subject to corrective action under the Consent Order. Other disposal units are RCRA-regulated disposal units subject to RCRA closure and postclosure care requirements. Low-level waste disposal operations will continue in Zones 4 and 6 at Area G. As analyzed in Appendix H, Section H.3, other waste management activities would be transferred to other LANL locations.

Site Investigations. Early investigations determined the soil moisture characteristic curves; intrinsic permeability and unsaturated hydraulic conductivity of the tuff; infiltration and redistribution of meteoric water in the tuff; presence of core and pore gas in the vadose zone; and presence of perched water. Volatile organic compounds were found in pore gas beneath the MDA. The primary volatile organic compound pore gas constituent was 1,1,1-trichloroethane, present to at least 153 feet (47 meters) below ground surface (LANL 2004c).

MDA G Phase I RFI fieldwork was conducted from 1993 through 2003. The results of these investigations are summarized below (LANL 2004c).

- There were infrequent detections of radionuclides in samples of tuff beneath pits, trenches, and shafts. No pattern of detections was seen from borehole samples.
- There were infrequent detections of inorganic chemicals in samples of tuff beneath the pits, trenches, and shafts. It could not be determined whether inorganic chemicals had been released from the disposal units.
- Tritium had been released into the tuff beneath the disposal units.
- Volatile organic compounds, mainly trichloroethane, were detected in subsurface pore gas.
- Drainage channel sediments contained low concentrations of methoxychlor, americium-241, cobalt-60, plutonium-238, plutonium-239, and tritium. Beryllium, cobalt, mercury, selenium, and silver were not found above background values; however, detection limits for some samples were elevated above background values. Cadmium was found above its background value.
- Volatile organic compounds and tritium were being released into the atmosphere from the subsurface.

The required Investigation Report for MDA G was submitted in September 2005 (LANL 2005q). Thirty-nine boreholes were drilled alongside MDA G disposal units, including two to depths of 556 to 700 feet (169 and 213 meters), respectively. Organic and inorganic chemicals were found beneath the disposal units at trace levels that were generally consistent with results from the Phase I RFI. Naturally-occurring and anthropogenic radionuclides were found above background values in soils and rock samples from beneath MDA G. Generally sporadic detections of americium-241, plutonium-238, plutonium-239, and strontium-90 occurred across the site. Thorium isotopes, uranium-234, uranium-235, and uranium-238 were found at concentrations within their natural variability in the subsurface. Volatile organic compounds were found in pore-gas samples from 38 of the boreholes, and tritium in pore-gas samples from 35 of the boreholes. The highest concentrations of volatile organic compounds and tritium were from boreholes in the eastern and south-central portions of MDA G. Perched groundwater was not found in any of the boreholes, including the one drilled to 700 feet (213 meters) (LANL 2005q). On July 26, 2006, NMED issued a notice of disapproval for the MDA G Investigation Report (NMED 2006a). On August 31, 2006, LANL staff sent a response to the notice of disapproval agreeing to deepen four existing boreholes to further characterize the vertical extent of organic vapor contamination (LANL 2006e). The results of the pore-gas sampling from boreholes

confirmed the results of the Phase I RCRA facility investigations, previous quarterly monitoring, and the 2005 site investigation (LANL 2007a).

In response to a September 13, 2006 letter from NMED about vapor-phase tritium found in increased concentrations with depth in a borehole down-gradient of the active tritium disposal shafts, DOE directed LANL staff to determine whether the trend extends to the basalt layer. The LANL management and operating contractor agreed to increase the depth of a nearby borehole, install equipment to monitor for tritium, and report the results of monitoring to NMED (LANL 2006j). Monitoring results showed that tritium concentrations peaked at 50 feet (15 meters) below ground surface near the base of the nearby 60-foot (18-meter) deep tritium shafts. The concentrations decreased as the sampling depth increased to about 240 feet (73 meters) below ground surface (LANL 2007a).

In July 2007, DOE issued a plan that describes the regulatory basis and the technical approach for performing a Corrective Measures Evaluation at MDA G. The plan identifies specific corrective measure alternatives to be evaluated including source containment or stabilization, source removal, contaminant extraction, or combinations of these alternatives (LANL 2007b). In July 2007, DOE also issued a work plan for implementing an *in situ* soil vapor extraction pilot study at MDA G (LANL 2007c).

I.2.5.5.2 Material Disposal Area H

MDA H (SWMU 54-004) is within a fenced 0.3-acre (0.1-hectare) area of TA-54. Nine shafts were used for disposal of classified waste from 1960 to 1986. A RCRA investigation program was completed and submitted to NMED in 2001, along with an addendum in 2002. A Corrective Measures Study Report for this MDA was completed in May 2003 (LANL 2003b), and an environmental assessment was issued in June 2004 (DOE 2004d).

NMED selected a corrective remedy for MDA H requiring complete encapsulation of the disposal shafts, a soil vapor extraction system, and construction of an engineered evapotranspiration cover (NMED 2007a). The Consent Order also requires collection and analysis of subsurface vapor samples and monitoring of groundwater in canyons potentially affected by MDA H (NMED 2005).

I.2.5.5.3 Material Disposal Area L

MDA L (SWMU 54-006) is within a 2.58-acre (1.0-hectare) site (Area L) north of Mesita del Buey Road between MDA G and MDAs H and J. The land north of MDA L drops steeply away to Cañada del Buey. Pajarito Canyon is to the south. Between about 1959 and 1985, chemical wastes were disposed of within unlined pits and shafts. Since 1986, Area L has stored RCRA waste, PCB waste, and mixed waste such as contaminated lead (LANL 1999b).

History of MDA L. MDA L was used from the late 1950s to 1986 for disposal of containerized and non-containerized nonradiological liquid wastes; bulk quantities of aqueous wastes; treated salt solutions and electroplating wastes, including precipitated heavy metals; and treated lithium hydride. The MDA consists of Pit A; Impoundments B, C, and D for liquids; and 34 shafts (**Figure I-16**). All disposal units are unlined (LANL 1992a, LANL 2003m). The dimensions and operation periods of each of the disposal units are summarized in **Tables I-20** and **I-21** (LANL 2003m). The pit, impoundments, and shafts are collectively identified as SWMU 54-006. Since 1986, Area L has stored RCRA waste, PCB waste, and mixed waste such as contaminated lead (LANL 1999b).

Pit and Impoundments. Pit A had three near-vertical walls on the north, south, and west sides and a ramp on the east side leading to a flat bottom. After being filled to within 3 feet (0.9 meters) of the surface, the pit was covered with crushed tuff in 1978. Impoundments B, C, and D had near-vertical walls on the east and west sides, and ramps on the north and south sides leading to flat bottoms. After Impoundments B and C were decommissioned, residual waste was covered with at least 3 feet (0.9 meters) of crushed tuff (LANL 2003m).

Impoundment D was used for treating small quantities of lithium hydride by reaction with water. The neutralized solutions were evaporated. Treatment was discontinued in 1984. Impoundment D was partially filled with crushed tuff in 1985 and completely filled in 1989. Between 1984 and 1989, aboveground used-oil storage tanks were placed next to Impoundment D (LANL 1992a). The waste oil storage tanks were emptied in 1985 and, in 1989, taken to Area G in TA-54²⁶ (LANL 2003m).

Shafts. The 34 shafts range from 3 to 8 feet (0.9 to 2.4 meters) in diameter and from 15 to 65 feet (4.6 to 20 meters) deep. (The depth of most is 60 feet [18 meters].) After layering the bottom 3 feet (0.9 meters) of each shaft with crushed tuff, the shafts were filled with waste to within 3 feet (0.9 meters) of the surface; the remaining void was filled with concrete. Before 1982, liquids were disposed of in containers without adding absorbents. Small containers were often dropped into the shafts. Larger drums were lowered by cranes. Spaces around the drums were filled with crushed tuff, and a 6-inch (15-centimeter) layer of tuff placed between each layer of drums. In early years, uncontainerized liquid wastes were dumped into the shafts. Between 1982 and 1985, only containerized wastes were emplaced. When MDA L was decommissioned in 1986, its surface was partially paved with asphalt for permitted storage of hazardous and mixed wastes (LANL 2003m).

Waste Inventory. Estimates of the waste types and quantities disposed of in MDA L are summarized in the Historical Investigation Report for MDA L (LANL 2003m). Waste disposal records for MDA L are found in un-numbered logbooks. Records before 1974 are incomplete, and many logbooks contain only brief descriptions. Residuals from treatment of wastes in the impoundments may have been left in place (LANL 2003m).

²⁶ The tanks were closed in 1990 under RCRA regulations.

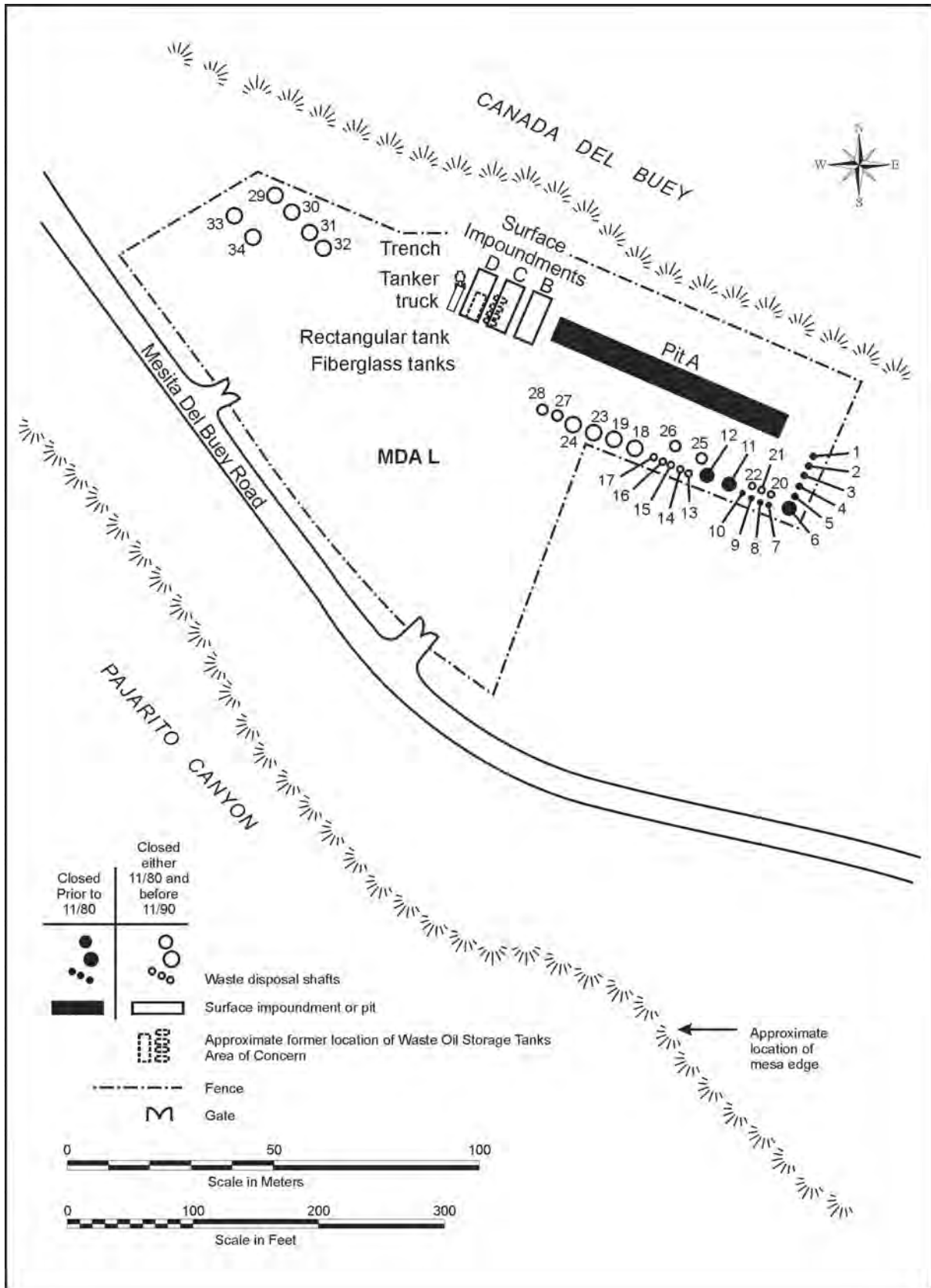


Figure I-16 Material Disposal Area L Inactive Waste Unit Locations

Table I–20 Material Disposal Area L Pit and Impoundment Dimensions and Operation Dates

| <i>Pit or Impoundment</i> | <i>Dimensions (feet) (length by width by depth)</i> | <i>Period of Use</i> |
|---------------------------|---|----------------------|
| A | 200 × 12 × 10 | 1950s - 12/1978 |
| B | 60 × 18 × 10 | 1/1979 - 6/1985 |
| C | 35 × 12 × 10 | 1964 - 1978 |
| D | 75 × 18 × 10 | 1972 - 1984 |

Note: To convert feet to meters, multiply by 0.3048.
Source: LANL 2003m.

Table I–21 Material Disposal Area L Shaft Dimensions and Operation Dates

| <i>Shaft</i> | <i>Diameter/Depth (feet)/(feet)</i> | <i>Period of Use</i> | <i>Shaft</i> | <i>Diameter/Depth (feet)/(feet)</i> | <i>Period of Use</i> |
|--------------|---|----------------------|--------------|---|----------------------|
| 1 | 3/60 | 4/80 - 8/83 | 18 | 8/60 | 6/79 - 5/80 |
| 2 | 3/60 | 2/75 - 6/79 | 19 | 8/60 | 4/80 - 4/82 |
| 3 | 3/60 | 2/75 - 10/78 | 20 | 3/60 | 3/82 - 8/83 |
| 4 | 3/60 | 2/75 - 4/80 | 21 | 3/60 | 3/82 - 12/84 |
| 5 | 3/60 | 2/75 - 5/77 | 22 | 3/60 | 3/82 - 8/83 |
| 6 | 4/60 | 6/75 - 5/79 | 23 | 4/60 | 4/82 - 2/84 |
| 7 | 3/60 | 6/75 - 5/79 | 24 | 4/60 | 4/82 - 3/84 |
| 8 | 3/60 | 6/75 - 5/79 | 25 | 6/60 | 9/82 - 4/85 |
| 9 | 3/60 | 6/75 - 5/79 | 26 | 6/60 | 9/82 - 2/84 |
| 10 | 3/60 | 6/75 - 5/79 | 27 | 4/60 | 1/83 - 1/85 |
| 11 | 8/60 | 1/78 - 6/79 | 28 | 4/60 | 1/82 - 4/85 |
| 12 | 4/60 | 1/78 - 6/79 | 29 | 6/65 | 12/83 - 7/84 |
| 13 | 8/60 | 6/79 - 4/82 | 30 | 6/65 | 12/83 - 4/84 |
| 14 | 3/60 | 6/79 - 4/82 | 31 | 6/61 | 12/83 - 8/84 |
| 15 | 3/60 | 6/79 - 4/82 | 32 | 4/15 | 3/84 - 8/84 |
| 16 | 3/60 | 6/79 - 4/82 | 33 | 6/65 | 3/84 - 1/85 |
| 17 | 3/60 | 6/79 - 4/82 | 34 | 6/63 | 2/85 - 4/85 |

Note: To convert feet to meters, multiply by 0.3048.
Source: LANL 2003m.

Pit and Impoundments. Pit A received containerized and uncontainerized liquid chemical wastes. About 5,123 cubic feet (145 cubic meters) of liquid waste was discharged to Pit A. A salt layer remained on the pit floor after the aqueous phase evaporated. Impoundments B and C evaporated treated salt solutions and electroplating wastes. Treated wastes placed in Pit A and Impoundments B and C were generated from the following processes (LANL 2003m):

- Ammonium bifluoride waste was neutralized with calcium chloride and calcium hydroxide, yielding an aqueous solution of ammonium chloride, calcium, fluoride, and water.
- Acids and caustics in quantities larger than 55 gallons (208 liters) were diluted and neutralized. Acids were neutralized with sodium hydroxide; bases with mineral acids. Heavy metals were precipitated and removed before disposal in shafts.

- Cyanide solutions were treated with calcium hypochlorite or calcium chloride and calcium hydroxide, resulting in cyanate, carbon dioxide, and nitrogen. After treatment, the aqueous solution was discharged to the pit or the impoundment. Solids from the process were mixed with cement in metal drums and disposed of in MDA L shafts.
- Chromium waste was treated with sodium hydroxide and a reducing agent (sulfur dioxide or sodium bisulfate). End products were sodium sulfate and chromium hydroxide. Treated chromium waste was disposed of in MDA L shafts.

Shafts. Shafts 1 through 34 were used for disposal of containerized and uncontainerized liquid wastes and precipitated solids from treatment of aqueous wastes. Heavy metals precipitated from acid or caustic solutions were packaged in 15-gallon (57-liter) drums and disposed of in the same shafts as the neutralized acid or caustic solutions. Shafts used for disposal of neutralized acid solutions were also used for disposal of treated chromium waste (LANL 2003m).

Current Configuration. A 3- to 4-foot-high (0.9- to 1.2-meters-high) vertical retaining wall bounds the north and east sides of the site, and a stormwater diversion channel runs outside this retaining wall, immediately above the escarpment. An electrical line is buried outside of the northern boundary of the site (Stephens 2005).

Figure I-17 shows the location of the MDA L disposal units along with important structures (LANL 2003d). Stormwater is directed to an outfall at the northeast corner of the liquid low-level radioactive waste storage dome discharging into Cañada del Buey. The area is surrounded by a security fence and is covered with asphalt. Administrative offices are outside of the security fence adjoining Mesita del Buey Road. The area has water, electricity, and telephone services (LANL 1992a, 2003m).

Site Investigations. Early investigations determined the soil moisture characteristic curves; intrinsic permeability and unsaturated hydraulic conductivity of the tuff; infiltration and redistribution of meteoric water in the tuff; presence of core and pore gas in the vadose zone; and the possible presence of perched water. Early investigations documented a subsurface vapor-phase volatile organic compound plume extending beneath the site and beyond the boundary of MDA L. The primary constituents were 1,1,1-trichloroethane, present to a depth of at least 200 feet (61 meters) below ground surface, and trichloroethene. Other organic vapor-phase compounds included carbon tetrachloride, chloroform, tetrachloroethene (also known as tetrachloroethylene or perchlorethylene), toluene, chlorobenzene, xylene, and 1,2,4-trimethylbenzene (LANL 2003m). Investigations also identified moist-to-wet conditions at multiple depths within basalt beneath MDA L (see below) (LANL 2003m).

Phase I RFI fieldwork was conducted from 1993 through 2003 (LANL 2003m). Channel sediment samples contained inorganic chemicals, methoxylchlor, and a single instance of plutonium-238. Inorganic materials, organic chemicals, and tritium were detected in tuff, and tritium was detected in ambient air. Pore gas samples showed detectable levels of volatile organic compounds. The primary volatile organic compound was trichloroethane, followed by trichloroethene (LANL 2003m).

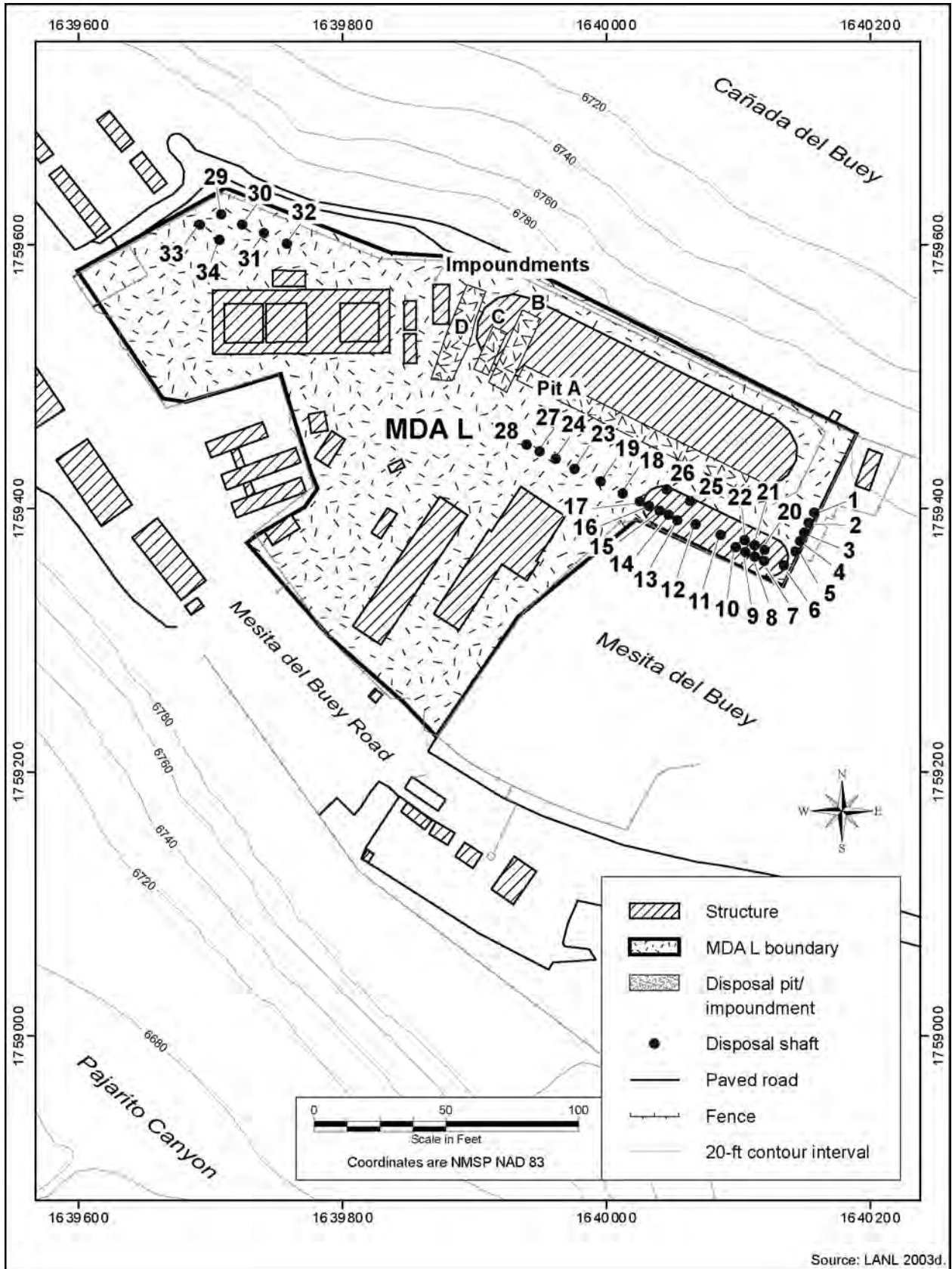


Figure I-17 Location of Subsurface Disposal Units at MDA L

Samples of surface flux were measured for tritium and for volatile organic compounds. All samples were obtained from areas of MDA L not covered by asphalt. Six samples had measured tritium emission fluxes of 2 to 5.5 picocuries per minute per square meter; one had a flux of 20,000 picocuries per minute per square meter; and one had a flux of 29,000 picocuries per minute per square meter. Twenty volatile organic compounds were detected, the most prevalent being trichloroethane, trichloroethene, and perchlorethylene (LANL 2003m).

The required Investigation Report for MDA L was submitted to NMED in September 2005 (LANL 2005r). Subsurface samples collected to evaluate moisture properties did not identify any perched groundwater zones to a depth of 660 feet (201 meters) beneath MDA L. Volatile organic compounds and tritium were found in pore-gas samples collected from 8 boreholes, each drilled to a minimum depth of 150 feet (46 meters). Among other points, the Investigation Report recommended using the results of a soil vapor extraction pilot study to evaluate this method as a potential remediation strategy (LANL 2005r). The workplan for this pilot study was submitted to NMED in May 2005 (LANL 2006h). Results of the study were addressed in a November 2006 Summary Report (LANL 2006m). In 2007, DOE issued an addendum to the Investigation Report for MDA L describing the results of supplemental drilling and sampling activities conducted to complete the investigation of MDA L (LANL 2007d) and issued a revision to the interim subsurface vapor monitoring plan for MDA L (LANL 2007e). In January 2008, DOE submitted a Corrective Measures Evaluation Report for MDA L to NMED recommending a corrective remedy that would feature an engineered evapotranspiration cover, a soil vapor extraction system, monitoring, and maintenance (LANL 2008a).

I.2.6 Other Solid Waste Management Units and Areas of Concern, Including Aggregate Areas

Section V of the Consent Order addresses requirements for all SWMUs and AOCs that are not addressed in Sections IV and VI of the Consent Order. (Section IV is discussed in Section I.2.5 of this appendix; Section VI is discussed in Section I.2.7.) The Consent Order sets forth requirements for identifying, investigating, and taking corrective action (if necessary) at any SWMU or AOC discovered after the effective date of the Consent Order, or any newly discovered releases from existing SWMUs or AOCs. Furthermore, the Consent Order presents requirements for addressing SWMUs and AOCs located in aggregate areas²⁷ (NMED 2005).

As required by the Consent Order, a list has been submitted to NMED identifying all aggregate areas and the SWMUs and AOCs within each aggregate area. Investigative work plans must be prepared for these aggregate areas. Following completion and submittal of the investigations, NMED may require corrective measure evaluations for any SWMU or AOC in any aggregate area. Investigation work plans for each aggregate area must be submitted in accordance with Consent Order schedules. Aggregate-area-specific investigation reports must be submitted by the dates specified in approved investigation work plans (NMED 2005).

²⁷ The Consent Order defines an aggregate area as an area within a single watershed or canyon made up of one or more solid waste management units (SWMUs) or Areas of Concern (AOCs) and the media affected or potentially affected by releases from those SWMUs or AOCs, and for which investigation or remediation, in part or in entirety, is conducted for the area as a whole to address areawide contamination, ecological risk assessment, and other factors.

The required list of aggregate areas was submitted in 2005 (LANL 2005n). All SWMUs and AOCs, except for canyons identified as AOCs,²⁸ were assigned to an aggregate area to ensure addressing cumulative impacts of all potentially collocated releases in the corrective action process. The SWMUs and AOCs were assigned to the aggregate areas based on factors such as operational history, potential historical risk, and physical location. Aggregate area boundaries were based mainly on boundaries of grouped subwatersheds, but were adjusted to maximize integration, consistency, and efficiency. The 29 aggregate areas within the eight major watersheds of the Rio Grande River and one watershed of the Jemez Mountains, are listed in **Table I–22** (LANL 2005n). The 29 aggregate areas contain hundreds of PRSs, many of which are described in other sections of this analysis.

Several work plans for these aggregate areas have been submitted to NMED, including those addressing the DP Site Aggregate Area at TA-21 (LANL 2004e); the Guaje, Barrancas, Rendija Canyons Aggregate Area at TA-00 (LANL 2005j); and the Pueblo Canyon Aggregate Area (LANL 2005g). In addition, the Bayo Canyon Aggregate Area Investigation Work Plan and the Middle Mortandad-Ten Site Canyon Aggregate Area Investigation Report have been submitted to NMED (LANL 2005m). Aggregate area Investigation Work Plans have also been submitted for Middle Los Alamos Canyon Aggregate Area, Upper Los Alamos Canyon Aggregate Area, and Cañon de Valle Aggregate Area.

Table I–22 Aggregate Areas and Watersheds

| <i>Watershed</i> | <i>Aggregate Area</i> | <i>Watershed</i> | <i>Aggregate Area</i> |
|------------------|------------------------------------|------------------|--------------------------------|
| Los Alamos | Guaje, Barrancas, Rendija Canyons | Pajarito | Twomile Canyon |
| | Bayo Canyon | | Starmer, Upper Pajarito Canyon |
| | Pueblo Canyon | | Lower Pajarito Canyon |
| | Upper Los Alamos Canyon | | Threemile Canyon |
| | Middle Los Alamos Canyon | Water | Cañon de Valle |
| | DP Site | | Potrillo, Fence Canyons |
| | Lower Los Alamos Canyon | | S-Site |
| Sandia | Upper Sandia Canyon | | Upper Water Canyon |
| | Lower Sandia Canyon | | Lower Water, Indio Canyons |
| Mortandad | Upper Mortandad Canyon | Ancho | North Ancho Canyon |
| | Middle Mortandad, Ten Site Canyons | | South Ancho Canyon |
| | Lower Mortandad, Cedro Canyons | Chaquehui | Chaquehui Canyon |
| | Upper Cañada del Buey | Frijoles | Frijoles Canyon |
| | Middle Cañada del Buey | Lake Fork | TA-57 (Fenton Hill) |
| | Lower Mortandad, Cañada del Buey | | |

TA = technical area.
Source: LANL 2005n.

I.2.7 Continuing Investigations

Section VI of the Consent Order requires continued investigation of the SWMUs listed in **Table I–23**. Investigations of these sites were planned or ongoing at the time the Compliance Order was originally issued in November 2002. Hence, many Consent Order requirements for the listed SWMUs have already been met.

²⁸ AOCs that are canyons were not assigned an aggregate area and are being investigated pursuant to Section IV.B of the Consent Order.

Table I-23 Solid Waste Management Units Requiring Continuing Investigation

| <i>SWMU</i> | <i>Description</i> |
|------------------------------|--|
| 3-010(a) | Used for disposal of vacuum oil from Building TA-3-30 pump repair area |
| 16-003(o) | Known as the fish ladder, the former outfall from Building TA-16-340 |
| 16-008(a) | Inactive, unlined pond 200 feet (61 meters) in diameter |
| 16-018 (MDA P) and TA-16-387 | SWMUs included with MDA P closure, including a former barium nitrate pile, the TA-16-386 and TA-16-387 and the septic tank drain field and outfall |
| 16-021(c) and 16-003(k) | Collectively the outfall, drainage, and associated sumps and drain lines from the active explosives machining building, TA-16-260 |
| 21-011(k) | Outfall for industrial wastewater from Buildings TA-21-35 and TA-21-257 |
| TA-35 | The Middle Mortandad-Ten Site Aggregate Area |
| TA-49, Areas 5, 6, and 10 | SWMUs associated with historic hydrodynamic studies at MDA AB |
| 53-002(a and b) | Impoundments that have received sanitary, radioactive, and industrial wastewater from several TA-53 facilities |
| 73-001(a-d) and 73-004(d) | Airport landfill, comprising five SWMUs: main landfill, waste oil pit, bunker debris pits, debris disposal area, and a septic system |
| 73-002 | Ash pile from a former incinerator next to the Los Alamos County Airport |

SWMU = solid waste management unit, TA = technical area, MDA = material disposal area.

Source: NMED 2005.

I.2.7.1 Solid Waste Management Unit 3-010(a): Vacuum Oil Disposal Area

SWMU 3-010(a) within TA-3 (South Mesa Site) was used between 1950 and 1957 for disposal of vacuum oil from the pump repair area within Building TA-3-30. The disposal site is 40 feet (12 meters) long by 15 feet (4.6 meters) wide and is on a hillside on the west side of Building TA-3-30. Consent Order investigations are meant to determine the extent of groundwater contamination, determine sources and flow directions, any connection between the shallow groundwater and deeper zones, and other contaminants (NMED 2005). The Groundwater Investigation Report for SWMU 03-010(a) was submitted to NMED on 31 August 2005. The report defined the nature and extent of chemicals of potential concern in soil and tuff, and concluded that the shallow groundwater body beneath this site and SWMU 03-001(e) (a former waste storage area) was of limited extent, and most likely recharged from stormwater runoff. Among other studies, quarterly groundwater monitoring will be conducted at the sites for two years to better understand the sources of the groundwater and to determine temporal trends of the contaminants of potential concern and their potential for natural attenuation (LANL 2006h).

I.2.7.2 Solid Waste Management Unit 16-003(O): Fish Ladder Site

Covering 2,410 acres (975 hectares), TA-16 is in the southwest corner of LANL. TA-16 is bordered by Bandelier National Monument south of New Mexico (NM) 4 and by Santa Fe National Forest west of NM 501. TA-16 is bordered to the north and east by TA-8, -9, -11, -15, -37, and -49. The northern border of TA-16 is Cañon de Valle (LANL 2003l). TA-16 was established to develop explosives, cast and machine explosives, and assemble and test explosives for nuclear weapons. This mission continues (LANL 2003l).

SWMU 16-003(o) comprises six inactive high explosive sumps and an outfall associated with the explosives synthetics building (Building 16-340), the largest of five structures that produced

plastic-bonded explosive powders from the early 1950s until October 1999. Between 1951 and 1988, explosive-contaminated wastewater was untreated before discharge. Starting in the early 1980s and lasting through 1998, various methods were used to reduce volatile organic compound concentrations in effluent. Although most volatile organic compounds were distilled during processing, the remaining solvents were discharged. The effluent historically discharged to a permitted outfall that was removed from the LANL National Pollutant Discharge Elimination System (NPDES) permit effective July 20, 1998 (LANL 2005c, NMED 2005).

The Consent Order requires continuing investigation to fully characterize the vertical and lateral extent of sediment and groundwater contamination by these contaminants and other metals (NMED 2005). The investigation report for the Fish Ladder Site was submitted to NMED on January 31, 2006, and was approved on October 25, 2006. Phase II investigations are ongoing.

I.2.7.3 Solid Waste Management Unit 16-008(a): Inactive Pond

Consolidated Unit 16-008(a)-99 comprises the footprints of former high explosive process buildings; former materials storage buildings; and sumps, drain lines, and outfall systems. Most structures were built in 1950 for machining high explosive. After 1970, the buildings were used for storage until, by 1991, they were all removed from service. The structures were removed in 1996 (LANL 2005c).

One SWMU (16-008(a)) is an inactive, unlined pond 200 feet (61 meters) in diameter. The pond received liquids from sumps and drain lines from process buildings. The discharge began as early as 1949; lasted until the mid-1950s; and contained explosives, barium, uranium, volatile organic compounds, machining oils, nickel, and cadmium. The area contains runoff and occasionally dries up in the summer (LANL 2005c, NMED 2005). The Consent Order requires continued investigation to fully characterize the vertical and lateral extent of surface, vadose, and groundwater contamination (NMED 2005).

The Investigation Work Plan for SWMU 16-008(a) and associated sites was submitted to NMED on March 31, 2004, and approved by NMED on June 28, 2004.

I.2.7.4 Solid Waste Management Unit 16-018 (Material Disposal Area P) and Technical Area 16-387

SWMUs incorporated into NMED-required closure activities for MDA P (SWMU 16-018) include the former barium nitrate pile (SWMU 16-016(c)); the TA-16-386 flash pad (SWMU 16-010(a)); the TA-36-387 flash pad (SWMU 16-019(b)); and the septic tank drain field and outfall (SWMU 16-006(e)) (NMED 2005).

MDA P was a 1.4-acre (0.57-hectare) waste pile near the south rim of Cañon de Valle. In 1995, LANL submitted a closure plan to NMED proposing to clean-close MDA P. NMED approved the closure plan for MDA P on February 20, 1997, and approved the closure plan for the TA-16-387 flash pad on April 28, 2000 (NMED 2005). Contamination was removed as described in Section I.3.3.1.3.1. A closure certification report for MDA P and the TA-16-387 flash pad was submitted to NMED on January 31, 2003. On April 30, 2003, NMED requested its

reformatting and resubmittal. One of the four documents composing the reformatted closure report was submitted to NMED on July 9, 2003 (NMED 2005).

The Consent Order requires submittal of the remaining three documents composing the closure report for MDA P (NMED 2005). All three documents were submitted in 2003. The MDA P closure certification report was approved by NMED, and no further actions are required under the Consent Order.

I.2.7.5 Solid Waste Management Units 16-021(c) and 16-003(k): 260 Outfall

Operating since 1951, Building 16-260 processed and machined HE (LANL 2002c). Machine turnings and HE washwater were flushed to building sumps and routed to the TA-16-260 outfall. Liquids from the outfall drained to a settling pond 40 feet (12 meters) away (**Figure I-18**) (LANL 2003). The settling pond was 50 feet (15 meters) long and 20 feet (6.1 meters) wide. Pond overflow flowed through the drainage channel for 300 feet (91 meters) before dropping to a lower drainage channel that continued to the bottom of Cañon de Valle (LANL 2003). EPA permitted the outfall in the late 1970s. The last NPDES permitting effort occurred in 1994, the outfall was deactivated in November 1996, and the outfall was removed from LANL's NPDES permit in January 1998. Liquids once routed to the outfall are now treated in the TA-16 wastewater plant that was completed in 1997 (LANL 2003).

Consolidated SWMU 16-021(c)-99 includes:

- SWMU 16-003(k), comprising 13 sumps in the HE machining building (TA-16-260) plus 1,200 feet (366 meters) of associated drain lines (concrete troughs) that ran 200 feet (61 meters) to the outfall east of the HE machining building
- SWMU 16-021(c), comprising the upper draining channel fed directly by the outfall, the settling pond and associated surge beds beneath the settling pond (see below), and the lower drainage channel leading to the bottom of Cañon de Valle

During 2000 and 2001, an interim measure removed contaminated soil from the settling pond and channel (LANL 2003).

The 260 Outfall has three areas of contamination (LANL 2003): an outfall source area (excluding the settling pond and surge beds); outfall settling pond and surge beds; and canyon springs and alluvial system. The outfall source area refers to the drainage channels. Fewer than 100 cubic yards (76 cubic meters) of residual contaminated soil remains within the outfall source area (LANL 2003). The settling pond has underlying surge beds at depths below ground surface of 17 and 45 feet (5.2 and 14 meters). The canyon springs and alluvial system refers to sediments, springs, surface water, and alluvial groundwater in Cañon de Valle and in Martin Spring Canyon (LANL 2003).

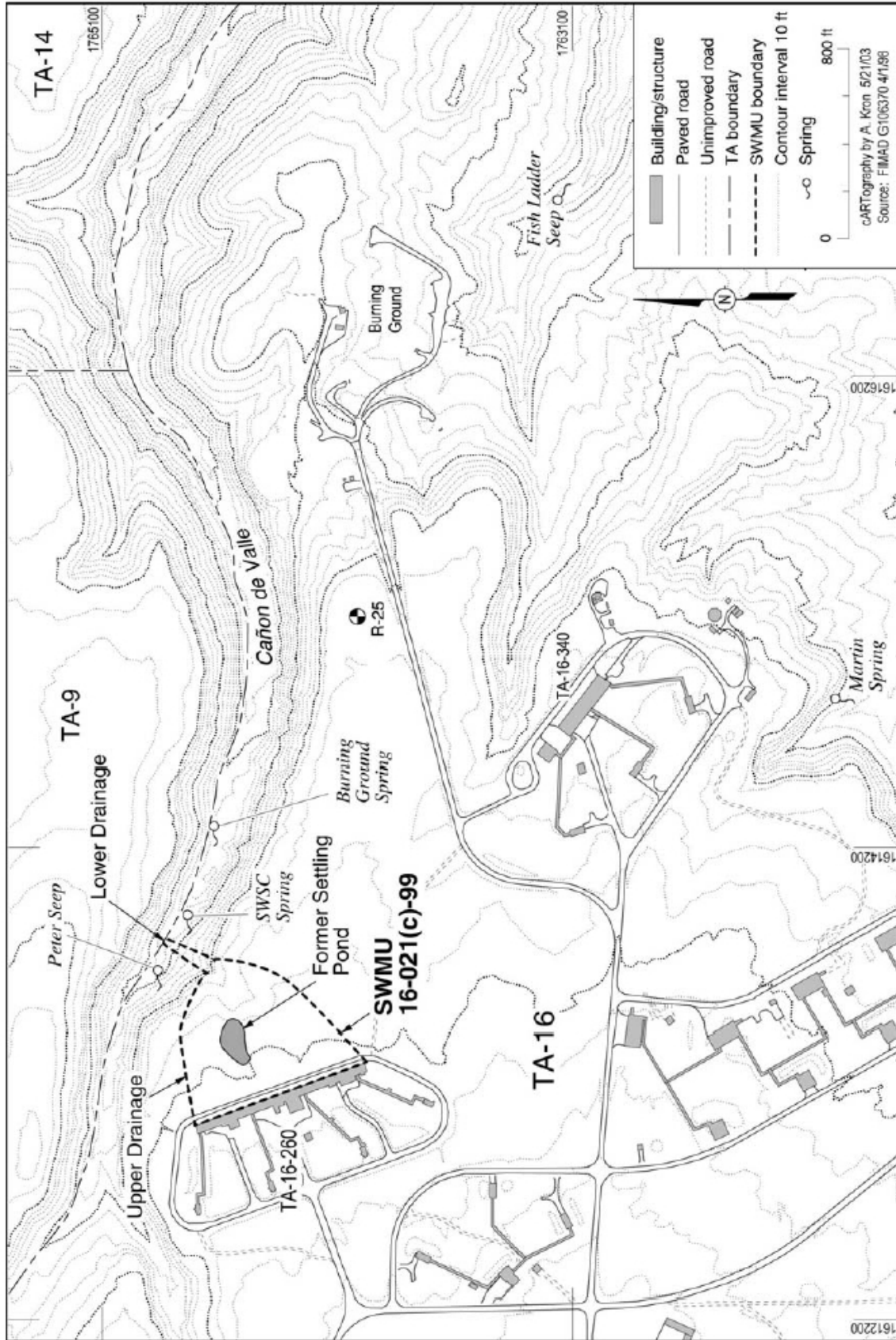


Figure I-18 260 Outfall Within Technical Area 16

Both the outfall and the drainage channel below the outfall are contaminated with high explosive and barium. Known contaminants include barium, RDX (hexahydro-1,3,5-trinitro-1,3,5-triazine), TNT (2,4,6-trinitrotoluene), and HMX (octahydro-1,3,5,7-tetranitro-3,5,7-tetrazocine). Suspected contaminants include other high explosive compounds, inorganic chemicals, volatile organic compounds, semivolatile organic compounds, and uranium. The 17-foot (5.2-meter) surge bed beneath the settling pond contains detectable levels of RDX, HMX, and TNT. The 45-foot (24-meter) surge bed contains detectable levels of RDX and HMX (LANL 2003i).

Several site investigations have been conducted as summarized in the Corrective Measures Study Report (LANL 2003i) and the Phase III RFI Report, issued in September 2003 (LANL 2003g) and revised in September 2004 (LANL 2004g).

NMED selected a final remedy for the surface and alluvial system on October 13, 2006. The investigation report for intermediate and regional groundwater was approved by NMED on November 29, 2006; and additional groundwater investigations are ongoing to support the intermediate and groundwater corrective measure evaluation.

The land adjacent to the outfall is dedicated to continued LANL operations (LANL 2003i).

I.2.7.6 Solid Waste Management Unit 21-001(k): Technical Area 21 Outfall

SWMU 21-011(k) was an NPDES-permitted outfall. The SWMU includes a drainage pipe and an outfall ditch that routed wastewater north over the south rim of DP Canyon and into the canyon itself. The outfall received industrial effluent from the wastewater treatment plant in Building 21-35 from 1952 until 1967 and from the wastewater treatment plant in Building 21-257 from 1967 until the early 1990s (LANL 2002f).

SWMU 21-011(k) was investigated in 1988, 1992, and 1993. A 1996 interim action removed the contaminated soil from the hillside (LANL 2002f). A November 2000 gamma spectrometry for the site was followed in March 2001 by collection of samples that identified remaining hotspots (LANL 2002f). A voluntary corrective measure was prepared that included the following actions: (1) excavate and dispose of the outfall drain line and other waste; (2) excavate and solidify contaminated tuff and sediment; (3) place solidified material in a cell excavated near the center of the SWMU; (4) place and compact clean fill over the entire site; and (5) conduct site inspections and radiation surveys (LANL 2002f). However, plans for the voluntary corrective measure were modified to eliminate the onsite solidification of waste. The remedy was implemented in 2003 (LANL 2003i). The Voluntary Corrective Measure Report for SWMU 21-011(k) was submitted to NMED on October 31, 2003, and approved by NMED on August 9, 2005.

I.2.7.7 Technical Area 35 (Middle Mortandad–Ten Site Canyon Aggregate Area)

TA-35 (Ten Site) is used for nuclear safeguards research and development; reactor safety research; optical science and pulsed-power system research; and metallurgy, ceramic technology, and chemical plating activities. TA-35 is on a finger mesa between Mortandad Canyon and Ten Site Canyon within the Mortandad Canyon Watershed.

Contaminants have been released from outfalls, air stack emissions, and cooling water and septic system discharges. From 1951 until 1963, the wastewater treatment facility discharged effluent into Ten Site Canyon. Spills occurred from leaks in pipelines, structures, and container storage areas. Potential contaminants include metals, PCBs, volatile organic compounds, and radionuclides (NMED 2005).

On March 29, 2002, a Sampling and Analysis Plan (LANL 2002e) was submitted that integrated most of the PRSs into one aggregate. Originally 102 PRSs were within TA-35. Fifty-four PRSs were SWMUs and 48 were AOCs. Of the 102 PRSs, 32 have been recommended or approved for no further action, leaving 70 PRSs, of which 65 will be investigated.²⁹ The PRSs addressed in the Sampling and Analysis Plan are listed in **Table I–24**, where the first column indicates whether the PRS is part of a consolidated unit and the second column indicates the PRS number. The third column describes the PRS, while the fourth column describes the subarea within TA-35 within which the PRS is located (LANL 2002e).

Table I–24 Potential Release Sites Considered in the Middle Mortandad–Ten Site Aggregate Sampling and Analysis Plan

| <i>Consolidated Unit</i> | <i>Potential Release Site</i> | <i>Potential Release Site Description</i> | <i>Subarea within the Aggregate</i> |
|--------------------------|-------------------------------|---|-------------------------------------|
| | 35-002 | MDA X | Mesa top |
| 35-003(a)-99 | 35-003(a) | Wastewater Treatment Facility | Mesa top |
| | 35-003(b) | Wastewater Treatment Facility | Mesa top |
| | 35-003(c) | Wastewater Treatment Facility | Mesa top |
| 35-003(d)-00 | 35-003(d) ^a | Wastewater Treatment Facility | Pratt Canyon |
| 35-003(a)-99 | 35-003(e) ^a | Wastewater Treatment Facility | Pratt Canyon |
| | 35-003(f) | Wastewater Treatment Facility | Mesa top |
| | 35-003(g) | Wastewater Treatment Facility | Mesa top |
| | 35-003(h) | Wastewater Treatment Facility | Mesa top |
| 35-003(j)-99 | 35-003(j) | Wastewater Treatment Facility | Mesa top |
| | 35-003(k) | Wastewater Treatment Facility | Mesa top |
| 35-003(d)-00 | 35-003(l) ^a | Wastewater Treatment Facility | Pratt Canyon |
| 35-003(a)-99 | 35-003(m) | Wastewater Treatment Facility | Mesa top |
| | 35-003(misc) | Industrial waste lines | Mesa top |
| | 35-003(n) | Wastewater Treatment Facility | Mesa top |
| | 35-003(o) | Wastewater Treatment Facility | Mesa top |
| | 35-003(p) | Wastewater Treatment Facility | Mesa top |
| 35-003(d)-00 | 35-003(q) ^a | Wastewater Treatment Facility | Pratt Canyon |
| | 35-003(r) | Outfall | Pratt Canyon |
| | 35-004(a) | Storage areas | Mesa top |
| | 35-004(b) | Storage areas | Mortandad slope |
| 25-004(g)-00 | 35-004(g) | Container storage area | Ten Site slope |
| | 35-004(h) | Container storage area | Mesa top |
| 35-014(g)-00 | 35-004(m) | Container storage area | Ten Site slope |
| 35-008-00 | 35-008 | Surface disposal and landfill | Mortandad Slope |

²⁹ PRSs 35-013(a), 35-013(b), 35-013(c), 35-006(g), and 35-016(h) are not being investigated in the Sampling and Analysis Plan because they are outside the watershed aggregate boundary or are within active buildings and have been deferred until decommissioning occurs (LANL 2002e).

| Consolidated Unit | Potential Release Site | Potential Release Site Description | Subarea within the Aggregate |
|--------------------------|-------------------------------|---|-------------------------------------|
| | 35-009(a) | Septic system | Ten Site slope, mesa top |
| 35-004(g)-00 | 35-009(b) | Septic system | Ten Site slope, Ten Site Canyon |
| | 35-009(c) | Septic system | Mortandad slope |
| | 35-009(d) | Septic system | Pratt Canyon |
| | 35-009(e) | Septic system | Ten Site slope |
| 35-010(a)-99 | 35-010(a) | Sanitary lagoon | Ten Site Canyon |
| | 35-010(b) | Sanitary lagoon | Ten Site Canyon |
| | 35-010(c) | Sanitary lagoon | Ten Site Canyon |
| | 35-010(d) | Sand filters | Ten Site Canyon |
| | 35-010(e) | Release from sand filter | Ten Site Canyon |
| | 35-011(d) | Underground storage tank | Mesa top |
| | 35-014(a) | Operational release | Mesa top |
| 35-003(j)-99 | 35-014(b) | Leaking drum | Mesa top |
| | 35-014(d) | Operational release | Mesa top |
| | 35-014(e) | Oil spill | Mortandad slope |
| 35-008-00 | 35-014(e) | Oil spill | Mortandad slope |
| 35-016(i)-00 | 35-014(e2) | Oil spill | Mortandad slope |
| | 35-014(f) | Soil contamination | Mesa top |
| 35-014(g)-00 | 35-014(g) | Soil contamination | Ten Site slope |
| | 35-014(g2) | Soil contamination | Ten Site slope |
| | 35-014(g3) | Soil contamination | Ten Site slope |
| | 35-015(a) | Soil contamination | Mesa top |
| 35-003(j)-99 | 35-015(b) | Waste oil treatment | Mesa top |
| 35-016(a)-00 | 35-016(a) | Drains and outfalls | Ten Site slope |
| | 35-016(b) | Outfall | Ten Site slope |
| 35-016(c)-00 | 35-016(c) | Outfall | Ten site slope |
| | 35-016(d) | Outfall | Ten site slope |
| | 35-016(e) | Outfall | Mortandad slope |
| | 35-016(f) | Storm drain | Mortandad slope |
| 35-016(i)-00 | 35-016(i) | Drains and outfalls | Mortandad slope |
| | 35-016(j) | Storm drain | Ten Site slope |
| 35-016(k)-00 | 35-016(k) | Drains and outfalls | Pratt Canyon |
| | 35-016(l) | Storm drain | Pratt Canyon |
| | 35-016(m) | Drains and outfalls | Pratt Canyon |
| 35-014(g)-00 | 35-016(n) | Storm drain | Ten Site slope |
| | 35-016(o) | Drains and outfalls | Mortandad slope |
| | 35-016(p) | Outfall | Mortandad slope |
| 35-016(a)-00 | 35-016(q) | Drains and outfalls | Ten Site slope |
| | 35-017 | Steam blowoff outfall from reactor | Ten Site slope |
| | 35-018(a) | Transformer | Mesa top |
| | C-35-007 | Soil contamination | Ten Site Canyon |

MDA = material disposal area.

^a These potential release sites are consolidated with mesa top potential release sites but also have a canyon component.

Among the PRSs in Table I–24 is MDA X (PRS 35-002) near the southeast corner of Building TA-35-2 on the south side of Ten Site Mesa. MDA X is the former site of the reactor from the Los Alamos Power Reactor Experiment No. 2 (LAPRE-II). After being decommissioned in 1959, the reactor was buried in place. But in 1991, MDA X was remediated as an interim action. MDA X was recommended for no further action in the Addendum to the Operable Unit 1129 RFI Work Plan (LANL 1999b).

NMED approved the sampling and analysis plan on June 9, 2003. A supplemental sampling and analysis plan addressing the remaining sites in the Middle Mortandad-Ten Site Canyon Aggregate Area was submitted to NMED on March 31, 2004, and approved on June 29, 2004. The sampling and analysis plan, and supplement, was implemented and the Investigation Report for the Middle Mortandad-Ten Site Canyon Aggregate Area was submitted to NMED in September 2005. Additional investigations for the Middle Mortandad-Ten Site Canyon Aggregate Area are ongoing.

I.2.7.8 Technical Area 49: Areas 5, 6, and 10

The Consent Order requires additional investigation of potential contamination at Areas 5, 6, and 10 within TA-49. Details about the activities conducted in these areas, the likely contamination present, their current configurations, and past investigations are discussed in Section I.2.5.3.

I.2.7.9 Solid Waste Management Unit 53-002 (a and b): Impoundments

SWMU 53-002(a) includes two impoundments (northeast and northwest), each 210 by 210 by 6 feet deep (64 by 64 by 1.8 meters deep), that were built in 1969 and received sanitary, radioactive, and industrial wastewater from TA-53 facilities. The impoundments occasionally overflowed to a channel draining east into a tributary of Los Alamos Canyon. A third impoundment (southern impoundment, SWMU 53-002(b)) was built in 1985 and measured 305 by 148 by 6 feet deep (98 by 45 by 1.8 meters deep). In 1989, the southern impoundment was restricted to radioactive liquids, while the other two impoundments received sanitary wastewater. All three impoundments are now inactive. As part of an interim action, the sludge and liners were removed from all three impoundments, and characterization samples were collected from the perimeter around each impoundment and from drainage channels leading from the southern impoundment (NMED 2005). The investigation and remediation report for the impoundments was submitted to NMED on January 29, 2004, and approved on July 25, 2006. NMED issued a Certificate of Completion on September 13, 2006.

I.2.7.10 Solid Waste Management Unit 73-001 (a-d) and 73-004 (d): Airport Landfill

The Airport Landfill consists of 5 SWMUs: a main landfill (73-001(a)), a waste oil pit (73-001-b)), bunker debris pits (73-001(c)), a debris disposal pit (73-001(d)), and a septic system (73-04(d)). DOE began operations in 1943. Trash collected from the townsite and from other locations was burned on the edge of a hanging valley. Burning continued until 1965, when Los Alamos County assumed operation. Operation ceased on June 30, 1973. From 1984 to 1986, the western portion of the landfill was removed and taken to the debris disposal pit. This allowed construction of airport hangers and tie-down areas (LANL 2001b, NMED 2005). RFI activities

occurred between 1994 and 1997 (LANL 1992e). An RFI report was submitted to NMED, and NMED agreed with the proposed remedy on December 8, 1999 (NMED 2005).

The Sampling and Analysis Plan for the Airport Landfill disposal areas describes the main landfill as covering 12 acres (4.9 hectares) and having a volume of 489,500 cubic yards (374,000 cubic meters). The west and south sides of the main landfill coincide with the edges of the asphalt tie-down area and the asphalt taxiway. The north site extends roughly to the chain-link security fence along the north side of the airport, and the east side extends to the end of the hanging valley. The debris disposal area consists of two, roughly parallel trenches dug to a maximum depth of 35 feet (11 meters). The debris disposal area covers 5 acres (2.0 hectares) and has a volume of 126,000 cubic yards (96,000 cubic meters) (LANL 2001e).

Subsequently, data needed to design a final cover for the landfill were collected, and an interim measure removed debris from landfill drainages. A closure recommendation was issued in June 2005. The preferred alternative is to leave the waste in place and install a MatCon (Modified Asphalt Technology for Waste Containment) asphalt cover and retaining wall at the main landfill and an evapotranspiration cover at the debris disposal area (LANL 2005i, DOE 2005b).

I.2.7.11 Solid Waste Management Unit 73-002: Incinerator Ash Pile

SWMU 73-002 is an ash pile from a former incinerator at TA-73. The ash pile is next to the Los Alamos County Airport. The incinerator equipment and stack were removed before 1973. An ash and surface disposal area is on the north-facing slope below the canyon rim (NMED 2005). The pile is several hundred feet northwest of the airport. The pile is 150 feet (46 meters) wide and 150 feet (46 meters) below the mesa top (LANL 2005e). RFI activities were conducted in 1996 and 1997. The RFI results were submitted in 1997 to NMED in a Phase II sampling and analysis plan. The plan was approved on February 28, 2000 (NMED 2005).

The Consent Order requires investigations to fully characterize the extent of contamination and the potential for migration of contaminants through fractures (NMED 2005). The investigation and corrective action work plan for SWMU 73-002 was submitted to NMED in May 2005 and approved in September 2005. Remediation of the ashpile is now complete and the Investigation Report for Consolidated Unit 73-002-099 and Corrective Action of Solid Waste Management Unit 73-002 at Technical Area 73 was submitted to and approved by NMED (LANL 2008a).

I.2.8 Additional Material Disposal Areas

MDAs in this section will be addressed as part of the aggregate area investigations.

I.2.8.1 Technical Area 8: Material Disposal Area Q

Also known as the GT or Anchor West Site, TA-8 is at the western end of LANL and is used for dynamic tests. MDA Q is within a 0.2-acre (0.8-hectare) site on Pajarito Mesa, in an area called the Gun-Firing Site (PRS 8-002), which once contained naval guns used to develop the Little Boy atomic weapon. Two concrete anchor pads for the gun mounts and two target sand butts remain (LANL 1999b).

MDA Q is a burial ground (SWMU 8-006(a)) that received waste in 1946 from the naval gun experiments, possibly including parts from Little Boy tests (LANL 2005c). The MDA occupies an irregularly shaped area having dimensions of 270 by 260 feet (81 by 78 meters) (LANL 1999b). Within this area, burial occurred in a pit of uncertain size. Investigations in the early 1990s suggested a size of 30 by 30 feet (9.1 by 9.1 meters) (LANL 1993d). Later investigations indicated that the disposal area covered a larger area (LANL 1993d). The MDA Core Document cites a 0.2-acre (0.8-hectare) area (LANL 1999b).

Radioactive contamination was absent in a gun mount unearthed in 1947. In 1994, copper and lead were found above background values in surface soil samples. No radioactive contamination was found (LANL 2005c).

I.2.8.2 Technical Area 9: Material Disposal Area M

TA-9 (Anchor East Site) is on the western edge of LANL. The site is used for explosives research. MDA M is on Pajarito Mesa southwest of Pajarito Canyon. MDA M (SWMU 09-013) consists of a 3.2-acre (1.3-hectare) circular surface MDA and a small disposal area 750 feet (229 meters) northwest. The main disposal area is surrounded by an earth berm that is eroded from surface runoff. MDA M was a dump for construction debris and other wastes. From 1960 through 1965, the site received nonhazardous wastes from construction at other sites. MDA M has been inactive since 1965 (LANL 2005c).

In 1996, all wastes were removed and the site surveyed. Twenty-six verification samples were analyzed for organic and inorganic chemicals, radionuclides, PCBs, and asbestos. All contaminants were either not detected or were below recommended cleanup levels. The site access road was regraded and revegetated, and the main disposal area was scarified, graded, tiered, and seeded to control soil movement and erosion. The report for the 1996 expedited cleanup recommended no further action (LANL 2005c).

I.2.8.3 Technical Area 15: Material Disposal Area N

MDA N (SWMU 15-007(a)) is within a 0.28-acre (0.11-hectare) site within TA-15. MDA N is a pit containing remnants of structures from R Site that had been exposed to explosive or chemical contamination. (If radioactive contamination is present, it is probably at a low level given nearby office buildings.) The MDA is shown in the RFI Work Plan for Operable Unit 1086 work plan as a 30- by 290-foot (9.1- by 88-meter) rectangle (LANL 1993c). A later report estimated the size as 300 by 100 feet (91 by 30 meters) (LANL 2005c). Opened in 1962, MDA N may have received waste from demolishing the control room and darkroom (Building 15-7) used to support Firing Point C (and probably D) (LANL 1993c). A 1965 aerial photograph showed it to be closed (LANL 2005c). The pit is covered and vegetated (LANL 1999b).

Little is known about use of hazardous materials. A 1989 aerial survey did not find radioactive materials. Neither high explosives nor uranium were handled. It is unknown how photographic chemicals were disposed (LANL 1993c).

I.2.8.4 Technical Area 16: Material Disposal Area R

TA-16 is described in Section I.2.7.2.

MDA R (SWMU 16-019) is an 11.5-acre (4.7-hectare) site on the edge of the mesa on the south side of Cañon de Valle. It is north of the explosives processing facility (Building 260). MDA R is an high explosive burning ground and disposal area that was used from 1945 until 1951. The MDA covers an area of 600 by 900 feet (180 by 270 meters), although the contaminated area is probably smaller (LANL 1999b).

A later document (LANL 2005c) reports an area of 2.27 acres (0.92 hectare). The MDA consists of three U-shaped, 75-square-foot (7.0-square-meter) bermed pits that were fenced and encircled by a road (LANL 1993f). During construction of the 260 Line, the berms and surface soil were graded northward into Cañon de Valle. Debris was pushed northward over the edge of the burning ground toward the canyon floor. Debris was held back by a natural barrier of wood and tress created by clearing the area for Building 16-260 in 1951. The area was covered with grasses and pine trees before the 2000 Cerro Grande Fire. Suspected contaminants are barium, high explosive, lead, asbestos, and organic chemicals (LANL 2005c). A geophysical survey suggests that the depth of waste at MDA R is shallow (LANL 1999b).

After the Cerro Grande Fire, 800 cubic yards (611 cubic meters) of clean soil was excavated and staged, as well as 1,500 cubic yards (1,147 cubic meters) of contaminated soil and debris. A runon diversion channel was built and erosion-control materials installed. The MDA was sampled in September 2000 to determine the nature and extent of contamination (LANL 2005c).

I.2.8.5 Technical Area 33: Material Disposal Areas D, E, and K

TA-33 (Hot Point Site) is near the southeast boundary of LANL. It spans the boundary of the Chaquehui Canyon and Ancho Canyon Watersheds. TA-33 was used from 1947 to perform experiments in underground chambers, on surface firing pads, and at firing sites where guns shot projectiles into berms. Weapons experiments ceased in 1972. A high-pressure tritium facility operated from 1955 until late 1990 (LANL 1999b). The TA is used for experiments that require isolation or do not need daily oversight.

I.2.8.5.1 Material Disposal Area D

MDA D (SWMUs 33-003(a) and (b)) is on the east end of the TA. MDA D consists of two underground chambers: TA-33-4 (SWMU 33-003(a)) and TA-33-6 (SWMU 33-003(b)). Built in 1948, the chambers were octagonal (18 by 18 by 11 feet high [5.5 by 5.5 by 3.4 meters high]), with the tops of the chambers 30 feet (9.1 meters) below grade. Access was via a 46-foot-deep (14-meter-deep) elevator shaft (Rogers 1977). The chambers were used for initiator tests using polonium-210 (138-day half-life), milligram quantities of beryllium, and large quantities of high explosive. Chamber TA-33-4 was used once in 1948. Chamber TA-33-6 was used in 1948 and April 1952. The second test destroyed the chamber. Debris ejected into the air spread over the mesa. The crater around the chamber was filled with recovered debris and covered with soil (LANL 1999b).

The Rogers report summarizes information indicating that the underground chambers may be contaminated with explosive residue, uranium-235, and possibly trace amounts of other uranium isotopes, polonium, and cobalt-60 (Rogers 1977).

A 1995 Phase I RFI report for the MDA recommended no further action for SWMU 33-003(a) because no release to the environment was apparent. A 1997 Phase I report recommended no further action for SWMU 33-003(b). The report recommended deferring evaluating ecological risks until a risk method had been developed (LANL 2005c).

I.2.8.5.2 Material Disposal Area E

On the south edge of the TA, MDA E is on a point formed by Chaquehui Canyon and one of its tributaries. Consolidated Unit 33-001(a)-99 (MDA E) consists of four waste disposal pits (SWMUs 33-001(a) through (d)) and an underground test chamber and shaft (SWMU 33-001(e)). The test chamber and shaft were last used in 1950, and the disposal pits ceased receiving waste in 1963. The consolidated unit covers 140 by 220 feet (43 by 67 meters) and is fenced (LANL 2005c). The four pits³⁰ have the following dimensions, based on contemporary engineering drawings (LANL 2005c):

- 33-001(a): 20 by 60 feet (6.1 by 18 meters);
- 33-001(b): 20 by 50 feet (6.1 by 15 meters);
- 33-001(c): not determined; and
- 33-001(d): 20 by 100 feet (6.1 by 30 meters).

The pits are probably shallow, each about 6 to 7 feet (1.8 to 2.1 meters) deep (Rogers 1977).

All four pits contain beryllium and uranium. A report by the U.S. Geological Survey referenced by Rogers (Rogers 1977) states that the area contains several hundred kilograms of depleted uranium. Pits 1 and 2 were reported to contain 240 curies and 60 curies, respectively. Pits 1 and 2 may contain hazardous wastes (LANL 1999b). Pit 3 contains a can of beryllium dust immersed in kerosene. Dates of construction cannot be confirmed. When disposal ceased in 1963, the pits were filled and compacted (LANL 2005c).

The underground chamber and shaft were built from November 1949 to February 1950. The octagonal chamber was 14 feet (4.3 meters) wide and 11 feet (3.4 meters) high and had concrete walls, floor, and ceiling. The adjacent shaft was 48 feet (15 meters deep). The chamber was used to conduct tests using explosives, beryllium, and tungsten. The chamber collapsed during an April 1950 experiment and was abandoned (LANL 2005c).

Sampling programs in 1982 and 1983 found tritium, cesium-137, and uranium. The RFI work plan indicated that subsurface contaminants were not being released from the pits and chamber (LANL 2005c).

I.2.8.5.3 Material Disposal Area K

MDA K (Consolidated Unit 33-002(a)-99) is in the northern part of the TA. The consolidated unit is in an unfenced area comprising a 3-acre (1.2-hectare) footprint (LANL 2005c). The six SWMUs composing the consolidated unit have a smaller footprint. The RFI Work Plan for Operable Unit 1122 estimates a size of 1 acre (0.4 hectare) (LANL 1992f). All former SWMUs

³⁰ Two additional pits were constructed but were backfilled, apparently without being used for waste disposal. Rogers (Rogers 1977) reports slightly different dimensions for the pits, based on a contemporary engineering drawing: Pit 1 = 15 by 75 feet (4.6 by 23 meters); Pit 2 = 15 by 45 feet (4.6 by 14 meters); Pit 3 = 5 feet (1.5 meters) in diameter; Pit 4 = 15 by 100 feet (4.6 by 30 meters).

are associated with the Tritium Facility (Building 33-86), which operated from June 1955 until 1990. The former SWMUs consist of a septic system (SWMU 33-002(a)), two sumps (SWMUs 33-002(b) and -002(c)), an outfall (SWUM 33-002(d)), a roof drain (SWMU 33-002(e)), and a surface disposal area (SWMU 33-002(f)) (LANL 2005c). SWMUs (33-002(a-e)) were remediated in 2005 as part of an accelerated corrective action at TA-33. The remedy completion report for this accelerated corrective action was submitted to NMED on March 2, 2006, and was approved with a Certificate of Completion on August 31, 2006.

The history and origins of waste within the surface disposal area (33-010(f)) are unknown. The surface disposal area comprises two groups of debris at the southeast corner of the MDA. One group of debris is 15 feet (4.6 meters) square, and it is 50 feet (15 meters) from a second 10- by 20-foot (3.0- by 6.1-meter) group of debris. Materials include pieces of concrete and concrete culvert, piles of tuff and cured asphalt, rusted metal cans, rebar, strapping bands, and other debris (LANL 2005c).

I.3 Description of Options

I.3.1 Overview of Options

To predict the impacts of carrying out future corrective measure decisions, three broad-scope options are considered for purposes of NEPA:

1. **No Action Option.** Environmental investigations and restoration efforts are assumed not to be carried out in accordance with the Consent Order. The LANL environmental restoration project would continue at a pre-Consent Order level, but no extensive corrective measures would be conducted for major PRSs.
2. **Capping Option.** The Consent Order would be implemented. For this appendix it was assumed that environmental investigations would take place in accordance with the Consent Order, LANL MDAs would be stabilized in place, and several other PRSs would be remediated annually.

The No Action Option is considered in this appendix because such an action is required by NEPA. DOE is legally required to carry out the provisions of the Consent Order.

Stabilizing MDAs in place means placing final covers over them and conducting certain other environmental restoration activities such as remediating the volatile organic compound plumes existing in soil at some MDAs. The General's Tanks within MDA A would be stabilized in place using a grout mixture. Transuranic waste in subsurface storage at MDA G would be removed, processed, and shipped to WIPP. Because a small volume of the stored transuranic waste in subsurface shafts within MDA G may be difficult to retrieve, an option to leave this stored waste in place would be considered. If this option were pursued, a performance assessment pursuant to 40 CFR Part 191 may be required. If such an assessment is required, the assessment results may indicate the need for additional waste stabilization or MDA final cover modification.

Remediating additional PRSs would include contamination removal at sites such as Firing Sites E-F and R-44 and the 260 Outfall. Other remediation activities could include

surge bed grouting, contaminated sediment natural flushing, use of permeable reactive barriers, pump and treat system installation, or other measures.

For MDAs A, B, T, U, C, L, G, and AB, it was assumed that remediation would be completed by the dates presented in Table I-2. For other MDAs and PRSs, it was assumed that remediation would be completed in compliance with appropriate Consent Order schedules, including those for aggregate areas. It was assumed that remediation of these MDAs and PRSs would occur from FY 2007 through FY 2016.

- 3. Removal Option.** The Consent Order would be implemented. For this appendix it was assumed that environmental investigations would take place as they would for the Capping Option. In addition, LANL MDA waste and contamination would be removed. All transuranic waste stored at MDA G would be removed and shipped to WIPP along with all other transuranic-contaminated material disposed of before 1970. Remediation of additional PRSs would again occur by various methods as discussed for the Capping Option. Remediation of MDAs or PRSs was assumed to be completed by the same dates assumed for the Capping Option.

The projected annual waste volumes and other environmental impacts are conservative. If extensive removal of waste and contamination from the MDAs were required, then for a variety of programmatic, funding, safety, and regulatory compliance reasons, the remediation process may extend beyond FY 2016, provided that a revised schedule is approved by NMED. If this were to occur, annual waste volumes and other impacts associated with the Removal Option would be smaller.

Environmental impacts associated with these three options are expected to bound those that could result from eventual implementation of MDA and PRS corrective actions. Remediation decisions will be made for specific MDAs and PRSs rather than groups, and may prescribe a combination of corrective measures. For example, some waste within an MDA may be removed and the remainder may be stabilized in place.

For all options, appropriate safety and environmental surveillance and maintenance would continue at LANL to maintain compliance with DOE and external criteria and standards, including those for nuclear environmental sites (Section I.3.2.3).

I.3.2 Continuing Environmental Restoration Work

Since LANL's environmental restoration project was established in 1989, progress has been made in characterizing and remediating LANL PRSs. Some of the numerous environmental investigations conducted by LANL have generated solid and liquid wastes. Additional wastes have resulted from implementing corrective measures. Projections of future waste generation are difficult. One reason is that waste generation rates depend on regulatory decisions yet to be made that would establish the scope of specific environmental restoration activities. Because the kinds of investigations conducted under the Consent Order will be basically the same as those previously performed (for example, well drilling), it was assumed that waste from environmental investigations would be encompassed by those in existing LANL forecasts (see Section I.3.2.1).

I.3.2.1 Existing Waste Forecasts

Estimates of waste generation from LANL’s environmental restoration project were presented in the 1999 *Site-Wide Environmental Impact Statement for Continued Operation of the Los Alamos National Laboratory, New Mexico (1999 SWEIS)* (DOE 1999a). Updated projections are in the August 17, 2004, *Information Document in Support of the Five-Year Review and Supplement Analysis for the Los Alamos National Laboratory Site-Wide Environmental Impact Statement (DOE/EIS-0238)* (LANL 2004f). The 2004 LANL information document provides 10-year forecasts of radioactive and nonradioactive waste generation at LANL. These forecasts are in two parts:

- Forecasts of wastes from several LANL sources, including the environmental restoration project and LANL operations. The forecasts are derived from a June 2003 report (LANL 2003c) that was attached to the 2004 LANL information document (LANL 2004f) as Appendix G.
- Forecasts of waste from a separate decontamination, decommissioning, and demolition (DD&D) project that would generate wastes from demolishing several LANL structures (LANL 2004f).

The focus of this appendix is on waste that could be generated from LANL’s environmental restoration project.³¹ Projections of environmental restoration project waste from the June 2003 report (LANL 2003c) as updated for years 2006 through 2008 by a subsequent report (LANL 2004i), are presented in **Table I–25** for FYs 2006 through 2012. For transuranic waste and mixed transuranic waste, the revised forecast projected an annual minimum of 52 cubic yards (40 cubic meters) of transuranic waste and an annual maximum of 105 cubic yards (80 cubic meters) of transuranic waste (LANL 2004i). The larger estimate is reflected in the table.

Table I–25 Projections of Los Alamos National Laboratory Environmental Restoration Project Wastes from Fiscal Year 2006 through Fiscal Year 2012

| Waste | Fiscal Year | | | | | | |
|---|-------------|-------|-------|-------|------|------|------|
| | 2006 | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 |
| Chemical - hazardous waste ^a (tons) | 7,591 | 1,644 | 1,165 | 162.7 | 0 | 38.4 | 27.6 |
| Low-level radioactive waste (cubic yards) | 1,295 | 989 | 3,640 | 4,175 | 31 | 0 | 0 |
| Mixed low-level radioactive waste (cubic yards) | 6.5 | 129 | 196 | 20 | 0 | 303 | 89 |
| Transuranic waste (cubic yards) | 100 | 100 | 100 | 0 | 0 | 0 | 0 |

^a Resource Conservation and Recovery Act (RCRA) waste, Toxic Substances Control Act (TSCA) waste, New Mexico State special solid waste, and waste not otherwise suitable for sanitary landfill disposal.

Note: To convert cubic yards to cubic meters, multiply by 0.76456; tons to metric tons, multiply by 0.90718.

Sources: LANL 2003c, 2004i.

The Consent Order requires the investigation and remediation of numerous potential release sites and areas of concern. Implementing the Consent Order may cause generation of larger quantities

³¹ Wastes potentially generated from DD&D of LANL structures are addressed in Appendix H, Section H.1, for structures in TA-18 and in Section H.2 for structures in TA-21. Waste estimates from recovery and shipment of stored transuranic waste at Area G of TA-54 are addressed in Section H.3. Waste estimates from combined LANL sources are addressed in the main body of this SWEIS.

of environmental restoration waste than previously projected. Because investigations are ongoing and many corrective action decisions remain to be made, it is not possible to precisely define the types and quantities of wastes that would be generated from actions taken under the Consent Order. Bounding estimates were therefore made.

It was assumed that MDAs A, B, T, U, AB, C, G, and L would be remediated in conformance with their remedy completion report due dates.³² For other MDAs, it was assumed that their remediation would start in FY 2007 and continue through FY 2016. Total quantities of wastes that may be generated under each option (capping or removal) were estimated and averaged from FY 2007 through FY 2016. For the remaining PRSs, waste generation rates from some representative PRSs were estimated, and an average annual waste generation rate was assumed starting in FY 2007 and continuing through FY 2016. This waste was added to that projected in Table I-25.

The waste types assumed for this appendix are listed in **Table I-26**. Nonliquid wastes are grouped into four types: solid waste, chemical waste, low-level radioactive waste, and transuranic waste. Solid waste refers to solid waste suitable for disposal into a solid waste landfill. Chemical waste is meant to be a general description for chemical or hazardous wastes that contain hazardous constituents regulated under RCRA or TSCA, are regulated as a special waste by the State of New Mexico pursuant to the New Mexico Solid Waste Act of 1990, or otherwise fail to meet waste acceptance criteria for sanitary landfill burial.

Table I-26 Waste Types Considered

| <i>Waste Types</i> | <i>Waste Subtypes</i> |
|---|-----------------------|
| Nonliquid Wastes | |
| Solid waste | – |
| Chemical waste | – |
| Low-level radioactive waste | Low-activity |
| | Mixed low-activity |
| | Alpha |
| | Mixed alpha |
| | Remote-handled |
| | Mixed remote-handled |
| Transuranic waste and mixed transuranic waste | Contact-handled |
| | Remote-handled |
| Liquid Wastes | |
| Industrial | – |
| Hazardous | – |
| Radioactive | Low-level |
| | Mixed low-level |

Low-level radioactive waste was assumed to be radioactive waste that is not high-level radioactive waste, spent nuclear fuel, transuranic waste, byproduct material (as defined in Section 11e(2) of the Atomic Energy Act of 1954, as amended), or naturally occurring

³² This assumption is conservative for MDA U because NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (see Section I.2.5.2.4 of this appendix).

radioactive material. Low-level radioactive waste was divided among six subtypes. This distinction was made to enable assessment for transportation impacts in this appendix and was not meant to represent official DOE waste classifications.

Low-activity low-level radioactive waste contains radionuclides in concentrations that do not exceed the Class A limits of 10 CFR Part 61 and have surface radiation levels smaller than 200 millirem per hour. Mixed low-activity low-level radioactive waste has similar radioactive properties but also meets the definition of RCRA hazardous waste. Alpha low-level radioactive waste contains alpha-emitting transuranic isotopes in concentrations between 10 and 100 nanocuries per gram; this waste is assumed to be contact-handled. Mixed alpha low-level radioactive waste is similar radiologically but also meets the definition of RCRA hazardous waste. Mixed remote-handled low-level radioactive waste has surface radiation levels that exceed 200 millirem per hour. Much of this waste may also exceed Part 61 Class A limits. Mixed remote-handled low-level radioactive waste is similar material but also meets the definition of RCRA hazardous waste.³³

Transuranic waste is not separated into mixed and nonmixed subgroups. Both mixed and nonmixed transuranic waste can be shipped directly to WIPP, provided that wastes having the RCRA characteristics of ignitability, corrosivity, or reactivity are treated. Transuranic waste is separated into contact-handled and remote-handled transuranic waste, where remote-handled transuranic waste containers have surface radiation levels exceeding 200 millirem per hour.

Liquid wastes would be generated in small volumes; for example, from equipment decontamination. Liquid low-level radioactive waste contains small concentrations of radioactive isotopes regulated by DOE under the Atomic Energy Act of 1954. Mixed low-level radioactive liquid waste is similar in radioactive properties but also meets the definition of RCRA hazardous waste. Hazardous liquid waste meets the definition of RCRA hazardous waste. Industrial liquid waste is process water that does not meet the definition of hazardous waste.

I.3.2.2 Investigations

The Consent Order requires investigations to fully characterize the nature, extent, fate, and transport of contaminants that have been released to air, soil, sediment, surface water, and groundwater. For example, the investigations of the canyon watersheds must address canyon alluvial sediments, surface water monitoring and sampling, and groundwater monitoring and sampling, focusing on the fate and transport of contaminants from the point of origin to each canyon watershed drainage system, and, if necessary, to the regional aquifer and the Rio Grande. The Consent Order requires the construction of new wells, the abandonment of some existing wells, and environmental sampling. Newly constructed wells include alluvial wells, intermediate wells, and regional aquifer wells. Requirements for specific LANL TAs are often prescribed in terms of individual MDAs. The investigations for each MDA must typically include a survey of disposal units, drilling explorations, soil and rock sampling, sediment sampling, vapor monitoring and sampling, intermediate and regional aquifer groundwater well installation, and

³³This grouping of different low-level radioactive waste subtypes contains simplifications. For example, some alpha-low-level radioactive wastes may require remote handling. However, there is insufficient information for further meaningful subgroupings.

groundwater monitoring (NMED 2005). These investigations would involve similar if not identical technologies that have long been used at LANL.

Investigations of PRSs must be conducted in accordance with work plans to be submitted to and approved by NMED. Investigations for most PRSs will be conducted in accordance with work plans for the aggregate areas containing these PRSs, and the details of the work plans will depend on the known and inferred characteristics of the PRSs within each aggregate area. Three example work plans are those addressing the DP Site Aggregate Area at TA-21 (LANL 2004e); the Guaje, Barrancas, Rendija Canyons Aggregate Area at the townsite (LANL 2005j); and the Pueblo Canyon Aggregate Area (LANL 2005g). The objectives of the work plans are to characterize the nature and extent of contamination, if any, and to determine the need for corrective action. Investigations may include (but are not necessarily limited to) geodetic and geophysical surveys, radiological surveys, surface and near-surface soil sampling, sampling soil and tuff from boreholes, and confirmation sampling of soil or tuff after conducting a remedial action. A phased approach will be used that will be tailored to each PRS, including site reconnaissance, screening, characterization, excavation, confirmation sampling, and evaluation of survey screening and sample data. This approach allows for acquisition of confirmation data and review of results before demobilizing the investigation program for that PRS.

In May 2005, LANL staff submitted an Interim Facility-Wide Groundwater Monitoring Plan to NMED. Four modes of water will be monitored: base flow, alluvial groundwater, intermediate perched groundwater, and regional aquifer groundwater. Monitoring within LANL boundaries will take place in seven major watersheds or water shed groupings. Monitoring outside LANL boundaries will be conducted in areas that LANL operations have affected, and, to provide baseline information, areas that LANL operations have not affected. Monitoring data will be reported in accordance with Consent Order schedules (LANL 2006h).

Any investigation-derived waste generated during the site investigation process will be managed in accordance with all applicable EPA and NMED regulations, DOE orders, and LANL implementation requirements. Investigation-derived waste may include drill cuttings, contaminated personal protective equipment, sampling supplies, plastic, and decontamination fluids. Some field investigations may also displace environmental media such as groundwater, surface water, surface and subsurface soils, rocks, bedrock, and gravel.

I.3.2.2.1 Well Installation

Exploratory and monitoring well borings must be drilled using the most effective, proven, and practicable method for recovery of undisturbed samples and potential contaminants. Methods to be used must be approved by NMED (NMED 2005). Monitoring wells are typically constructed by advancing a boring with a drilling rig, installing a well casing and screen, and backfilling the annulus between the casing and the wall of the borehole (Hudak 1996). Based on drilling conditions, the borings may be advanced using one of the following methods: hollow-stem auger, air rotary, mud rotary, percussion hammer, sonic, dual-wall air rotary, direct-push technology, cryogenic, and cable tool. Drilling techniques will be selected and used that minimize collateral disturbance and investigation-derived waste. NMED prefers hollow-stem auger or direct-push technology drilling methods if vapor-phase or volatile organic compound

contamination is known or suspected. Air rotary drilling is preferred for borings intersecting the regional aquifer. The type of drilling fluid used must be approved by NMED (NMED 2005).

Each of these drilling methods are summarized below.

Hollow-stem auger. A hollow-stem auger may be used to install monitoring wells in unconsolidated or poorly consolidated materials, but is inappropriate for solid rock. No drilling fluids are required (Hudak 1996).

Air rotary. Rotary drilling uses circulating fluids to remove drill cuttings and maintain an open hole as drilling progresses. In the air rotary method, air is forced down the drill pipe and back up the borehole to remove drill cuttings. Air rotary is often discouraged for environmental investigations because of the difficulty of yielding representative samples (Hudak 1996).

Mud rotary. Mud rotary drilling, like water rotating drilling, requires the introduction of fluids through the drill pipe to maintain an open hole, to provide drill bit lubrication, and to remove drill cuttings. Mud rotary drilling is often used instead of water drilling when the subsurface properties make it difficult to maintain an open borehole (Hudak 1996).

Dual-wall air rotary. The dual-wall reverse-circulation rotary method employs a double-walled drill pipe. Air (or water) is forced down the outer casing and circulated up through the inner pipe. Cuttings are forced to the surface through the pipe (Hudak 1996).

Percussion hammer. This drilling technique uses compressed air to hammer a series of short, rapid blows to the drill rods or bits and also simultaneously applies a rotating motion. Drill cuttings are flushed to the surface by compressed air (TH 2005).

Sonic. Resonant sonic drilling uses a combination of mechanically generated vibrations and limited rotary power to penetrate soil. The drill head, attached to the drill pipe, uses two counter-rotating, out-of-balance rollers, causing the drill pipe to vibrate in resonance. The vibration and weight of the drill pipe, along with the downward thrust of the drill head, permit penetration of the geologic formation without adding drilling mud or lubricating fluid. The technique is adaptable to any slant angle and virtually any geologic formation and typically produces no cuttings or secondary waste streams (NCDENR 2005, CPEO 2005).

Direct-push technology. Direct-push technologies use hydraulically powered machines that drive small-diameter tools directly into the surface. This technology generates little to no investigation-derived wastes and can be mounted on relatively small vehicles, allowing for use at sites that are difficult to access and minimizing collateral disturbance to surrounding soil and vegetation (ICON 2005, Fugro 2005).

Cryogenic. Cryogenic drilling replaces ambient air with cold nitrogen liquid or gas—as cold as 320 °F (degrees Fahrenheit) (-196 °C [degrees Celsius])—as the circulating medium. The nitrogen stream freezes moisture in the ground surrounding the borehole, thus stabilizing it (DOE 1998b).

Cable tool. The cable tool drilling method uses a heavy string of drilling tools that are repeatedly lifted and dropped within a borehole. The drill bit breaks and crushes consolidated rock into

small fragments and loosens unconsolidated material. The reciprocating action of the tools mixes the crushed and loosened rock particles with water to form a slurry. A sand pump or bailer removes the slurry (Hudak 1996).

I.3.2.2.2 Well Purging

Procedures for purging monitoring wells before sampling must be approved by NMED. The Consent Order requires temporary storage of purged groundwater and decontamination water until proper characterization and disposal can be arranged. Disposal methods must be approved by NMED (NMED 2005).

I.3.2.2.3 Test Excavations

Site investigations may include test excavations, including trenches and test pits in areas of contamination. Test excavation programs have been conducted at LANL PRSs. Future test excavation programs should cause small areas of temporary surface disturbance, generally in areas such as MDAs that have already been changed from natural conditions. Test excavations will result in temporary removal, stockpiling, and return of uncontaminated soil and material, as well as generation of small volumes of waste.

I.3.2.3 Maintenance of Nuclear Environmental Sites

Some of the PRSs addressed in this appendix are nuclear environmental sites, which are inactive waste handling or disposal areas that contain sufficient radioactive material to be classified as hazard category 2 or 3 according to DOE Standard thresholds (DOE 1997b). These nuclear environmental sites are listed in **Table I–27**. LANL staff perform routine inspections and maintenance at these sites to maintain compliance with 10 CFR Part 830. LANL staff has developed a documented safety analysis for surveillance and maintenance of the sites (LANL 2004I).

Consistent with the surveillance and maintenance documented safety analysis implementation plan, all nuclear environmental sites have been initially inspected. Results of those inspections indicated the need for several actions, which are ongoing. The work elements required to address these findings fall into several distinct categories of similar actions:

- General maintenance
- Boundary marking
- Baseline radiological survey
- Erosion control studies and maintenance efforts
- New fencing

Table I-27 Hazard Categories and Descriptions of Nuclear Environmental Sites

| <i>Nuclear Environmental Site</i> ^a | <i>Associated PRS</i> | <i>Description</i> | <i>Hazard Category</i> |
|--|-----------------------|---|------------------------|
| TA-21 MDA A | 21-014 | Subsurface tanks and pits associated with historical liquid and solid waste disposal | 2 |
| TA-21 MDA B | 21-015 | Undifferentiated subsurface areas associated with historical waste disposal | 3 |
| TA-21 MDA T | 21-016(a)-99 | Shafts and absorption beds associated with liquid wastes | 2 |
| TA-35 MDA W | 35-001 | Subsurface tanks used for disposal of sodium coolant from reactor experiments | 3 |
| TA-35 Wastewater Treatment Plant | 35-003(a)-99 | Areas of residual contamination associated with leakage from, and removal of, components of former Wastewater Treatment Plant | 3 |
| TA-35 Pratt Canyon | 35-003(d)-00 | Areas of residual contamination associated with discharge from former Wastewater Treatment Plant | 3 |
| TA-49 MDA AB | 49-001(a)-00 | Shaft areas associated with historical subcritical experiments involving nuclear materials | 2 |
| TA-50 MDA C | 50-009 | Complex of pits and shafts used for disposal of combustible and noncombustible debris and sludge-filled drums | 2 |
| TA-53 Resin Tank | 53-006(b)-99 | Subsurface tank that received contaminated ion exchange resins from an accelerator facility | 2 |
| TA-54 MDA H | 54-004 | Shafts formerly used for disposal of classified waste | 3 |

PRS = potential release site, TA = technical area, MDA = material disposal area.

^a An additional site is outside the LANL boundary in Bayo Canyon.

Source: LANL 2004I.

General Maintenance. Activities may include mowing, debris clearing, foliage removal, and fence repair. Tasks such as mowing, clearing brush, removing debris, and removing small trees are performed to maintain site surface characteristics and to limit combustible materials. Equipment used includes miscellaneous hand tools and cutters, chain saws, tractors with fixed or adjustable cutting attachments, weed-line or blade trimmers, push mowers, tractors with fixed or adjustable (hydraulic) mower decks, and trucks and transport vehicles, including cherry picker hydraulic lifts. Repairing existing fences involves minor site preparation, such as light scraping and removal of vegetation. Small hand- and power tools may be used.

Boundary Marking. The disposal units that comprise the inventory driving the nuclear facility categorization are being demarcated. Activities may include general surveying, placement of posts, and placement of temporary barriers such as orange construction fencing. General surveying is usually conducted by a surveyor and assistant. Some surveying equipment (for example, tripods, survey rods) slightly intrudes into the subsurface to provide a firm base for instruments. The depth of penetration in typical soils is less than 3 inches (7.6 centimeters). Personnel use pin flags, flagging, and wooden or metal stakes to mark locations and may pound stakes 1 foot (0.3 meter) or deeper into the subsurface. General surveying may require the installation of permanent benchmarks using hand- or battery-operated rock drills to make small holes in bedrock and cementing the benchmarks in the drilled holes. To provide a clean line of sight for instrument readings, personnel may use small saws, axes, or clippers to clear brush and thin branches in areas of vegetation.

Baseline Radiological Survey. Baseline radiological surveys are being performed at several sites. The goal of a baseline survey is to establish surface radiological conditions at a specific

point in time. If future inspections indicate significant physical changes such as biodegradation, erosion, or burrowing animals, the impacts of these changes can be evaluated by performing radiological surveys in the areas of changed condition. Survey equipment includes a wide array of devices that are generally small, handheld, and self-contained. To conduct a survey, personnel may require access to radioactive storage areas; waste lagoons; areas downwind of stack release points or exhaust vents; areas near storm, septic, sanitary, or drainage systems; and areas where runoff may collect. These areas may be within or outside of nuclear environmental site boundaries. Survey personnel may work in areas of dense vegetation or rough terrain and along parking lots and roadways near traffic. Survey instruments may be mounted on all-terrain vehicles.

Erosion Control Studies and Maintenance. Erosion control measures may include installation and maintenance of check dams, straw wattles, or surface basecourse or earthen berms.

New Fencing. New fence construction can include digging holes, placing concrete, setting posts, and using a “come along” or other light equipment to stretch fencing. Personnel performing these tasks may use trucks and transport vehicles with mounted hydraulic lifts and pole drivers to install posts and lift materials; vehicle-mounted, power, or manual augers to excavate post holes; hand tools to support post and fence placement; cutting torches to cut fencing or signage materials; radiological and industrial-hygiene survey equipment; oxy-acetylene or arc welding units; or electric or pneumatic cutting drills and saws.

I.3.3 Remediation of Material Disposal Areas

The MDAs contain a variety of radionuclides or hazardous constituents within wastes that have been disposed of in pits, trenches, and shafts. To evaluate alternative corrective measures, potential corrective measure technologies would be screened to eliminate those that prove infeasible to implement, rely on technologies unlikely to perform satisfactorily or reliably, or do not achieve corrective action objectives within a reasonable time. Conceptual models would be established and the likely performance of the MDAs would be evaluated against the corrective measure objectives established for the corrective measure process.

The purpose of this section is not to preclude this screening process, but to identify a range of corrective measure technologies that might be suitable. At any MDA, a number of corrective measure technologies may be used. For example, portions of MDAs may be removed and portions may be stabilized in place. Some MDAs may require treatment of volatile organic compound plumes.

I.3.3.1 Corrective Measure Technologies Possibly Suitable for Material Disposal Areas

Corrective measure technologies continue to be developed, for example as part of DOE’s Environmental Remediation Science Program. One information source of environmental remediation technologies is the Federal Remediation Technologies Roundtables Remediation Technologies Screening Matrix and Reference Guide (FRTR 2005). Each of the MDAs presents a unique mix of challenges for remediation. Nonetheless, possible treatment technologies can be grouped as follows:

- *Stabilization in place* – containment and in situ treatment technologies
- *Removal* – excavation/removal and ex situ treatment technologies

I.3.3.1.1 Possible Containment and in Situ Treatment Technologies Associated with the Stabilization in Place Option

Contamination would be treated in situ or contained in place by installing a final cover. Possible technologies are listed in **Table I–28**.

Table I–28 Possible Technologies for Containment and in Situ Treatment

| <i>Category</i> | <i>Subcategory</i> | <i>Technology</i> |
|-------------------|----------------------------------|--|
| Containment | Vertical barriers | Slurry walls |
| | | Rock-grout mixing |
| | | Synthetic membrane |
| | Deep-surface horizontal barriers | Deep-surface horizontal barriers |
| | Near-surface horizontal barriers | Soil-grout mix |
| | | Vitrification |
| | Surface barriers | Asphalt cover |
| | | Compacted clay cover |
| | | Multilayer cover |
| | | Evapotranspiration cover |
| Biotic barriers | | |
| In Situ Treatment | Biological treatment methods | Microorganisms |
| | Physical treatment methods | Soil gas venting |
| | | Soil vapor extraction |
| | | Pneumatic fracturing |
| | | Electrokinetic soil treatment |
| | | Vitrification |
| | | Compaction with conventional equipment |
| | | Dynamic compaction |
| | | Waste stabilization |
| Thermal treatment | | |

Vertical Barriers

Vertical (lateral) barriers could be installed around the perimeters of the disposal units, including:

- *Slurry walls*. A slurry wall is formed by placing cement grout or similar materials into narrow, deep trenches or in a series of adjacent open boreholes surrounding the perimeter of a group of disposal units.
- *Rock-grout mixing*. Rock-grout barriers are formed by drilling adjacent deep shafts around the perimeter of a group of disposal units and then mixing the cut rock with injected grout as the shaft is drilled.

- *Synthetic membrane.* A geosynthetic liner or similar membrane can be placed in a vertical trench, thereby forming a barrier that impedes or restricts the lateral movement of contaminants.

These barriers are principally meant to prevent lateral movement of contaminants from disposal units. Assuming that vertical barriers were combined with an effective cap, the two technologies would act essentially as an upside-down box over the waste. This would reduce the potential for human or bio-intrusion.

Vertical barriers were considered as stabilization alternatives for the nine waste disposal shafts at MDA H. Under one alternative, a vertical sidewall barrier would be constructed at a predetermined depth and width around the entire perimeter of MDA H. Concrete caps would be placed above the shafts and the surface covered with an evapotranspiration cover. Under a second alternative, which was selected as a partial corrective remedy by NMED (NMED 2007a), interlocking boreholes filled with grout would surround each of the 6-foot shafts. A concrete cap would be installed (DOE 2004b). A third alternative was the deep-surface horizontal barrier discussed below.

Deep-Surface Horizontal Barrier

A horizontal barrier could be installed underneath disposed waste to reduce the downward aqueous-phase movement of contaminants. Such a barrier was selected by NMED for encapsulation of the nine disposal shafts at MDA H (LANL 2003b, NMED 2007a). A wall would be constructed around each disposal shaft by drilling interlocking shafts around each disposal shaft that would be filled with cement slurry. At the bottom of each disposal shaft a bottom seal would be constructed using a three-fluid (“Kajima”) system. An injector assembly would be lowered to the bottom of one or more shafts. As the injector assembly rotated, it would direct high-energy jets of water against the tuff. An air jet producing an aureole of compressed air concentric about the jet would augment the effectiveness of the water jet. At the same time, cement grout would be injected into the void and the surrounding soil through a second nozzle. A mixing radius of over 6 feet (1.8 meters) can be achieved (LANL 2003b).

The Kajima system may not be effective for all disposal units considered in this appendix. Most MDAs are much larger than MDA H, comprising pits and trenches covering large surface areas in addition to shafts.

Near-Surface Horizontal Barrier

These technologies provide horizontal barriers above disposed waste to reduce vertical infiltration of water into waste and to reduce the potential for intrusion by plants, animals, or humans. Technologies include a soil-grout mixture and vitrification:

- *Soil-grout mix.* A soil-grout mixture would be emplaced over the tops of the disposal units. The mixture could range in thickness up to several feet. After the mixture hardens, it would restrict infiltration or intrusion.
- *Vitrification.* Electrical resistance would heat several feet of soil above disposed waste to temperatures high enough to melt the soil. This melted area would cover the entire surface

of a disposal unit.³⁴ When the melted soil or rock cools, a glasslike mixture would cover the tops of the disposal units. The glass mixture would be theoretically impenetratable against water infiltration and biological intrusion.

A soil-grout mix may be more generally suitable to the MDAs considered in this appendix. Vitrification would subject the top layers of waste within the MDAs to high levels of heat, possibly causing unsafe reactions.

Surface Barriers

These technologies comprise barriers placed over the tops of disposal units to restrict infiltration of water, erosion, or biointrusion. Possible barriers may include asphalt covers, compacted clay covers, multiple-layer covers, evapotranspiration covers, and biotic barriers.

Asphalt covers. A layer of asphalt would be placed over the tops of the disposal units. Asphalt layers have been placed over portions of disposal units at MDA AB (Area 2), MDA L, and MDA B. Investigations at Area 2 of MDA AB have shown that moisture has been trapped beneath its asphalt layer. Absent the asphalt, the moisture may have evapotranspired. Also, if portions of the asphalt collapse from settling or subsidence of the underlying waste and backfill, the holes produced in the asphalt can act as a funnel for infiltration.³⁵

Compacted clay cover. A 1- to 3-foot (0.3- to 0.9-meter) layer of compacted clay would be placed over the tops of disposal units. Because clay, when effective, has a very low permeability and therefore resists water infiltration, a clay cap has been recommended or used at numerous waste disposal sites. But in arid and semiarid environments the clay can dry and crack, leading to comparatively large rates of infiltration through the cracks. And to the extent that the underlying waste and soil is structurally unstable, leading to subsidence and differential settling, the barrier provided by the compacted clay may be disrupted.

Multiple-layer cover. Multiple-layer covers consist of layers of different geologic and synthetic materials. They have been proposed for several radioactive waste disposal sites and are being used at RCRA landfills. The Corrective Measures Study Report for MDA H cites cases where multiple-layer covers at RCRA landfills were damaged through settlement that compromised the continuity of the cover's discrete layers. The clay layer at the bottom of a differentially settled area at a landfill may be breached. Also, a geomembrane may tear if enough settlement occurs. The drainage layer above the barrier layer can funnel moisture to the low area where infiltration occurs at the breached portions of the clay layer (LANL 2003b).

Evapotranspiration cover. Evapotranspiration covers are designed to enhance soil water storage capacity by retaining infiltrated water until it can be evaporated by solar radiation and transpired by shallow-rooted plants. Two types of evapotranspiration covers have been investigated: monolithic evapotranspiration covers and evapotranspiration covers having capillary barriers. Monolithic evapotranspiration covers consist of a single, vegetated soil layer having a site-specific mix of soil texture, soil thickness, and vegetation. Evapotranspiration covers having

³⁴ See the *In Situ Physical Treatment* section for a brief discussion on applying vitrification to waste in an entire disposal unit. In this case, vitrification is used for long-term waste stabilization.

³⁵ The asphalt layer at MDA AB was removed in 1999 and an evapotranspiration cap installed (LANL 1999a).

capillary barriers include an interface between an upper fine-textured soil and lower coarse-textured material.³⁶ The capillary barriers are placed below the water storage zone to provide additional protection against downward water flow (INEEL 2000).

Unlike clay covers, evapotranspiration covers do not rely on low hydraulic conductivity. Mechanisms that increase the hydraulic conductivity of evapotranspiration covers (that is, drying out) do not significantly affect their performance. Hence, evapotranspiration covers—particularly monolithic covers—may be less susceptible to loss of function from subsidence and differential settlement than either a compacted clay cap or a multiple-layer cap.

Evapotranspiration caps have been developed explicitly for landfills in arid and semiarid environments. Case studies addressing the use of evapotranspiration caps at landfills covering a range of climatic conditions have been summarized in a technology overview by the Interstate Technology and Regulatory Council (ITRC 2003a). Research has been ongoing about use of evapotranspiration caps at LANL disposal units since the early 1980s (Breshears, Nyhan, and Davenport 2005; Nyhan 2005).

Biotic barriers. These barriers control the intrusion of plants or animals into disposal units. One approach would be to place layers of hard, long-lasting natural materials such as cobble-sized rocks or pea gravel. These barriers discourage penetration by burrowing animals and, depending on design, can potentially discourage penetration by deep-rooting plants.

Research has been performed on burial of herbicides (or other plant poisons) within discharge units at depths below those associated with desirable types of local, shallow-rooted plants. Plants having roots that grow into the herbicide layer are killed. The efficacy of this technology is limited to the secretion period of the discharge units.

At MDA AB, chain-link fencing has been placed on the surface of a disposal cover. Although vegetation readily grows through the fencing, intrusion by burrowing animals is discouraged (LANL 1999b).

In Situ Biological Treatment

These technologies use processes that feed on organic material. The technologies have been effective in treating low-level concentrations of radionuclides in wastewater, but have not been demonstrated at radioactive waste disposal sites (LANL 2003b).

In Situ Physical Treatment

Several technologies may help remediate or physically stabilize waste disposal sites, including those described below.

Soil gas venting. Boreholes are drilled into the soil and left open, allowing release of subsurface vapors and gases to the atmosphere or a treatment system. Soil gas venting may be used to

³⁶ Under unsaturated conditions, water in the small pores of the fine-textured soil is held at high tension and will not flow into the large pores of the coarse-textured soil where the water tension is low. For the water to flow out of the soil and into the coarse-textured material, it must be at sufficiently low tension. Tension decreases as the soil approaches saturation. Once breakthrough occurs, water will drain into the coarse material at a rate largely controlled by the hydraulic conductivity of the overlying soil (INEEL 2000).

remove an underground source of volatile organic compounds or to reduce volatile organic migration. It is less effective when volatile organic compound concentrations are in the parts-per-billion range. It has been postulated for release of tritium in a gaseous or vapor form (LANL 2003b).

Soil vapor extraction. A force is applied to underground gases or vapors to accelerate their removal from soil. Forces have included: (1) air pressure injected into one or more wells; (2) a vacuum pulling the gas or vapor from one or more wells; or (3) a steep diffusion force that removes gas or vapor from an area. The extracted gas or vapor may be directed to a treatment system. The technology is less effective for volatile organic compounds when volatile organic compound concentrations are in the parts-per-billion range (LANL 2003b).

Pneumatic fracturing. A fluid is injected at high pressure to create open fractures in an area where a contaminant plume exists. The opened flow paths allow access to the contaminated media for removal or treatment. The technology injects large amounts of water, which may accelerate contaminant movement. If the contaminant includes explosives, the technology might promote their detonation (LANL 2003b).

Electrokinetic soil treatment. This technology continuously removes ionic or charged species from soils. A low-intensity direct current is produced between ceramic electrodes that are divided into a cathode array and an anode array. Charged species are mobilized toward the electrodes. Metal ions, ammonium ions, and positively charged organic compounds move toward the cathode. Chlorides, cyanides, fluorides, nitrates, negatively charged organic compounds, and other anions move toward the anode. Contaminants that migrate toward the polarized electrodes may be removed. If the contaminant includes explosives, the technology may promote their detonation. Effectiveness is reduced for waste having a moisture content smaller than 10 percent (LANL 2003b, FRTR 2005).

Vitrification. In situ vitrification uses an electric current to melt soil or waste at temperatures from 2,900 to 3,650 degrees F (1,600 to 2,000 degrees C). Most inorganics are immobilized within the vitrified glass and crystalline mass, and most organics are destroyed by pyrolysis. Water vapor and organic combustion products are captured and drawn into a treatment system. Vitrification leaves a chemically stable, leach-resistant crystalline material similar to obsidian or basalt (FRTR 2005). In situ vitrification has been demonstrated at LANL by treating a small portion of one absorption bed at MDA V (LANL 2003e, 2004j).

Compaction with conventional equipment. Decreased infiltration and percolation through a disposal unit cover (by reducing porosity and thus permeability) can be achieved using commercially available equipment. Equipment may include sheepsfoot rollers, rubber-tire rollers, smooth-wheel rollers, vibrating baseplate compactors, and crawler tractors. Soil to be compacted would be applied in 6- to 12-inch (15- to 30-centimeter) lifts and several passes made to compact each lift to the desired density. The depth of compaction can range from 0 to 6 feet (0 to 1.8 meters) (NRC 1981).

Dynamic compaction. This technology compacts and consolidates waste in place. It may greatly reduce settling and subsidence over time. It has potential use at pits and trenches where the surface area is large relative to the disposal unit depth. A heavy weight is raised above a disposal

unit and dropped, compressing the area underneath the weight. The weight is lifted, moved to cover an adjoining area of the disposal unit, and dropped. This process is continued until all the area over the disposal unit is compressed. The voids created by the process are backfilled and compacted. The technology has drawbacks: for maximum effectiveness, compaction should extend to the bottom of the disposal units. If the compactor breaks through the cover placed over the waste, contamination may be ejected. (Significant ejection of material might be avoided by making repeated compacting runs over the same area, each time filling in voids after each compacting effort.) The physical shock may destroy the integrity of any buried waste container. It may drive moisture from the disposal unit into the surrounding soil matrix (NRC 1981).

Waste stabilization. Wastes can be stabilized using a lance to inject a grout mixture (or similar) into the waste zone. The process to be employed, and the grout formulation, would be developed through a test program. The grout could be mixed at a conveniently sited batch plant, delivered to the work site by truck, and fed into pumps that deliver the grout to an injection lance using high-pressure lines. The injection lance would be driven into the waste using technology such as a rotary percussion drill to the maximum depth of the waste, or until refusal. As grout is forced out of jet nozzles located in the tip of the lance, the lance is rotated as it is withdrawn. After the lance is retracted, it is decontaminated and moved to the next location. Care is needed to minimize the return of grout to the surface. Another concern is ground heaving. Properly performed, the technique can increase the density of the disposed waste without any increase in waste volume. In addition to waste stabilization, the technique reduces the permeability of the waste, and provides encapsulation and chemical buffering (INEEL 2002c).

In situ grouting has been analyzed and tested at several DOE sites as summarized in an Idaho National Laboratory report (INEEL 2002c). Grout consisting of Portland cement, epoxy, hematite grout, paraffin grout, and other proprietary formulations have been investigated or considered (INEEL 2002c). In situ grouting is an option for stabilization of the trenches, pits, and shafts at the Idaho National Laboratory surface disposal area (INEEL 2002a). A variation was considered for encapsulation of the LANL MDA H shafts (DOE 2004b).

Thermal treatment. Several techniques have been developed to decompose heat-sensitive contaminants into less-toxic or less-mobile forms. These techniques can be used to heat a contaminant into a vapor phase, and in so doing, enhance its extractability. Heat may be generated using microwave, radiofrequency, thermal radiation, or other methods. But if the contaminants include reactive or explosive materials, this technology might promote undesirable chemical reactions (LANL 2003b).

I.3.3.1.2 Possible Removal, Ex Situ Treatment, and Disposal Technologies

A decision to remove waste or contaminated soil results in an interlinked series of operations:

- Excavation;
- Material characterization;
- Material classification;
- Treatment and packaging; and
- Storage or disposal of the material.

The first three operations are addressed in Section I.3.3.1.2.1; the last two are addressed in Section I.3.3.1.2.2. Some case studies are summarized in Section I.3.3.1.2.3.

I.3.3.1.2.1 Removal Technologies and Operations

Removal activities must be conducted in a manner that ensures worker and public safety, minimizes the spread of contamination, and minimizes possible negative effects on biological, cultural, and operational resources. Typical removal activities are listed in **Table I–29**.

Table I–29 Typical Removal Activities

| <i>Activity</i> | <i>Typical Subactivities</i> |
|----------------------------|--|
| Planning | Engineering and operations Material disposition Safety assessments and plans Biological and cultural assessments and resource protection plans Stormwater pollution prevention plans Best management practices for erosion control NEPA reviews Readiness reviews |
| Permits and authorizations | National Pollutant Discharge Elimination System General Permit Regulatory corrective action approval NEPA documentation Safety authorization Other authorization |
| Preliminary work | Site preparation (establish roads and equipment; material; and waste storage, handling, and decontamination areas and reroute utilities) Remove buried pipes or lines or overheads (ensure utilities, if needed) Establish environmental and safety monitoring networks Perform tests and further develop equipment and procedures (test excavations, etc.) Perform surface and subsurface tests and sample collections to determine the extent of contamination |
| Operations | Excavation Contamination control Sorting Media characterization Material characterization Material classification Packaging for transport Safety and environmental monitoring |
| Finish work | Backfilling Final cover, if needed Cleanup and remediation |
| Closeout | Final sampling and monitoring Regulatory approval |

NEPA = National Environmental Policy Act.

After the planning, authorization, and site preparation phases are completed, excavation would commence and continue until the operational objectives are met. Overburden over the contaminated material, or uncontaminated material excavated near the contaminated material, would be stockpiled for return to the excavation when contamination removal is completed.

Removal operations can be differentiated into:

- *Standard removals*: Those that can be safely and relatively quickly conducted using standard construction equipment

- *Specialized removals*: Those requiring more extensive planning and effort and use of specialized procedures and equipment

Standard, usually small-scale, removals have taken place at several DOE sites. Procedures for radiation and industrial safety, contamination control, waste characterization, and classification are well established. Waste equipment commonly used for such removals is listed in **Table I–30** (INEEL 2002b).

Table I–30 Equipment Commonly Used for Standard Removals

| <i>Equipment</i> | <i>Description</i> | <i>Comments</i> |
|----------------------|--|--|
| Backhoe | Tracked or wheeled excavators used for digging small areas, having a typical bucket size of 2 cubic yards (1.5 cubic meters). Auxiliary equipment can include clamshell buckets, drum grapplers, dippers, loader buckets, and hammers. | Useful for trench digging and area excavation up to 45 feet (13.7 meters) deep. Linear reach less than 100 feet (30 meters). |
| Front-end loader | Tracked or wheeled excavators capable of digging, lifting, dumping, and hauling. Bucket size is up to 20 cubic yards (15 cubic meters). | Useful for excavating large areas having short travel distance needs (< roughly 300 feet [91 meters]). |
| Bulldozers | Tracked vehicle having a blade or bucket for surface work. | Useful for removing surface layers, clearing surface debris, and general earthmoving. Less useful for retrieval of buried waste. |
| Trencher | Wheeled excavator capable of excavating and grading. Commonly called a ditch witch, it can use auxiliary equipment such as a backhoe, backfill blade, or an auger. | Useful for small-scale digging. |
| Vacuum/soft trencher | Vacuum removes soil without disturbing large debris. Can use jetted air to loosen soil before vacuum removal. | Potentially useful for loose soil removal at dig face. Not useful for retrieving buried waste. |
| Soil skimmer | Removes thin layers of soil in a controlled manner. | |
| Skid-steer loader | Small excavator similar to a front-end loader. Often called a Bobcat. | |

Source: INEEL 2002b.

Specialized removals require more extensive planning and effort and use of specialized procedures and equipment such as remote-control excavators or excavators designed to protect the operators from external radiation or airborne contamination hazards. An Idaho National Laboratory report (INEEL 2002b) provides 13 case histories of demonstrations where (mainly) DOE sites have: (1) used remote excavators and end-effectors; (2) modified standard equipment so a person in a sealed environment could operate the equipment; and (3) faced conditions similar to those at the Idaho National Laboratory subsurface disposal area. Another reference surveys commercially available remote-control machines for excavation and recovery of buried ordnance (LLNL 2002). Appendix G of the Sandia Mixed Waste Landfill Corrective Measures Study Final Report reviewed excavation of a portion of the landfill using robotics (SNL 2004). Examples of specialized excavators and ancillary equipment are listed in **Table I–31** (INEEL 2002b).

Example measures for controlling contamination during excavation are listed in **Table I–32** (adapted from INEEL 2002b).

Table I-31 Examples of Specialized Excavators and Other Equipment

| <i>Equipment</i> | <i>Comments</i> |
|---|---|
| Remote Excavators | |
| Brokk | Remote controlled excavator with a telescoping arm. Available with several end-effectors for hammering, cutting, and scooping wastes. The largest BROKK can reach about 13 feet (4 meters) below ground surface (bgs). Used at Hanford for retrieval of high-dose debris and at Idaho National Laboratory for demolition. |
| Kiebler Thompson | Remote-controlled excavator with a telescopic boom capable of three-dimensional movement. Available with several end-effectors. The largest machine can reach about 16 feet (5 meters) below ground surface. Similar to the Brokk. |
| T-Rex | A tele-operated, heavy-lift, long-reach excavator used to retrieve boxes, drums, and containers using a front-shovel excavator. Controls can be operated up to 1,250 feet (381 meters) away. Developed at Idaho National Laboratory. |
| HERMES | A tracked computer controlled excavator with a hydraulic manipulator. The system (Hybrid Remote Robotic Manipulation and Excavation System [HERMES]) was developed by Boissiere Engineering and Applied Robotics (BEAR), Inc., and used for exhuming LANL's MDA P. |
| Modified Standard Equipment | |
| Sealed, pressurized cabins | Standard construction equipment with cabin modifications. Can supply air to the operator either using filtered air intakes or externally supplied air. Possibly useful for environments where the inhalation hazard is high. |
| Shielded cabins | Standard construction equipment with cabin modifications. The walls and cabin windshield would be shielded for use in high external radiation environments. |
| Remote Cranes | |
| Cooperative Telerobotics Retrieval System | System consists of a 80-foot-wide (24-meter-wide) girder, two trolley assemblies with vertically telescoping masts, two manipulators, and a 5-ton (4.5 metric ton) remotely operated hoist. Presently at Idaho National Laboratory. |
| RoboCrane | Cable-driven platform for a parallel link manipulator. Provides load control via teleoperative, graphic offline programming, and hybrid control modes. |
| Remote End-Effectors | |
| Safe excavation | High-pressure probe dislodges compacted and other hardened materials using air-jet/vacuum end-effector system. Vacuums up soil. |
| Tentacle, highly manipulative | Teleoperated manipulator and bellows actuator. Used with a crane and manipulator. Load capabilities less than 4,000 pounds (1,814 kilograms). |
| Schilling Tital II | Manipulators deployed by crane for selective retrieval of barrels from soil. Basic components include hydraulic system, positioning system, electronics module, and mechanical interface. |
| Confined sluicing end-effector | Water jet designed for waste tank cleanout. Uses high-pressure water jets to cut material into small pieces and evacuates with a vacuum jet pump. Captures slurry water. Creates additional waste. |
| Innovative end-effector | Consists of a thumb, an attachable integrated transfer module, and a shovel assembly. Capable of soil retrieval and dust-free waste dumping. |

MDA = material disposal area.

Source: INEEL 2002b.

In situ soil remaining after excavation must be characterized to determine whether it is sufficiently contaminated to warrant removal. Screening levels would be determined for the removal based on expectations about the future use of the site and upon established health, safety, or environmental protection criteria. Soils that do not exceed the screening levels would be left in place. Characterization techniques to be used, and their implications on operations, will depend on the contaminant under consideration; its in situ concentration; and operational or environmental factors.

Table I-32 Example Contamination Control Options

| <i>Options</i> | <i>Description</i> |
|---|--|
| Confinement | Confinement structures made from plastic, metal, or other materials can enclose a piece of equipment, a work area, or a site and thereby prevent the spread of airborne contaminants. Enclosures used at a site or work area have ranged from lightweight, portable units to substantial structures. |
| Ventilation and vacuum systems | These systems use laminar airflow at a dig-face within enclosures to direct dust to filters. Vacuums remove loose particulates from equipment and structures and collect dust and debris. |
| Foams, sprays, misters, fixatives, and washes | These options can be used to control odors, volatile organic compounds, dust, and other emissions; create a barrier between work surfaces and the atmosphere; settle loose airborne contamination; and decontaminate personnel and equipment. |
| Electrostatics | Electrically charged plastic and electrostatic curtains form barrier walls against spread of contamination from enclosed areas. Curtains can be used upstream of emission filtering systems to neutralize charged dust particles. |
| In situ stabilization | Used before excavation to fix contamination into the soil and waste matrix and thereby minimize its dispersion into the air or surface water. Processes include injection of grout, resin, or polymer; vitrification; or ground-freezing. |

Source: INEEL 2002a.

Excavated material must be similarly characterized in terms of its radionuclide or hazardous content to enable decisions about its further disposition. Soil or other materials that do not exceed screening levels may be recycled, disposed of as solid waste, or used as backfill. Contaminated material can be considered waste or decontaminated, if feasible and cost effective, and the decontaminated material reused, recycled, or disposed of.

Requirements for the subsequent disposition of the waste depend on the waste’s classification. Wastes containing RCRA hazardous constituents must be treated according to regulatory-prescribed methods. DOE classifies wastes containing radionuclides as low-level radioactive waste if the concentrations of alpha-emitting transuranic isotopes (having half-lives exceeding 20 years) do not exceed 100 nanocuries per gram of waste.

As site preparation and excavation proceeds, site survey and monitoring programs would be conducted to ensure worker health and safety and to detect movement of radioactive or hazardous constituents from the work area to the environment.

After removal is complete, the site must be restored. An excavation at an MDA would be backfilled with soil, compacted, and revegetated. There would be an investigative effort to confirm that the corrective action objectives of the removal had been achieved. Appropriate after-action reports would be prepared for submittal and approval.

I.3.3.1.2.2 Treatment and Disposal Options

Following removal, wastes may require treatment and perhaps specialized packaging before their further disposition. Treatment options for wastes containing RCRA hazardous constituents include (LANL 2003b):

- *Neutralization.* Reactive materials can often be neutralized. Acids can be neutralized using bases and vice versa. Lithium compounds can be neutralized through reaction with water.
- *Thermal treatment.* Burning to destroy the explosive compounds can treat HE. This technology has long been used at LANL.

- *Cement stabilization.* Some materials may require stabilization before disposal as hazardous or mixed waste. This technology has long been used.
- *Debris treatment.* Treatment standards for materials meeting the RCRA definition of debris are specified in 40 CFR 268.45 and New Mexico Administrative Code 20.4.1.800. Microencapsulation is authorized for treating lead or lead-containing debris.

Some of the wastes possibly recovered from MDAs may be compressed gas cylinders.³⁷ Gas cylinders may present a physical hazard if they are recovered still pressurized and a chemical hazard depending on the gases contained within the cylinders. Gases in recovered cylinders may be toxic or reactive. Gases may be caustic or acidic, for example, or unstable. For example, hydrogen cyanide and ethylene oxide can undergo exothermic polymerization, while gases such as hydrogen bromide can react with moisture. Pyrophoric liquids may be stored in nonpressurized gas cylinders.

Recovered cylinders may be safely opened and the contents either recovered or treated. Basically, the recovered cylinder is placed within an explosion-resistant pressure vessel configured with various cutting tools and perhaps an inert-gas environment. (Recovered cylinders can be transported to a treatment facility external to the excavation using overpacks designed to contain the contents of the cylinder if it leaks or fails during transport.) Once the container contents are released within the pressure vessel, the gases or liquids may be transferred to appropriate external reactors or collection tanks. Gases, for example, can be transferred to wet scrubbers for neutralization. Systems are also available to treat cylinders containing biological or chemical weapon material (IES 2005).

Treatment of waste contaminated with high explosives would take place at LANL. Treatment of other RCRA hazardous wastes could take place either at LANL, if treatment capacity exists, or at an offsite location. Radioactive waste would be treated to meet the waste acceptance criteria for the facility receiving the waste.

Onsite Disposal Capacity

Onsite solid waste capacity. Solid waste currently generated by LANL's environmental restoration project is typically sent to an offsite solid waste landfill. However, a municipal solid waste landfill (to be closed) does exist within the LANL boundary (see Section I.4.9).

Onsite low-level radioactive waste capacity. The only operating low-level radioactive waste disposal facility at LANL is at Area G in TA-54. Because of the impending lack of capacity in existing disposal units, and because LANL personnel must complete remediation at MDA G by the end of 2015, LANL is expanding low-level radioactive waste disposal operations into Zone 4 and Zone 6 in TA-54 (see Section I.4.9).

³⁷ Because LANL's mission during the period when compressed gas cylinders could have been disposed of was oriented much more to research and development than production of nuclear materials, pressurized containers possibly disposed of in LANL MDAs were probably lecture-size bottles containing no more than 1 pound as a pressurized liquid.

Offsite Treatment and Disposal Capacity

Offsite treatment and disposal capacity exists for solid waste, hazardous waste, low-level, and mixed low-level radioactive wastes, and transuranic waste. Examples are described below.

Solid waste capacity. The Solid Waste in New Mexico, 2000 Annual Report lists 50 active solid waste landfills, including 3 landfills that accept construction and demolition wastes (NMED 2000).

Hazardous waste capacity. The 2006 U.S. Army Corps of Engineers *Report on Treatment, Storage & Disposal Facilities (TSDF) for Hazardous, Toxic, and Radioactive Waste* provides information about eighteen facilities currently engaged in commercial disposal of RCRA Subtitle C hazardous waste (ACE 2006). Five of these facilities hold a Toxic Substances Control Act permit for disposal of PCB-contaminated materials. Information about six hazardous waste sites near LANL is provided in **Table I-33**.

Table I-33 Selected Hazardous Waste Operations Near Los Alamos National Laboratory

| <i>Operator and Location</i> | <i>Hazardous Waste Operations^a</i> | <i>Waste Groups Accepted^a</i> |
|--|--|---|
| Clean Harbors Westmorland, LLC Westmorland, CA | Treatment of heavy metals and other wastes; micro-encapsulation; solidification; waste landfill; processing of bulk or drummed wastes; storage before treatment or disposal. | RCRA hazardous waste; naturally occurring radioactive material waste from geothermal operations; Animal and Plant Health Inspection Service soils; and California-regulated wastes. |
| Clean Harbors Dear Trail, LLC Dear Trail, CO | TSD. Analytical capacity for TCLP, cyanide, alkaline chlorination; chemical reduction; stabilization or solidification; deactivation and neutralization; micro-encapsulation; landfill. | Contaminated process wastewaters; inorganic cleaning solutions; organic and inorganic laboratory chemicals; paint residues; debris from toxic or reactive chemical cleanups; off-spec commercial products. |
| U.S. Ecology Nevada, Inc. Beatty, NV | Chemical oxidation; stabilization; thermal; micro- and macro-encapsulation. | RCRA hazardous wastes, debris, and solid waste greater than 500 parts per million VOCs; PCBs; non-hazardous solid industrial, commercial, and agricultural chemical wastes; liquids for solidification; bulk or drummed solid waste; household hazardous waste; lab packs; State-regulated hazardous wastes; waste from conditionally-exempt small quantity generators; corrosive wastes and acids; asbestos or asbestos-RCRA debris. |
| Clean Harbors Lone Mountain, LLC Waynoka, OK | Waste treatment and storage; RCRA hazardous landfill operations; waste water treatment; rail transfer operations. | PCB soil and debris; non-hazardous soil; hazardous soil for direct landfill; hazardous soil for treatment of metals and organics on a case basis; debris for micro- or macro-encapsulation; plating waste; acidic waste; caustic waste; cyanide and sulfide bearing waste; and hazardous and nonhazardous liquids. |
| Waste Control Specialists Andrews, TX | TSD. Chemical oxidation or reduction; deactivation; macro-encapsulation; neutralization; stabilization; controlled reaction; amalgamation. Can dispose of treated soil. Can shred debris or treat VOC waste; aqueous waste; soil; dioxin, inorganic and organic sludges and solids; paint sludges; PCBs; pesticides; reactive material; solvents; TCLP metals; acids; caustics; oil. | Accepts >2,000 RCRA waste codes and TSCA materials. Most accepted radioactive waste is not disposed of. Can dispose of some exempt radioactive wastes, including some source material; some material containing thorium; some NORM; some materials containing rare earths; depleted uranium used for shielding; and materials exempt from licensing under Texas regulation. |

| <i>Operator and Location</i> | <i>Hazardous Waste Operations^a</i> | <i>Waste Groups Accepted^a</i> |
|--|--|---|
| Clean Harbors Grassy Mountain, LLC Salt Lake City, UT | Truck and rail logistics; drain and flush for PCB transformers; solidification & stabilization; repackaging. | PCBs; non-hazardous soils and other nonhazardous industrial wastes; asbestos wastes; hazardous waste for treatment of metals; plating wastes; acidic wastes; caustic wastes; hazardous debris; and non-PCB liquid wastes for solidification and landfill. |

TSD = treatment, storage, and disposal; RCRA = Resource Conservation and Recovery Act; TCLP = toxicity characteristic leaching procedure; VOCs = volatile organic compounds; PCB = polychlorinated biphenyl; TSCA = Toxic Substances Control Act; SNM = special nuclear material; CFR = *Code of Federal Regulations*.

^a The listed information is a summary. Consult hazardous waste operators for specific information about operations, waste groups accepted, and restrictions.

Source: ACE 2006.

Low-level and mixed low-level radioactive waste capacity. Offsite treatment and disposal capacity exists for commercial and DOE disposal of low-level radioactive waste and mixed low-level radioactive waste. Some of the treatment and disposal options that may be considered may include the Chem-Nuclear³⁸ low-level radioactive waste disposal facility near Barnwell, South Carolina; the U.S. Ecology low-level radioactive waste disposal facility on the Hanford Reservation; the EnergySolutions disposal facility near Clive, Utah; the Waste Control Specialists Facility near Andrews, Texas; and DOE's Nevada Test Site.

Neither the Chem-Nuclear nor the U.S. Ecology facility accepts mixed low-level radioactive waste for treatment or disposal, and both limit (or shortly will limit) the quantities of wastes that may be accepted. After FY 2008, only waste generated by members of the Atlantic Interstate Low-Level Radioactive Waste Compact may be accepted.³⁹ The U.S. Ecology facility accepts waste only from the eight states composing the Northwest Interstate Compact and from the three members of the Rocky Mountain Compact. Although New Mexico is a member of the Rocky Mountain Compact, waste from DOE generators is not encouraged (WSDOE 2005).

The EnergySolutions disposal facility near Clive, Utah, accepts Class A⁴⁰ low-level and mixed low-level radioactive wastes. The facility accepts bulk and containerized materials, and mixed waste for treatment by stabilization, oxidation-reduction, deactivation, chemical fixation, neutralization, and macro- and micro-encapsulation. The wastes managed at the disposal facility may not have an external contact dose rate equal to or exceeding 200 millirem per hour on a manifested container; 500 millirem per year on external, accessible surfaces of individual wastes within a container; or 80 millirem per hour for containers of resin (EnergySolutions 2006).

The Waste Control Specialists Facility near Andrews, Texas, accepts low-level and mixed low-level radioactive wastes for treatment. Low-level radioactive waste disposal is not yet authorized. Treated waste is either returned to the generator or sent to another site for disposal. RCRA hazardous wastes may be disposed of (WCS 2002).

³⁸ Chem-Nuclear, LLC, is a wholly owned subsidiary of Duratek, Inc., which merged in 2006 with other companies to form EnergySolutions, LLC.

³⁹ South Carolina Code of Laws, Title 48, Chapter 46, Atlantic Interstate Low-Level Radioactive Compact Implementation Act.

⁴⁰ The NRC system in 10 CFR 61.55 for classifying low-level radioactive waste is based on two tables listing waste class concentration limits for short- and long-lived radionuclides. For example, low-level radioactive waste containing alpha-emitting transuranic isotopes having half-lives exceeding 5 years is classified as Class A waste if concentrations do not exceed 10 nanocuries per gram of waste, or as Class C waste if concentrations are greater than 10 nanocuries per gram and less than or equal to 100 nanocuries per gram.

DOE's Nevada Test Site disposes of low-level and mixed low-level radioactive waste from DOE Nevada activities, as well as from approved generators, generally defined as those DOE sites and contractors that have traditionally shipped waste to the Nevada Test Site. (LANL has, in the past, shipped waste to the Nevada Test Site for disposal.)

Transuranic waste capacity. Transuranic waste disposal capacity is available at WIPP near Carlsbad, New Mexico. WIPP currently accepts defense-generated transuranic waste for disposal. Mixed contact-handled transuranic waste is acceptable; however, waste that exhibits RCRA characteristics of ignitability, corrosivity, or reactivity must be treated (DOE 2002, WIPP 2004). WIPP initially received only contact-handled transuranic waste, but the WIPP permit modification for receipt of remote-handled transuranic waste was approved in October 2006.

Transuranic waste must contain alpha-emitting transuranic isotopes, having half-lives exceeding 20 years, in concentrations exceeding 100 nanocuries per gram of waste. Pursuant to the WIPP Land Withdrawal Act, the total capacity at WIPP is 6.2 million cubic feet (0.18 million cubic meters) of transuranic waste. Several restrictions exist for acceptance of remote-handled waste.

I.3.3.1.3 Related Remedial Actions

Section I.3.3.1.3.1 summarizes case histories of removals at MDA P and the Sandia Chemical Waste Landfill. Section I.3.3.1.3.2 summarizes the removal alternative considered for remediation of MDA H. Section I.3.3.1.3.3 presents observations.

I.3.3.1.3.1 Selected Case Histories

LANL MDA P. MDA P in TA-16 operated from 1950 to 1984 and contained detonable HE, HE residues in soil, barium, and asbestos; and low levels of uranium, lead, and cadmium. The closure process began in February 1997 (LANL 2001a), when a clean closure plan was approved by NMED. The volume to be removed was estimated to be 30,000 cubic yards (22,900 cubic meters). But in the fall of 1997, work crews discovered HE ranging from the size of a fingernail to that of a softball. Plans for removal were changed. A remote excavator was acquired, as well as a team of explosive ordinance experts to screen excavated materials for high explosive (LANL 2001d). Excavation resumed in February 1999 and was completed on May 3, 2000 (LANL 2001a). Work crews used high-pressure water to remove debris potentially contaminated with HE (LANL 2001d). Nonremote excavation of contaminated soil beneath the waste pile began after the May 2000 Cerro Grande Fire and was completed in March 2001. Additional material was removed in February 2002 (LANL 2001a).

Material excavated from MDA P included 52,500 cubic yards (40,100 cubic meters) of soil and debris (including hazardous and industrial waste and recycled material); 387 pounds (176 kilograms) of detonable high explosive; 820 cubic yards (627 cubic meters) of hazardous waste with some radioactive contamination; 6,600 pounds (3,000 kilograms) of barium nitrate; 2,605 pounds (1,180 kilograms) of asbestos; 200 pounds (91 kilograms) of mixed waste;

235 cubic feet (6.7 cubic meters) of low-level radioactive waste, and 888 containers of unknown content (LANL 2001a).⁴¹ The high explosive was burned (LANL 2001d).

Sandia Chemical Waste Landfill. This landfill was a 1.9-acre (0.77-hectare) landfill near Albuquerque, New Mexico, that was used for disposal of chemical and solid waste between 1962 and 1985 and as a storage area for hazardous waste drums between 1981 and 1989. Liquid and solid waste disposal was discontinued in 1981 and 1985, respectively. Closure of the landfill was initiated in 1988 (SNL 2003).

The site was prepared for excavation following a 2-month preparation period that included mobilization of equipment and administration trailers. Excavation began in September 1998 and was completed in February 2002, when 52,000 cubic yards (40,000 cubic meters) of soil, solid, hazardous, and mixed waste was removed. Excavation extended to 12 feet (3.7 meters) below ground surface and occasionally to 30 feet (9.1 meters). In addition to soil, excavated debris included compressed gas cylinders, intact chemical containers, partially expended munitions, thermal and chemical batteries, large metal objects (such as tanks or gloveboxes), waste containing radionuclides, asbestos-containing tiles and blocks, and biohazardous waste.

Management of the excavated waste was performed in a manner consistent with its hazard. The 357 compressed gas cylinders—apparently intact—that were recovered were processed in an onsite mobile facility. Of these, 233 were empty. Various combinations of five methods were used to process the remaining cylinders, including (SNL 2003): carbon adsorption; devalving of the containers with or without the use of liquid nitrogen; neutralization of the cylinders using sulfuric acid or sodium hydroxide; recontainerization of solids and liquids from the cylinders for appropriate disposal; and venting of the gases through a carbon scrubber.

Excavation was conducted using a large tracked backhoe (trackhoe) having Lexan windows for shielding against explosion. (Blast-resistant Lexan shielding was placed near the excavation for protection of ground personnel.) Workers were equipped with protective clothing and supplied-air breathing apparatus. The project experienced several delays and work slowdowns over the 3.25-year excavation period because of deficiencies in the rate at which excavated material could be sorted; weather conditions; safety concerns (for example, unexpected encountering of chlorobenzylidene malonitrile, an irritating powder; and an apparently erroneous detection of hydrogen cyanide); space limitations in staging and disposing of material; and other issues. Three different technologies for screening excavated soil and debris were tried. A tent was constructed over the sorting area, and a motorized conveyor belt with a site-built hopper was used to avoid manually handling excavated rock. During the first year of the project, the average excavation rate was 155 cubic yards (119 cubic meters) per 50-hour workweek; thereafter, this rate was raised to about 374 cubic yards (286 cubic meters) per 50-hour workweek.

I.3.3.1.3.2 Material Disposal Area H Removal Alternative

At MDA H (PRS 54-004), nine shafts were used for disposal of classified wastes, receiving weapons components, classified documents and paper, aluminum, plastic, stainless steel, rubber, graphite shapes, weapon mockups, depleted uranium scraps and classified shapes, and other materials (DOE 2004b, LANL 2005c). An investigation program has been completed and the

⁴¹ Revised waste summaries are in the MDA P Closure Certification Report (LANL 2003h).

results submitted to NMED, along with an addendum. A Corrective Measures Study Report for MDA H was completed in May 2003 (LANL 2003b) and an environmental assessment in June 2004 (DOE 2004b). The recommended corrective remedy was capping with an evapotranspiration cover, although DOE also addressed the corrective measure alternatives of removal, and partial or complete encapsulation of the shafts. Complete encapsulation was selected by NMED, along with installation of an engineered evapotranspiration cover and a soil vapor extraction system (NMED 2007a).

For the removal alternative, the above documents present conceptual designs for the structural and site changes needed to facilitate removal (see **Figure I–19**) (DOE 2004b). Pre-excavation activities include: modification and provision of utilities; delivery of a construction trailer and portable toilets; construction of a waste sorting and declassification structure, including a storage vault; erection of excavation tenting and moisture protection around the shaft area; installation of an enclosed conveyor system; establishment of an overburden storage area; relocation and expansion of the site security fence; an access road between the sorting and declassification, characterization, and packaging operations; and maintaining an exclusion area.

Waste removal using a crane was considered a safety hazard. Backhoes would not have been able to dig sufficiently deep to recover all waste. Therefore, site excavation was to proceed by removing waste laterally in 5-foot (1.5-meter) lifts: Two trenches would be excavated parallel to the shafts and on both sides to depths of 3 to 5 feet (0.9 to 1.5 meters). The trenches would be dug to within 18 to 24 inches (45 to 60 centimeters) of the shafts but would not breach the shaft or shaft contents. The waste in the top lift would be removed. Then the two trenches would be excavated another 3 to 5 feet (0.9 to 1.5 meters) and the next layer of waste removed. This process would be repeated until all the waste was removed. The trenches would be benched at a distance of 5 feet (1.5 meters) horizontally for every 15 to 20 feet (4.6 to 6 meters) of depth. The tuff adjacent to the shafts would be dug to 62 feet (18.9 meters) below ground surface. The complete, excavated footprint would measure 260 by 120 feet (78 by 36 meters) at the bottom of the excavation and 290 by 150 feet (87 by 45 meters) at the top of the excavation. Roughly 50,000 cubic yards (38,000 cubic meters) of uncontaminated tuff would be removed from the two trenches (DOE 2004b).

Because of the possible hazard of reaction of materials such as lithium hydride, high explosive, and pyrophoric uranium hydride, different options were considered for minimizing the hazard. One option was to perform removal under a tented enclosure using a computer-controlled, remotely operated, tracked hydraulic excavator to remove potentially reactive materials. A second option was to remove the waste by operating the excavator inside an enclosure filled with an inert gas such as nitrogen. This option would maintain an atmosphere having a sufficiently low level of oxygen to manage the possibility of an unwanted reaction with oxygen. Under either option, nonsparking tools and chemical “sniffers” would be used (DOE 2004b).

Wastes removed from the shafts would be conveyed by the conveyor system to the sorting and declassification area where the waste would be checked for hazard (radiation level, fire, explosion potential). Materials requiring declassification would be shredded or crushed to declassify the materials and to reduce volume. The conveyor would be designed to convey the wastes in an inert atmosphere, if needed. The conveyor could consist of a series of units containing gloveboxes terminating in a visual inspection station (see **Figure I–20** [DOE 2004b]).

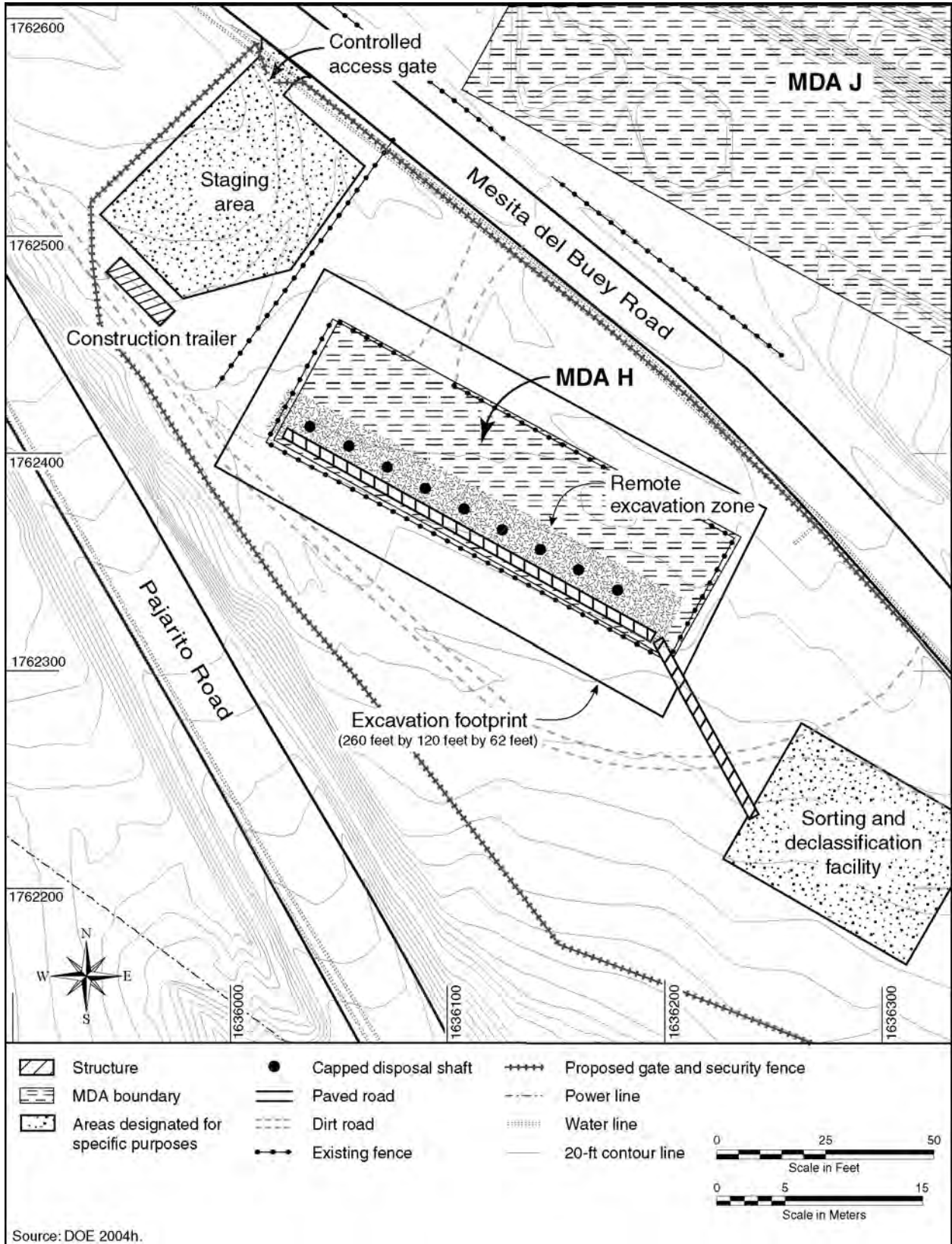


Figure I-19 Closeup View of Conceptual Site Changes to Facilitate Complete Excavation and Removal Corrective Measure Option



Figure I-20 Example of a Remotely Operated Dismantling System and Inspection Station

The inspection station would be remotely controlled, if needed, and contain manipulator arms, tools, and equipment to characterize the wastes and declassify and dismantle materials. Reactive material would be maintained in an inert environment before treatment (for example, high explosive would be safely burned). The enclosed conveyance system would move waste into a packaging and sorting area for placement of the wastes into containers (DOE 2004b).

After excavation and waste sorting is complete, the site would be restored. Stored overburden would be placed back in the hole and additional fill would be trucked in. After grading the filled area, stored topsoil would be reused and the site revegetated (DOE 2004b).

Removal would require 6 months to design and 40 months to implement. Total time for the removal operation would be 48 months. Excavation of the shafts would require 75 to 85 workers during the 48-month implementation period (DOE 2004b).⁴²

I.3.3.1.3.3 Observations from Case Histories

Several observations can be made from the above case histories and analyses, including the following:

- Existing case histories are for relatively shallow disposal units. The radiation levels associated with most actual removals have been relatively low.
- Excavation can be dangerous and slow. There can be frequent problems to work around.

⁴² Upgrading the existing cap, or installing an engineered cover, would require 10-12 workers for 5 months. Partial or complete encapsulation of the shafts would require 24 to 38 workers for 12 months (DOE 2004b).

- Unexpected conditions (such as the need to exhume explosives) can greatly increase the risk of removal, time required to complete removal, and expense for removal.
- Excavation of shafts can require a considerable amount of soil disturbance.

Some additional observations and comparisons can be made for the large LANL MDAs:

- The large MDAs considered in this appendix are generally deeper than those analyzed (except for MDA H).
- The large MDAs considered in this appendix frequently contain transuranic and other radionuclides and often present external radiation hazards.
- The large MDAs considered in this appendix are often nearby other, operating facilities.

I.3.3.2 Options for Remediation of Material Disposal Areas

The two major options for remediation of the MDAs are stabilization in place (Section I.3.3.2.1) and removal (Section I.3.3.2.4). Remediation of any MDA may be a combination of treatment methods.

I.3.3.2.1 Stabilization-in-Place Option

An engineered evapotranspiration cover would be placed over the MDAs using standard construction equipment. Cover placement would include best management practices. Site monitoring and maintenance would be performed thereafter.

Disposal practices at LANL have generally been performed in a manner that has reduced short-term subsidence. At most disposal trenches and pits, waste was placed in layers that were covered with thin layers of tuff and compacted. Much waste was not containerized. This reduced subsidence compared to that from adding backfill and cover to pits or trenches filled with waste. Additional measures to enhance stabilization of the MDAs could include in situ grouting or waste encapsulation, or dynamic compaction. Implementing these measures would invoke tradeoffs such as safety concerns, costs, and the time to install a final cover.

I.3.3.2.1.1 Operational Elements

Operational elements are presented in the text box.

Preliminary site work is assumed to include planning and permitting; demolishing or relocating existing operations, structures, or materials (as needed); rerouting or modifying utilities or pipelines (as needed); mobilization of equipment; and initial site preparation. It is assumed that a management area would be established near the MDA for staging heavy equipment and vehicles. A trailer or similar structure would be temporarily sited for management of operations. The size of the management area may depend on the size of the MDA and the complexity of closure operations, but would probably not, for most MDAs, exceed a few thousand square feet. An area for parking personal vehicles would be needed; in most cases probably in existing nearby parking lots or areas nearby the MDA. Utilities would be made available; for example, by accessing

existing utilities in the vicinity of the MDA. Water may need to be delivered by truck at some MDAs. Portable toilets would be installed in the management area, and sanitary waste from the toilets would be trucked to a disposal location either on or offsite.

Capping Operational Elements

- *Design, Planning, and Permitting* – Includes planning for site operations, including equipment and personnel coordination. Includes health and safety plans, site security plans, erosion control plans, and others. Includes permits and authorizations.
- *Demolishing/Relocating Existing Operations, Structures, or Materials* - Includes moving, demolishing, or relocating existing structures or operations.
- *Rerouting/Modifying Utilities, Pipelines, or Similar* – Includes rerouting or modifying water, electrical, telephone, or other underground or overhead lines as needed to preclude damage. Includes removal or rerouting of liquid waste or chemical piping to preclude damage.
- *Mobilization* – Includes mobilization and initial site placement of equipment such as cranes, backhoes, dump trucks, water trucks, and graders. Includes installation of a site management trailer. Includes site storage of equipment and initial mobilization of the workforce.
- *Site Preparation* – Includes explorations needed to determine the specific locations of disposed wastes, and other site-specific studies and tests such as removal of areas of surface contamination. Includes clearing of vegetation. Includes the demolition or removal of asphalt or other hard covers over disposal units. Includes removal and disposal of existing security fencing.
- *Perform Special Activities* – Includes activities unique to a specific MDA. For MDA A, it includes stabilizing the buried General's Tanks.
- *Install Moisture Monitoring System* – Before cover installation, includes the possible placement of moisture detection probes at selected locations, as well as ancillary equipment.
- *Regrading/Evaportranspiration Cover Installation/Revegetation* – Includes placement of the cover, including spreading and fine-grading of topsoil, compaction using heavy construction equipment, watering for dust abatement, and watering of planted areas for vegetation germination at approved levels.
- *Install New Fencing/Gate* – Includes security fencing with a gate large enough for vehicle passage, as well as appropriate signage.
- *Demobilization* - Includes demobilization of equipment such as backhoes, dump trucks, water trucks, and graders. Includes removal of the management trailer.
- *Health and Safety* – Includes development of a site health and safety plan; performing surface sampling confirming nonhazardous site conditions; monitoring site activities; and conforming to standard construction health and safety policies, laws, and procedures.
- *Project Management* – Includes an onsite project manager or foreman, who reports daily site progress, as well as site office support. Includes, as needed, specialists such as an evapotranspiration specialist for confirmation of material placement.
- *Monitoring and Surveillance* – Includes semiannual site visits to repair fencing and covers, eruption control, etc.

Areas may be needed for stockpiling cover materials before emplacement, as well as areas for packaging, characterizing, and storing wastes generated as part of preliminary operations or cover installation. The sizes of these support areas will depend on factors such as operational or impact mitigation considerations (such as minimizing delivery of bulk materials during times of high traffic density), the scope of needed preliminary demolition work, and the expected volumes of wastes to be generated. For example, capping MDAs in TA-21 would be accompanied by operations to remove nearby structures (see Section I.3.3.2.2.1), which would generate wastes

requiring temporary management before transport to a disposal facility. Areas for stockpiling cover materials, or overburden removed as part of initial preparation, would be protected from erosion or runoff, from airborne dispersion, and from possible cross contamination. Temporary roads may be needed between the MDA and the support areas.

Preliminary site work is also assumed to include removal of fencing to allow for site grading and placement and compaction of cover materials. This fencing may or may not be contaminated. In some cases, it may be reused; in others disposed of as waste. (The latter is conservatively assumed at large MDAs.) But depending on the size of the MDA, only portions of the fence may require removal, and removal might occur as part of the cover placement process as different sections of the MDA are sequentially addressed. For security, temporary fencing could be placed at fence openings and moved as needed.

Several of the MDAs are partially covered by asphalt or concrete. Before capping commences, this material may be removed or broken into rubble and covered. In other MDAs, such as those in TA-21, several buildings or structures may require removal. Removal of buildings and structures in TA-18 and TA-21 is addressed in, Sections H.1 and H.2, respectively, of Appendix H.

Assumptions for packaging and transporting wastes generated from capping MDAs are presented in Section I.3.5.

Capping includes placement of the cover, including spreading and fine-grading of topsoil, compaction using construction equipment, watering for dust abatement, and watering of planted areas for vegetation germination at approved levels. The Capping Option may include the installation of moisture monitoring systems, including moisture detection probes and ancillary equipment, at some of the MDAs (LANL 1999b). Each moisture monitoring system would consist of several Time Domain Reflectometry probes placed at selected locations, and a data collection center at each MDA (or group of adjacent MDAs), including a data logger, remote data access, associated solar equipment to operate the data center, and a tipping bucket rain gauge to monitor precipitation.

Because past site investigations at the MDAs have shown incidents of low levels of contamination in surface soil, capping may be preceded by efforts to remove localized pockets of radioactive or hazardous constituent contamination.

The design of each evapotranspiration cover would be tailored to each MDA based on an analysis of the potential for erosion, runoff and runoff, precipitation rate, evapotranspiration, and biointrusion (see, for example, Appendix C of the *MDA Core Document* [LANL 1999b]). At all MDAs, the cover would be a mixture of tuff, gravel, cobbles, and soil amendment or compost. Each cover would be contoured to promote runoff without erosion. Cover thicknesses would be typically larger toward the centers of the footprints of the disposal units. Covers would extend beyond the footprints of the disposal units, and taper at shallow angles.

Because final cover designs for the MDAs are still being developed, a range of average thicknesses was assumed to determine cover material volumes. Consistent with a recent survey of sources for borrow materials for cover materials (Stephens 2005), it was assumed that each

cover over each MDA would consist of either 3 feet (0.9 meters) or 8.2 feet (2.5 meters) of crushed tuff or similar material. For either assumed thickness, it was assumed that subgrade fill may be required. It was also assumed that the final cover over each MDA would include additional materials such as cobbles, gravel, topsoil, or soil amendment. It was assumed that the thickness of additional material would be about 10 percent of the base (crushed tuff) thickness.

I.3.3.2.1.2 Closure of Material Disposal Area G within Area G of Technical Area 54

The current schedule for the Consent Order requires submittal of a remedy completion report for MDA G within TA-54 by December 6, 2015. Closure of MDA G will be coordinated with closure of disposal units in the current 63-acre Area G footprint that are not subject to the Consent Order. Existing waste stored within Area G will require recovery, and existing waste management operations will require relocation. Closure of MDA G will be closely coordinated with closure of MDA L, which is addressed in Section I.3.3.2.1.3. The transition of waste management operations from current locations in Areas G and L so that Areas G and L can undergo closure is analyzed in Appendix H, Section H.3.

I.3.3.2.1.2.1 Overview

Area G within TA-54 is used for a variety of radioactive waste management operations. Belowground radioactive waste storage and disposal units are listed in **Table I-34** (LANL 2005k). They include:

- Numerous trenches, pits, and shafts containing radioactive waste subject to corrective action under the Consent Order (MDA G). Early disposal units may contain transuranic isotopes in concentrations exceeding current transuranic waste definitions.
- Two subsurface disposal units subject to closure under RCRA.
- Active disposal units for low-level radioactive waste that do not contain mixed low-level radioactive waste. These disposal units are neither permitted under RCRA nor subject to corrective action under the Consent Order.

Other waste management operations include radioactive waste storage; low-level radioactive waste characterization, verification, and compaction capacity; and capacity for characterizing, processing, and shipping contact-handled transuranic waste. This existing capacity is addressed in a 2005 TA-54 status report (LANL 2005k).

Waste management activities within Area G occur within structures having systems and components designed and constructed in accordance with DOE's systems of hazard and performance categorization (DOE 1993, 1997b). LANL staff conducts operations in a manner that restricts the aboveground inventory of radioactive materials within individual structures and over all of Area G. The limit for all aboveground activity in Area G, including stored waste, is 150,000 plutonium-239-equivalent curies (LANL 2006a).

Table I-34 Belowground Storage and Disposal Units at Area G

| <i>Atomic Energy Act-Regulated Storage and Disposal Units</i> | | <i>Corrective Action Storage and Disposal Units^a</i> | | <i>RCRA Storage and Disposal Units</i> |
|--|---|---|--|---|
| <i>Low-level Radioactive Waste Disposal</i> | <i>Transuranic Waste Storage</i> | <i>Waste Disposal</i> | <i>Transuranic Waste Storage</i> | |
| Pits 15, 38, 39 Shafts 21, 23, 97, 137, 141-144, 147-149, 161-177, 197, 300, 301, 307, 308, 360-367, 369, 370 Shafts C11, C14, 321, 323, 325, 327, 329, 331, 333, 335, 339, 341, 343, 345, 347, 349, 351, 355, 357 Shafts ^b 309, 311, 313, 317, 319, 337, 353, 359 | Shafts 235-243, 246-253, 262-266, 302-306 | Pits 1-10, 12, 13, 16-22, 24-30, 32-33, 35-37 Pit 31 Shafts C1-C10, C12, C13, 1-20, 22, 24-96, 99-112, 114, 115, 118-123, 125-136, 138-140, 150-160, 189-192, 196 | Pit 9 Trenches A-D Shafts 200-232 Shaft 233 ^b Transuranic waste corrugated metal pipes (stored atop Pit 29) | Pit 29 (below storage of transuranic waste corrugated metal pipes) Shaft 124 |

RCRA = Resource Conservation and Recovery Act.

^a Units regulated under RCRA and Corrective Action Requirements are also regulated by DOE under the Atomic Energy Act.

^b Unused and empty.

Source: LANL 2005k.

Closure of MDA G within the constraints of the Consent Order would occur as waste management operations and facilities are transitioned from Area G as described in Section H.3. This would include the removal of transuranic wastes stored underground. The removal of these operations and facilities will occur in a phased approach, as described in **Table I-35**, that would allow closure activities to begin without waiting for all waste management operations and facilities to be removed (LANL 2005k).

While MDA G is being closed, new low-level radioactive waste disposal capacity would be developed, initially into Zone 4 at TA-54, and then into Zone 6 at TA-54 as needed. Six buildings across from Area L would be removed. A new guard and access station would be constructed. A waste characterization and verification facility would be constructed, as would a new low-level radioactive waste compactor facility (LANL 2005k).

I.3.3.2.1.2.2 Options for Remote-Handled Transuranic Waste

Shafts 200-232 within Area G are 33 1-foot-diameter (0.3-meter-diameter) shafts having carbon steel pipe liners that contain high-activity remote-handled transuranic waste. The environmental impacts associated with removal of this waste from 3 shafts, which would require a temporary facility to be constructed over the shafts, are analyzed in Appendix H, Section H.3.

Another option is to leave the waste in place consistent with health, safety, and environmental analyses in accordance with all applicable regulatory standards. In addition to any analyses performed as part of the Consent Order process, for example, an analysis may be required pursuant to 40 CFR Part 191, EPA’s “Environmental Standards for the Management and

Disposal of Spent Nuclear Fuel, High-Level and Transuranic Radioactive Wastes.” The analysis must provide a reasonable expectation that the following quantitative criteria will be met:⁴³

Table I–35 Closure Phases for Existing Area G Footprint

| |
|--|
| <p>Phases 1 and 2 (Western Portion): Retrieve contact-handled transuranic waste from Pit 9, from Pit 29, and from aboveground storage structures. Characterize and ship 5,500 cubic yards (4,200 cubic meters) of formerly stored and newly generated transuranic waste. Relocate low-level radioactive waste characterization and verification operations. Clean-close or decontaminate and decommission 66 structures. Modify infrastructure such as power lines and fences, as needed. Construct a final cover.</p> |
| <p>Phases 3 and 4 (Central Portion): Retrieve contact-handled transuranic waste from Trenches A-D and from aboveground storage structures. Retrieve remote-handled transuranic waste from five shafts (shafts 302-306). Characterize and ship 2,600 cubic yards (2,000 cubic meters) of formerly stored and newly generated transuranic waste. Relocate low-level radioactive waste compactor operations. Clean-close or decontaminate and decommission 18 structures. Modify infrastructure, as needed. Construct a final cover.</p> |
| <p>Phases 5 and 6 (Eastern Portion): Retrieve contact-handled transuranic waste from aboveground storage structures. Retrieve contact-handled transuranic waste from 5 shafts (shafts 262-266). Retrieve remote-handled transuranic waste from 17 shafts (shafts 235-243 and 246-254). Retrieve remote-handled transuranic waste from 33 shafts (shafts 200-232). If necessary, construct a remote-handled facility for waste retrieval and processing for shipment. Alternatively, leave remote-handled waste in place if compliant with a 40 CFR Part 191 analysis. Characterize and ship 5,000 cubic yards (3,800 cubic meters) of formerly stored and newly generated transuranic waste. Construct a transuranic facility outside of Area G for newly generated transuranic waste. Clean-close or decontaminate and decommission 31 structures. Modify infrastructure, as needed. Construct a final cover.</p> |

CFR = Code of Federal Regulations.

Source: LANL 2005k.

- Containment criterion – A limit on the total quantities of particular radionuclides hypothetically released into the accessible environment over 10,000 years following waste disposal. (Allowable projected releases are scaled to the initial inventory. Because the shafts have a small inventory, allowable projected releases would be very small.)
- Individual protection criterion – An annual dose limit (15 millirem in a year) to individuals in the accessible environment for 10,000 years following waste disposal.
- Groundwater protection criterion – A requirement to project compliance with drinking water maximum contaminant levels in the accessible environment for 10,000 years following waste disposal.

The final configuration of the disposal unit containing the wastes would be designed in compliance with all required analyses and regulatory standards. Further stabilization or containment of the waste, using technologies such as in situ grouting or in situ vitrification, or modifications to the design and installation of the final cover, may be required.

⁴³ 40 CFR Part 191 also contains qualitative requirements pertaining to the use of active and passive institutional controls, monitoring, resource avoidance, and so forth.

Additional analyses would be needed to make a decision on this option. It may be noted, however, that possible consequences of leaving contact- and remote-handled transuranic waste in place at LANL were addressed as part of a NEPA analysis prepared in support of disposal of transuranic waste at WIPP (DOE 1997a). This NEPA analysis addressed the consequences of leaving transuranic waste in place as part of a No Action Alternative considered in the *WIPP Disposal Phase Supplemental Environmental Impact Statement (SEIS-II)* (DOE 1997a), based on an analytical model developed by Pacific Northwest National Laboratory (PNNL 1997). *SEIS-II* considered stored and previously buried waste at seven generator-storage sites, including LANL. Stored waste configurations included soil-covered configurations and surface-stored configurations, such as storage in buildings. The analysis considered the consequences that could hypothetically occur assuming that waste at the generator-storage sites would be stored indefinitely into the future, and that loss of institutional control at the generator-storage sites would occur after 2133. Consequences included those that may be experienced by a future inadvertent human intruder into the stored and previously buried waste, and those that may result from long-term release into the environment. The analysis addressed radiological doses and risks, as well as impacts of exposure to chemical carcinogens and noncarcinogens (DOE 1997a).⁴⁴ The preferred alternative and decision (63 FR 3624) was to dispose transuranic waste in WIPP. WIPP disposal capacity is expected to be sufficient for disposal of all retrievably stored transuranic waste and all newly generated transuranic waste from the DOE complex over the next few decades, but not sufficient for this waste plus all transuranic waste buried before 1970 across the DOE complex.

Buried waste intrusion scenarios included the driller and gardener scenarios (DOE 1997a):

- *Driller*. A hypothetical intruder drills a well directly through buried or soil-covered waste to underlying groundwater, bringing contaminated soil to the surface that is mixed with topsoil.
- *Gardener*. A gardener farms a garden on the land containing the contaminated soil following the drilling incursion.

Surface-stored waste intrusion scenarios included the scavenger and farm family scenarios (DOE 1997a):

- *Scavenger*. A hypothetical scavenger intruder comes into direct contact with surface-stored transuranic waste over a 24-hour period.
- *Farm Family*. A hypothetical farm family of two adults and two children lives and farms on the land immediately over the former surface-stored transuranic waste area.

Populations and individuals living near the generator-storage sites were assumed to be impacted by long-term environmental release of contaminants. The following two scenarios were used to evaluate impacts on the maximally exposed individual (MEI) of chronic long-term environmental releases (DOE 1997a):

⁴⁴ The analysis is described in detail in Appendix I of *SEIS-II*, which is available for viewing at the WIPP Internet site, www.wipp.energy.gov.

- *Groundwater exposure.* The MEI from a farm family lives 980 feet (300 meters) downgradient of a waste storage area. The family grows and consumes their own crops and livestock and uses contaminated groundwater for drinking water and for watering the crops and livestock. This receptor was considered for long-term release from buried or soil-covered transuranic waste and surface-stored transuranic waste.
- *Air Pathway Exposure.* A hypothetical individual was assumed to be exposed to the maximum airborne contaminant concentration released from a stored transuranic waste site. This receptor, located at least 330 feet (100 meters) from the site but within a 50-mile (80-kilometer) radius, was considered only for long-term releases from surface-stored transuranic waste.

Offsite populations within 50 miles (80 kilometers) of the sites were assumed to be exposed via atmospheric transport of radionuclides or by contamination of surface water (used for drinking water) from releases to the groundwater pathway. (Population exposures from the groundwater-surface water pathway were not considered for LANL.) Long-term releases from both buried or soil-covered transuranic waste and surface-stored transuranic waste were included (DOE 1997a).

Analyses were performed using the modular risk analysis method used in the DOE waste management programmatic environmental impact statement and the GENII and MEPAS computer codes. Site-specific radionuclide inventories were developed for each generator-storage site, and a typical inventory of organic and inorganic constituents was considered for all generator-storage sites. The results of the analysis for a future inadvertent intruder into buried and stored transuranic waste at LANL are presented in **Table I–36**. Maximum lifetime MEI and population impacts calculated for long-term releases to the environment are summarized in **Table I–37**. Noncarcinogenic impacts were determined to have a maximum Hazard Index of 1.7×10^{-3} , principally from mercury through the resuspended soil ingestion pathway (DOE 1997a).

Table I–36 Inadvertent Future Intruder Impact Summary

| | <i>Intrusion into Buried Waste</i> | | | | <i>Intrusion into Surface-Stored Waste</i> | | | |
|--|------------------------------------|-----------------------|-----------------------------|-----------------------|--|---------------------|-----------------------------|---------------------|
| | <i>Contact-Handled Waste</i> | | <i>Remote-Handled Waste</i> | | <i>Contact-Handled Waste</i> | | <i>Remote-Handled Waste</i> | |
| Impact measure | Driller | Gardener ^a | Driller | Gardener ^a | Scavenger | Farmer ^b | Scavenger | Farmer ^b |
| Dose (rem) | 4.5×10^{-3} | 41 | 2.2×10^{-3} | 6.1 | 6.58 | 2,400 | 1.39 | 550 |
| Radiological LCF | 2.3×10^{-6} | 0.021 | 1.1×10^{-6} | 3.6×10^{-3} | 3.3×10^{-3} | 1.2 | 6.9×10^{-4} | 0.27 |
| <i>Hazardous Chemical Impacts</i> | | | | | | | | |
| PEL ^c | | | | | | | | |
| Cadmium | 9.8×10^{-2} | | 9.8×10^{-2} | | 5.2 | | 5.2 | |
| Beryllium | 17 | | 17 | | 91 | | 91 | |
| Lead | 27 | | 3,000 | | 1,400 | | 160,000 | |
| Mercury | 12 | | 12 | | 6.2 | | 6.2 | |
| <i>Hazard Quotient/Index</i> | | | | | | | | |
| Cadmium | | 0.01 | | 0.01 | | 15 | | 15 |
| Beryllium | | 0.08 | | 0.08 | | 10 | | 10 |
| Lead | | 36 | | 3,900 | | 50,000 | | 5.2×10^6 |
| Mercury | | 77 | | 77 | | 100,000 | | 100,000 |

| | <i>Intrusion into Buried Waste</i> | | | | <i>Intrusion into Surface-Stored Waste</i> | | | |
|-------------------------|------------------------------------|----------------------|-----------------------------|----------------------|--|------|-----------------------------|------|
| | <i>Contact-Handled Waste</i> | | <i>Remote-Handled Waste</i> | | <i>Contact-Handled Waste</i> | | <i>Remote-Handled Waste</i> | |
| Cancer Incidence | | | | | | | | |
| Cadmium | 1.4×10^{-9} | 2.0×10^{-5} | 1.4×10^{-9} | 2.0×10^{-5} | 2.0×10^{-6} | 0.02 | 2.0×10^{-6} | 0.02 |
| Beryllium | 1.3×10^{-7} | 1.0×10^{-4} | 1.3×10^{-7} | 1.0×10^{-4} | 2.0×10^{-4} | 1.9 | 2.0×10^{-4} | 1.9 |

LCF = latent cancer fatality, PEL = permissible exposure limit.

^a Impact measures for the gardener are totals over 30 years.

^b Impact measures for the farmer are for the first year of intrusion.

^c Air concentrations exceeding PEL – that is, “17” means 17 times the PEL.

Note: From the *Waste Isolation Pilot Plant Disposal Phase Final Supplemental Environmental Impact Statement* (DOE 1997a) No Action Alternative 2 Analysis.

Source: DOE 1997a.

Table I-37 Maximum Lifetime Maximally Exposed Individual and Population Impacts after Assumed Loss of Institutional Control

| <i>Receptor</i> | <i>Radiological Impacts</i> | | | <i>Chemical Carcinogenic Impacts</i> | |
|-----------------|---|---------------------------------|-------------------------|--------------------------------------|----------------------------|
| | <i>Lifetime Dose (rem per 70 years)</i> | <i>Lifetime LCF^a</i> | <i>Dominant Pathway</i> | <i>Lifetime Cancer Incidence</i> | <i>Dominant Pathway</i> |
| MEI | 0.09 | 4.5×10^{-5} | Inhalation | 2.4×10^{-4} | Resuspended soil ingestion |
| Population | 162 | 8.1×10^{-2} | Inhalation | 2.4×10^{-4} | Resuspended soil ingestion |

LCF = latent cancer fatality, MEI = maximally exposed individual.

^a Lifetime LCF is the probability of an LCF for an MEI and the number of LCFs in a population.

Note: From the *Waste Isolation Pilot Plant Disposal Phase Final Supplemental Environmental Impact Statement* (DOE 1997a) No Action Alternative 2 Analysis.

Source: DOE 1997a.

I.3.3.2.1.2.3 Final Stabilization of Area G

Stabilization of the existing 63-acre Area G footprint will proceed in three separate periods. In each of these periods, after removal of structures in the specific area to be covered, the area would be graded and capped. In addition, a soil vapor extraction system would be placed in Area G to remove and treat the volatile organic compound plume at the eastern portion of the MDA (LANL 2005k).

Waste Generation. It was postulated that small quantities of waste would be generated as part of capping MDA G and other disposal units in the existing 63-acre footprint of Area G. These volumes were estimated by assuming that the fencing currently surrounding the MDA is removed and disposed of as waste, and that the concrete and asphalt covering a portion of the site is removed and disposed of as waste. However, the fencing may actually be recycled or reused, and the asphalt and concrete may actually be broken up and buried beneath the final cover. See Section I.3.3.2.2.1 for estimated volumes.

Bulk Materials for Area G Final Cover. The cover for the existing 63-acre Area G footprint is being developed with the support of the updated Area G performance assessment and composite analysis. The final cover would cover all disposal units in the existing footprint, including the active and inactive disposal units that are subject to RCRA closure and the Consent Order (LANL 2005k), and is assumed to cover 65 acres (Stephens 2005). The cover design and thickness will be consistent with a final stabilization analysis that will evaluate alternatives such

as stabilization of specific pits before installation of a final cover. The current cover ranges considerably in thickness. A 2002 report proposed increasing the thickness of the interim cover by 4.6 to 7.9 feet (1.4 to 2.4 meters), resulting in a fairly uniform final thickness of about 11.2 feet (3.4 meters) (LANL 2002b).

The current conceptual design for the cover includes the following materials (DOE 2005a):

- Crushed tuff – 514,000 cubic yards (393,00 cubic meters)
- Imported cap material (crushed tuff from another location) – 818,000 cubic yards (625,000 cubic meters)
- Imported clay – 80,000 cubic yards (61,000 cubic meters)
- Imported rock – 167,000 cubic yards (128,000 cubic meters)
- Imported rock armor – 70,000 cubic yards (54,000 cubic meters)
- Imported top soil or soil amendment – 65,000 cubic yards (50,000 cubic meters)
- Pea gravel – 25,000 cubic yards (19,000 cubic meters)
- Surface area for vegetation, mulch, and fertilizer – 80 acres (32 hectares)

This design is assumed to represent the higher end of a reasonable range of possible thicknesses—that is, the thickness of the crushed tuff (514,000 + 818,000 = 1,332,000 cubic yards [1,018,000 cubic meters]) represents a maximum thickness of 8.2 feet (2.5 meters). Again, cover thickness would vary to promote drainage. A thinner cap (about 3 feet [1 meter]) would imply about 487,000 cubic yards (372,000 cubic meters). For this appendix, it was assumed that the additional clay, rock, topsoil, and other material would be roughly similar for either a thin or a thick cover. The minimum and maximum material and shipment requirements assumed in this appendix are listed in **Table I–38**.

Table I–38 Estimated Cover Materials for Material Disposal Area G and Other Area G Disposal Units

| <i>Materials</i> | <i>Thin Cover</i> | | | <i>Thick Cover</i> | | |
|----------------------|--------------------------------------|---|--------------------------|--------------------------------------|---|--------------------------|
| | <i>In-Place Volume (cubic yards)</i> | <i>Delivered Quantities^a</i> | | <i>In-Place Volume (cubic yards)</i> | <i>Delivered Quantities^a</i> | |
| | | <i>Cubic Yards</i> | <i>One-Way Shipments</i> | | <i>Cubic Yards</i> | <i>One-Way Shipments</i> |
| Tuff | 487,000 | 643,000 | 38,000 | 1,330,000 | 1,760,000 | 104,000 |
| Additional Materials | 407,000 | 537,000 | 32,000 | 407,000 | 537,000 | 32,000 |
| Total | 894,000 | 1,180,000 | 70,000 | 1,740,000 | 2,300,000 | 136,000 |

^a Delivered quantities are based on an assumed 20 percent swell after excavation from a borrow, a density of 1.3 tons per cubic yard, a 10 percent contingency, and an average load per truck of 22 tons.

Note: To convert cubic yards to cubic meters, multiply by 0.76456. Numbers have been rounded.

I.3.3.2.1.2.4 Schedules

The following start and completion dates (and elapsed months) for the three assumed groups of Area G closure phases are used in this appendix (LANL 2005k):

- Phases 1 and 2: 10/1/2010 - 9/30/2011 (12 months);
- Phases 3 and 4: 12/1/2012 – 9/30/2013 (12 months); and
- Phases 5 and 6: 9/29/2014 – 12/28/2015 (16 months).

I.3.3.2.1.3 Closure of Material Disposal Area L within Area L of Technical Area 54

Background. All disposal units in Area L are inactive. Some subsurface disposal units (MDA L) are subject to corrective action under the Consent Order; other subsurface disposal units are RCRA-regulated units subject to RCRA closure and postclosure care. Active waste management operations include storage of mixed low-level radioactive waste and storage and processing of wastes regulated under RCRA or TSCA as described in Section H.3. This waste is managed in container storage units (CSUs) subject to RCRA permitting or interim status requirements.⁴⁵ The waste is sent offsite for further processing (as needed) and disposal. Waste management units at Area L are summarized in **Table I-39** (LANL 2005k).

Table I-39 Summary of Waste Management Units at Area L

| <i>RCRA Disposal Units</i> | <i>Corrective Action Disposal Units (MDA L)</i> | <i>Aboveground CSUs</i> | <i>Lead Stringer Shaft CSUs</i> |
|--|---|---|---------------------------------|
| Shafts 1, 13-17, and 19-34 Impoundments B and D | Shafts 2-12 and 18 Pit A Impoundment C | 54-215, 54-216, 54-31, 54-32, 54-35, 54-36, 54-58, 54-68, 54-69, 54-70, 54-39, and Area L CSU | Shafts 36 and 37 |

RCRA = Resource Conservation and Recovery Act, MDA = material disposal area, CSU = container storage unit.
Source: LANL 2005k.

The RCRA disposal units are inactive subsurface units used for hazardous waste disposal after the effective date of the RCRA hazardous waste management regulations. They are subject to RCRA closure and postclosure requirements under 40 CFR Part 264. Some of these disposal units have been previously identified as being subject to corrective action. But under the terms of the Consent Order (NMED 2005), these disposal units are not subject to corrective action but to RCRA closure and postclosure care (LANL 2005k).

In addition to remedial investigations, a pilot study has been conducted to determine the effectiveness of an extraction system for the vapor phase volatile organic compound plume under the site (LANL 2005k, 2006m). A January 2008 Corrective Measures Report to NMED recommended a corrective remedy incorporating an engineered evapotranspiration cover, a soil vapor extraction system, monitoring, and maintenance (LANL 2008a).

Scope of Closure. The intent is to close in a single integrated action those subsurface disposal units regulated under RCRA and those subject to corrective action. Closure would be performed in a manner allowing for continued use of Area L for hazardous and toxic waste treatment and

⁴⁵ Container storage units at MDA L are described in Attachment G of the LANL TA-54 Part B Permit Renewal Application (LANL 2003h).

storage. To accomplish this, waste management operations would need to be either altered so a smaller area is impacted, or completely removed. These changes to waste management operations are described and analyzed in Appendix H, Section H.3.

Closure activities analyzed in this appendix include capping of the subsurface disposal units and treating the subsurface volatile organic compound vapor plume under the site. One option would be to emplace two separate covers. One cover would envelop the pit and three impoundments and the lines of shafts to the south of Pit A. A second cover would cover the six shafts at the northwest portion of the site. As a second option, a single cover may be installed covering the pits, impoundments, and all shafts except for the lead stringer shafts.

The corrective measure determined by NMED may include removal of some or all of the subsurface units subject to corrective action. In this case, closure and future use plans would require modification.

Waste Generation While Capping. It was postulated that small quantities of waste would be generated as part of capping MDA L. These volumes were estimated by assuming that a portion of the fencing currently surrounding Area L would be removed and disposed of as waste, and that the concrete and asphalt covering a portion of the site would be removed and disposed of as waste. However, the fencing may be recycled or reused, and the asphalt and concrete may be broken up and buried beneath the final cover. See Section I.3.3.2.2.1 for estimated volumes.

Materials for Site Stabilization. The final cover for MDA L is being developed. The 2005 Status Report for TA-54 envisions two 3-foot-thick alternative RCRA covers (LANL 2005k). However, for conservatism, a single large cover was assumed consistent with the 2005 Borrow Source Survey (Stephens 2005).

The Stephens report prepared preliminary designs for MDAs C and L (Stephens 2005). The materials required under this proposal for MDA L are listed in **Table I-40**, assuming two thicknesses of cover. Although the ultimate design for MDA L may differ from that described by Stephens, the range in thicknesses should bound the volumes of bulk cover material that may be required (Stephens 2005). The two thicknesses—i.e., either 3 feet (1 meter) or 8.2 feet (2.5 meters)—refer to the thickness of the fill before addition of topsoil, rock armor, or similar material. Adding this material would add about 10 percent to the final thickness.

Placement of this cover may require removal of a gabion retaining wall that exists along the northern and eastern site boundaries to meet the requirement for cover longevity (Stephens 2005).

Schedules. In its January 2008 Corrective Measures Evaluation Report for MDA L, DOE proposed a DD&D schedule starting in fall 2008 and continuing through 2010; the proposed capping schedule was to start in Spring 2011 and extend through Spring 2012 (LANL 2008a). The actual remediation scope and schedule will depend on decisions made by NMED.

Table I-40 Bulk Materials for Material Disposal Area L Final Cover

| Material | Three-Foot Cover | | | | Eight-Foot Cover | | | |
|---|-------------------------------|-----------------------------------|--------|-------------------|-------------------------------|-----------------------------------|--------|-------------------|
| | In-Place Volume (cubic yards) | Delivered Quantities ^a | | | In-Place Volume (cubic yards) | Delivered Quantities ^a | | |
| | | Cubic Yards | Tons | One-Way Shipments | | Cubic Yards | Tons | One-Way Shipments |
| Soil rooting medium | 5,052 | 6,669 | 8,670 | 394 | 26,153 | 34,522 | 44,879 | 2,040 |
| Topsoil | 1,344 | 1,774 | 2,306 | 105 | 1,918 | 2,532 | 3,291 | 150 |
| Select fill | 2,942 | 3,883 | 5,048 | 229 | 2,784 | 3,675 | 4,777 | 217 |
| Gravel | 134 | 177 | 230 | 10 | 192 | 253 | 329 | 15 |
| Cobbles | 134 | 177 | 230 | 10 | 192 | 253 | 329 | 15 |
| Angular boulders (1- to 2-foot diameter) ^b | 543 | 717 | 932 | 42 | 555 | 733 | 952 | 43 |
| Soil amendment/compost ^c | 67 | 88 | 88 | 4 | 96 | 127 | 127 | 6 |
| Total | 10,216 | 13,485 | 17,504 | 796 | 31,890 | 42,095 | 54,685 | 2,487 |

^a Delivered quantities are based on assumed 20 percent swell after excavation from a borrow, a soil density of 1.3 tons per cubic yards, and a contingency of 10 percent. Shipments are based on assumed use of trucks containing average individual loads of 22 tons (Stephens 2005).

^b Angular boulders may be optional on slopes of 25 to 33 percent.

^c Soil amendment density: 1 cubic yard = 1 ton.

Note: To convert cubic yards to cubic meters, multiply by 0.76456; tons to kilograms, multiply by 907.18.

Source: Stephens 2005.

I.3.3.2.2 Materials Requirements for Stabilizing Additional Large Material Disposal Areas

I.3.3.2.2.1 Site Preparation

Capping would be initiated by suitable site preparation, including removal of existing structures, demolition of fences surrounding the MDAs, clearing of vegetation as needed, and regrading.

Additional work would be needed at MDA T to remove many of the existing structures. Building 21-257 and associated structures (tanks) would be removed under a TA-21 DD&D program (see Appendix H, Section H.2). This would include portions of Buildings 21-005, 21-150, and all of Building 21-286, the aboveground Diesel Tank 21-57, about half of the remaining slab of Building 21-228, and Water Tower 21-342. Removal would include foundations and buried gas and water pipes because they lie within the outer 50 feet (15 meters) of the intended cap (see below). The abovegrade portion of the structures would be removed, and concrete slabs, sumps, and tank pads would be reduced to rubble and left in place along with the below-grade concrete foundations and remaining pipes. Pipes may be filled with a solidifying foam prior to terminating within 50 feet (15 meters) of the cap edge.⁴⁶ A 6-inch (0.2-meter) cross-mesa buried gas pipeline located between MDAs T and A would require relocation to the east of MDA A. Approximately 350 feet (107 meters) of pipe would be left in place after filling with solidifying foam. Another 100 feet (30 meters) of the pipe would be removed (LANL 2006a).

⁴⁶ Pipes beyond 50 feet (15 meters) would be removed under remedy programs for other solid waste management units.

At MDA A, before capping would take place, Water Tower 21-342 and abovegrade Diesel Tank 21-57 would be removed under a TA-21 DD&D program (see Appendix H, Section H.2). Removal would include foundations and buried gas and water pipes because they lie within the outer 50 feet (15 meters) of the intended cap (LANL 2006a).

For both MDA T and MDA A, removal and relocation of the perimeter road would be required, as well as electrical poles.

At MDA C, rather than removing or relocating existing buildings and pipes, retaining walls may be constructed (Stephens 2005).

For the remaining large MDAs, it was assumed that small quantities of wastes would be generated as part of final stabilization. To estimate the volumes of these wastes, it was assumed that as part of site preparation, some or all of the fencing around the MDAs would be removed and disposed of, and that some or all of the concrete and asphalt covering portions of some of the MDAs would be removed and disposed of.

Table I–41 presents the assumed volumes of solid waste produced from site preparation, where the linear footage of fencing removed was estimated based on scale drawings of the MDA sites. Also presented are the estimated volumes of waste, assuming that each 100 linear feet (30 meters) of fence generates about 2,300 pounds (1,040 kilograms) of waste (including mesh, posts, top bars, and concrete footers).⁴⁷ Assuming that the bulk density is about the same as common rubbish, then 100 linear feet (30 meters) of fencing would generate about 2.8 cubic yards (2 cubic meters) of solid waste.⁴⁸

Portions of MDAs A, B, L, and G are covered with asphalt or concrete that would be broken up or removed before installation of the site covers. Waste volumes were estimated by multiplying an assumed area removed by an assumed average thickness of 6 inches (15 centimeters). (Much of the concrete and asphalt at the MDAs is probably thinner than 6 inches [15 centimeters]).

- MDA A: Estimated upon assumption of 10 to 20 percent of surface covered with asphalt. Fifteen percent of 1.3 acres (0.53 hectare) is 8,200 square feet (762 square meters).
- MDA B: Estimated from Section I.2.5.2.2 (1,500 by 120 feet = 180,000 square feet [457 by 37 meters = 16,909 square meters]).

⁴⁷ Considered poles, top bar, mesh, concrete, and neglected fittings and gates. Assumed an 8-foot fence, with 10-foot-6-inch (3.2-meter) poles every 10 feet (3 meters). Assumed each pole was embedded in concrete footings 8 inches in diameter and 30 inches deep. From www.hooverfence.com, assumed mesh weighs 561 pounds (254 kilograms) per 100 feet (30 meters), and the weight of a 10-foot 6-inch (3.2 meter) post is 24.3 pounds (11 kilograms). Assumed the density of concrete to be 150 pounds per cubic foot (2.4 grams per cubic centimeter). Rounded addition of posts, top pole, mesh and concrete to 2,300 pounds (1,040 kilograms) per 100 feet (30 meters) of fencing.

⁴⁸ From (Reade 2005), the bulk density of common rubbish (garbage) is 480 kilograms per cubic meter (30 pounds per cubic feet).

Table I-41 Solid Waste Generation during Capping of Large Material Disposal Areas

| <i>MDA</i> | <i>Fencing Removed (linear feet)</i> | <i>Solid Waste (cubic yards)</i> |
|----------------|--------------------------------------|----------------------------------|
| A | 1,300 | 37 |
| B ^a | 4,800 | 140 |
| T | 1,500 | 43 |
| U ^b | 700 | 20 |
| AB | 450 | 13 |
| C | 6,900 | 200 |
| G ^c | 9,500 | 270 |
| L | 500 | 14 |

MDA = material disposal area.

^a These volumes are conservatively included for completeness. The current plan is to completely remove the waste in MDA B (see Section I.3.3.2.7 of this appendix).

^b These volumes are conservative because NMED has issued a Corrective Action Complete with Controls certificate for the SWMUs comprising MDA U (NMED 2006b) (see Section I.2.5.2.4 of this appendix).

^c Capping MDA G includes capping other disposal units in the existing 63-acre Area G footprint that are not subject to the Consent Order.

Note: To convert cubic yards to cubic meters, multiply by 0.76456; feet to meters, multiply by 0.3048. Numbers have been rounded.

- MDA L: Estimated by scaling from Figure B-1 of the MDA L Historical Investigation Report (LANL 2003m).⁴⁹
- MDA G: Estimated by scaling from Figure B-5 of the Investigation Work Plan for MDA G (LANL 2004c).

Except for MDA L, it was assumed that half could be disposed of as solid waste and half as low-activity low-level radioactive waste. For MDA L, it was assumed that about half would be solid waste and half chemical waste. Waste quantities are listed in **Table I-42**. (See Section I.3.5 for assumptions about shipment of waste to disposal facilities.)

Table I-42 Asphalt or Concrete Removal from Material Disposal Areas

| <i>Parameter</i> | <i>MDA A</i> | <i>MDA B</i> | <i>MDA L</i> | <i>MDA G</i> |
|---|--------------|--------------|--------------|--------------|
| Surface area (square feet) | 8,200 | 180,000 | 4,300 | 130,000 |
| Waste volume (cubic yards) ^a | 150 | 3,300 | 80 | 2,400 |
| Waste volume (cubic meters): ^b | 120 | 2,500 | 61 | 1,800 |
| Solid waste | 58 | 1,300 | 30 | 920 |
| Chemical waste ^c | | | 30 | |
| Low-level radioactive waste | 58 | 1,300 | | 920 |

MDA = material disposal area.

^a Assuming an average asphalt thickness of 6 inches (15 centimeters) and an average concrete thickness of 6 inches (15 centimeters).

^b As-shipped volumes would be larger because packaging efficiencies are less than 100 percent.

^c Includes waste regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or is otherwise unacceptable for sanitary landfill disposal.

Note: To convert square feet to square meters, multiply by 0.0929. Numbers have been rounded.

⁴⁹ Area L is currently entirely covered with asphalt. The only asphalt expected to be removed would be that needed for remediation of MDA L pursuant to the Consent Order. If all asphalt from Area L were to be removed from the 2.6-acre site, then up to an additional 1,050 cubic yards (800 cubic meters) of solid waste would be generated, as would up to an additional 1,050 cubic yards (800 cubic meters) of chemical waste. This would require up to 80 shipments of solid waste and 87 shipments of chemical waste.

I.3.3.2.2 Cover Materials

Cover material assumptions for MDA G and MDA L are provided in Sections I.3.3.2.1.2.3 and I.3.3.2.1.3, respectively. Cover assumptions for other MDAs and landfills are presented below.

Large MDAs. The Stephens report includes preliminary designs for MDA C (Stephens 2005). Materials are listed in **Table I–43**, assuming two thicknesses for fill tuff. Although the ultimate design for MDA C may differ from that described by Stephens, the range in thicknesses should bound the required volumes of bulk cover material. The two thicknesses—that is, either 3 feet (0.9 meters) or 8.2 feet (2.5 meters)—refer to the thickness of the fill before addition of topsoil, rock armor, or other material. Adding this material adds about 10 percent to the final thickness.

Table I–43 Bulk Materials for Material Disposal Area C Final Cover

| Material | Three-Foot Cover | | | | Eight-Foot Cover | | | |
|---|-------------------------------|-----------------------------------|---------|-------------------|-------------------------------|-----------------------------------|---------|-------------------|
| | In-Place Volume (cubic yards) | Delivered Quantities ^a | | | In-Place Volume (cubic yards) | Delivered Quantities ^a | | |
| | | Cubic Yards | Tons | One-Way Shipments | | Cubic Yards | Tons | One-Way Shipments |
| Soil rooting medium | 37,237 | 49,153 | 63,899 | 2,905 | 117,942 | 155,683 | 202,388 | 9,199 |
| Topsoil | 7,943 | 10,485 | 13,630 | 620 | 8,730 | 11,524 | 14,981 | 681 |
| Select fill | 51,544 | 68,038 | 88,449 | 4,020 | 51,964 | 68,592 | 89,170 | 4,053 |
| Gravel | 794 | 1,048 | 1,363 | 62 | 873 | 1,152 | 1,498 | 68 |
| Cobbles | 794 | 1,048 | 1,363 | 62 | 873 | 1,152 | 1,498 | 68 |
| Angular boulders (1- to 2-foot diameter) ^b | 1,094 | 1,444 | 1,877 | 85 | 2,911 | 3,843 | 4,995 | 227 |
| Soil amendment/compost ^c | 397 | 524 | 524 | 24 | 436 | 576 | 576 | 26 |
| Total ^d | 99,803 | 131,740 | 171,105 | 7,778 | 183,729 | 242,522 | 315,106 | 14,323 |

^a Delivered quantities are based on assumed 20 percent swell after excavation from a borrow, a soil density of 1.3 tons per cubic yard, and a contingency of 10 percent. Shipments are based on assumed use of trucks containing average individual loads of 22 tons (20 metric tons) (Stephens 2005).

^b Angular boulders may be optional on slopes of 25 to 33 percent.

^c Soil amendment density: 1 cubic yard = 1 ton.

^d Does not include retaining walls for Material Disposal Area C.

Note: To convert cubic yards to cubic meters, multiply by 0.7646; tons to metric tons, multiply by 0.907; square feet to square meters, multiply by 0.0929.

Source: Stephens 2005.

Because of the proximity of buildings and buried pipes, retaining walls may be installed at MDA C to terminate the cover edge. Retaining walls would range in length from 1,000 to 1,400 feet (305 to 427 meters) for the 3-foot (0.9-meter) and 8.2-foot (2.5-meter) covers, respectively. The Stephens report estimates material quantities in terms of linear feet for a reinforced concrete option or square feet for a dry-stack rock option. Material quantities are listed in **Table I–44**, along with the average and maximum heights of the retaining walls corresponding to the optional 3- and 8.2-foot (0.9- and 2.5-meter) cover thicknesses (Stephens 2005).

Table I-44 Summary of Material Disposal Area C Retaining Wall Quantities

| Material Disposal Area C Cover | Retaining Wall Dimensions | | | Surface Area (square feet) |
|--------------------------------|---------------------------|---------------|---------|----------------------------|
| | Length (feet) | Height (feet) | | |
| | | Average | Maximum | |
| 3-foot | 1,001 | 4.6 | 11 | 4,571 |
| 8.2-foot | 1,412 | 8.7 | 16 | 12,333 |

Note: To convert feet to meters, multiply by 0.3048; square feet to square meters, multiply by 0.0929.

Source: Stephens 2005.

A dry-rock retraining wall was assumed for this appendix. It is a mortarless wall using stacked rocks (or prefabricated reinforced concrete elements, usually L-shaped to enable interlocking successive layers) sloped against the horizontal force of backfill and provided with drain holes to avoid hydrostatic pressure. The depth of a concrete reinforced block often ranges from 1 to 1.5 feet (0.3 to 0.5 meters), depending on variables such as the height of the wall. Assuming 1.5-foot (0.5-meter) blocks, the total wall mass would be 184 pounds per square foot (900 kilograms per square meter) (DCA 2005). This information yields an estimate of about 420 tons (381 metric tons) of concrete reinforced block for the 4-foot (1.2-meter) cover and 1,135 tons (1,030 metric tons) of concrete reinforced block for the 8.2-foot (2.5-meter) cover. Assuming use of 22-ton (20-metric-ton) trucks, this implies (including a 10 percent contingency) 21 to 57 rock retaining wall shipments (one way).

For the remaining MDAs, cover materials were estimated on a nominal cover acreage, an assumed minimum thickness of added tuff of 3.0 feet (0.9 meters), and an assumed maximum thickness of added tuff of 8.2 feet (2.5 meters). Additional cover materials (topsoil, rock, soil amendment, gravel, etc.) were assumed, representing a 10 percent increase in in-place material volume. In addition, subgrade fill would be provided for the MDAs in quantities amounting to about 20 percent of the in-place tuff volume. For cover acreage, LANL expects that MDAs A and T would be capped as a single unit because only 120 feet (37 meters) separate them. LANL indicates that the cap for MDA A would extend 100 feet (30 meters) beyond the limits of the fence surrounding MDA A, thus covering 2.7 acres (1.1 hectares). The cap for MDA T would extend 100 feet (30 meters) beyond the limits of the fence surrounding the MDA, thus covering 6.2 acres (2.5 hectares) (LANL 2006a). The northern edge of the MDA T cap may require riprap (covering about 0.75 acre [0.3 hectare]) to control surface water runoff without erosion (LANL 2006a). For the remaining MDAs, cover acreages assumed for the *Borrow Source Survey* (Stephens 2005) are also assumed here. Material requirements are listed in **Table I-45**.

Current NNSA plans call for complete removal of the waste in MDA B (Section I.3.3.2.7); consequently, the volumes provided in Table I-45 for MDA B are conservative estimates based on assumed capping of all waste and contamination in MDA B. Also, because NMED has determined that the Consent Order requirements have been satisfied for the SWMUs comprising MDA U (NMED 2006b), capping may be unnecessary.

Table I-46 presents the assumed numbers of one-way shipments that would be required for delivery of these materials, assuming that each truck contains 22 tons (20 metric tons) of material and a 20 percent swell factor (Stephens 2005). A 10 percent contingency factor was assumed.

Table I–45 Cover Materials for Selected Material Disposal Areas (cubic yards)

| Material Disposal Area | Cover Area | | Minimum Cover Thickness (3 feet of tuff) | | | Maximum Cover Thickness (8.2 feet of tuff) | | |
|------------------------|------------|-------------|---|---------------------|--------|---|---------------------|---------|
| | Acres | Square Feet | Tuff | Additional Material | Total | Tuff | Additional Material | Total |
| A | 2.7 | 120,000 | 16,000 | 1,300 | 17,000 | 43,000 | 3,600 | 46,000 |
| B ^a | 6.0 | 260,000 | 35,000 | 2,900 | 38,000 | 95,000 | 7,900 | 100,000 |
| T ^b | 6.2 | 270,000 | 36,000 | 3,000 | 39,000 | 98,000 | 8,200 | 110,000 |
| U ^c | 0.2 | 8,700 | 1,200 | 97 | 1,300 | 3,200 | 260 | 3,400 |
| AB | 1.4 | 61,000 | 8,100 | 680 | 8,800 | 22,000 | 1,900 | 24,000 |

^a Estimates for MDA B are based on the assumption that all waste and contamination at MDA B would be capped. Current plans call for complete removal of waste from MDA B. The Capping Option is retained for MDA B for completeness.

^b Does not include 0.75 acres of riprap comprising 1,210 cubic yards, assuming a thickness of 1 foot.

^c Estimates for capping MDA U are conservative because NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b).

Note: To convert acres to hectares, multiply by 0.4047; square feet to square meters, multiply by 0.092903; cubic yards to cubic meters, multiply by 0.7646. Because numbers have been rounded, the sums may not equal the indicated totals.

Table I–46 One-Way Shipments for Delivery of Cover Materials for Selected Material Disposal Areas

| Technical Area | Material Disposal Area | Minimum Cover Thickness (3 feet of tuff) | | | Maximum Cover Thickness (8.2 feet of tuff) | | |
|----------------|------------------------|---|---------------------|-------|---|---------------------|-------|
| | | Tuff | Additional Material | Total | Tuff | Additional Material | Total |
| 21 | A | 1,200 | 100 | 1,300 | 3,300 | 280 | 3,600 |
| 21 | B ^a | 2,700 | 230 | 2,900 | 7,400 | 620 | 8,000 |
| 21 | T ^b | 2,800 | 230 | 3,000 | 7,700 | 640 | 8,300 |
| 21 | U ^c | 91 | 8 | 98 | 250 | 21 | 270 |
| 49 | AB (Areas 1-4) | 630 | 53 | 690 | 1,700 | 140 | 1,900 |

^a Estimates for MDA B are based on the assumption that all waste and contamination at MDA B would be capped. Current plans call for complete removal of waste from MDA B. The Capping Option is retained for MDA B for completeness.

^b Delivery of riprap for MDA T would entail an additional 72 shipments.

^c Estimates for capping requirements for MDA U are conservative because NMED has issued a Corrective Action Complete with Controls certification for SWMUs comprising MDA U (NMED 2006b).

Note: Because numbers have been rounded, the sums may not equal the indicated totals.

Small MDAs and landfills. Remediation may be required at several small MDAs and landfills.⁵⁰ Assuming that these MDAs are capped in place, the assumed coverage areas of the MDA caps, and capping thicknesses, are listed in **Table I–47**. Cover materials were estimated based on a nominal cover acreage, an assumed minimum thickness of added tuff of 3 feet (0.9 meters), and an assumed maximum thickness of added tuff of 8.2 feet (2.5 meters). Additional cover materials (topsoil, rock, soil amendment, gravel) were assumed, representing an increase in in-place material volume of 10 percent. In addition, subgrade fill was assumed to be provided for the MDAs in quantities amounting to about 20 percent of the in-place tuff volume. For material shipments, each truck was assumed to contain 22 tons (20 metric tons) of material with a 20 percent swell factor. A 10 percent contingency was assumed (**Table I–48**).

⁵⁰ Some MDAs are not addressed in this section. MDA M has been remediated and has been recommended for no further action. MDA S is an active 100-square-foot (9.3-square-meter) test plot. MDA W is administratively complete. MDA X has been remediated and recommended for no further action. MDA K has been largely remediated, although two small aboveground disposal areas remain. Capping is not a reasonable option for these disposal areas.

Table I-47 Cover Assumptions for Remaining Material Disposal Areas (cubic yards)

| Technical Area – Material Disposal Area | Assumed Cover Area | | Minimum Cover Thickness (3 feet of tuff) | | | Maximum Cover Thickness (8.2 feet of tuff) | | |
|---|--------------------|-------------|--|---------------------|--------|--|---------------------|--------|
| | Acres | Square Feet | Tuff | Additional Material | Total | Tuff | Additional Material | Total |
| 06 - F | 1.4 | 61,000 | 8,100 | 680 | 8,800 | 22,000 | 1,900 | 24,000 |
| 08 - Q | 0.2 ^a | 8,700 | 1,200 | 97 | 1,300 | 3,200 | 260 | 3,400 |
| 15 - N | 0.92 ^b | 40,000 | 5,400 | 450 | 5,800 | 15,000 | 1,200 | 16,000 |
| 15 - Z | 0.23 ^c | 10,000 | 1,300 | 110 | 1,400 | 3,600 | 300 | 3,900 |
| 16 - R | 2.3 ^d | 99,000 | 13,000 | 1,100 | 14,000 | 36,000 | 3,000 | 39,000 |
| 33 - D | 0.11 ^e | 4,800 | 640 | 53 | 690 | 1,700 | 150 | 1,900 |
| 33 - E | 0.7 ^f | 30,000 | 4,100 | 340 | 4,400 | 11,000 | 930 | 12,000 |
| 36 - AA | 0.4 ^g | 17,000 | 2,300 | 190 | 2,500 | 6,300 | 530 | 6,800 |
| 39 - Y | 0.66 ^h | 29,000 | 3,900 | 320 | 4,200 | 11,000 | 880 | 11,000 |

^a Dimensions uncertain, estimated (LANL 1999b). The Capping Option for this MDA may be unlikely.

^b Assumed a pit, 40,176 square feet.

^c Dimensions uncertain. Assumed 10,000 square feet, with some existing material removed.

^d Dimensions uncertain. Assumed 2.27 acres (LANL 2005c). The Capping Option for this MDA may be unlikely.

^e Assumed cap is 2,400 square feet to account for depth of chambers.

^f Assumed one large cap over four pits, a test chamber, and a shaft. Site comprises 0.7 acres.

^g Assumed two separate trenches, with cap extending to 12 feet around sides of both trenches (i.e., footprint for one trench is 6,656 square feet; footprint for second trench is 10,056 square feet).

^h Assumed one cap covers northern two trenches, and a second cap covers southern trench. Assumed cap extends 12 feet around all sides of both trench groups (i.e., northern footprint is 17,888 square feet; southern footprint is 11,008 square feet). Does not include any rock armor or other measures to preclude erosion from nearby ephemeral stream.

Note: To convert cubic yards to cubic meters, multiply by 0.7646; acres to hectares, multiply by 0.405; square feet to square meters, multiply by 0.0929. Because numbers have been rounded, the sums may not equal the indicated totals.

Table I-48 One-Way Shipments of Cover Materials for Remaining Material Disposal Areas

| Technical Area – Material Disposal Area | Minimum Cover Thickness (3 feet of tuff) | | | Maximum Cover Thickness (8.2 feet of tuff) | | |
|---|--|---------------------|-------|--|---------------------|-------|
| | Tuff | Additional Material | Total | Tuff | Additional Material | Total |
| 06 - F | 630 | 53 | 690 | 1,700 | 140 | 1,900 |
| 08 - Q ^a | 91 | 8 | 98 | 250 | 21 | 270 |
| 15 - N | 420 | 35 | 450 | 1,100 | 95 | 1,200 |
| 15 - Z | 100 | 9 | 110 | 280 | 24 | 310 |
| 16 - R ^a | 1,000 | 86 | 1,100 | 2,800 | 230 | 3,000 |
| 33 - D | 50 | 4 | 54 | 140 | 11 | 150 |
| 33 - E | 320 | 26 | 340 | 870 | 72 | 940 |
| 36 - AA | 180 | 15 | 200 | 490 | 41 | 530 |
| 39 - Y | 300 | 25 | 330 | 820 | 68 | 890 |

^a The Capping Option for these material disposal areas may be unlikely.

Note: Because numbers have been rounded, the sums may not equal the indicated totals.

Capping these MDAs may result in generation of waste. Projected waste generation rates for these MDAs are listed in **Table I-49**. Most wastes were from MDAs R and Z. Both MDAs contain debris that is piled above grade, as well as buried debris. It was assumed that the aboveground debris from both MDAs would be removed before capping. This removal waste volume was assumed to be half of the total volume of debris estimated for these MDAs (see Section I.3.3.2.4.3).

In addition to MDAs, other landfills or contaminated areas may require capping. These include the landfill at Area 6 at TA-49 and contaminated soils in Area 12 at TA-49. Capping of the Airport Landfill was completed in 2007 and the landfill remedy completion report was submitted to and approved by NMED (LANL 2006a). Remediation decisions about Areas 6 and 12 of TA-49 have not yet been made.

Table I-49 Waste Generation through Fiscal Year 2016 from Capping Additional Material Disposal Areas

| | <i>Solid Waste</i> | <i>Chemical Waste</i> | <i>Low-Level Radioactive Waste</i> | <i>Mixed Low-Level Radioactive Waste</i> | <i>Total</i> |
|---------------------------------------|--------------------|-----------------------|------------------------------------|--|--------------|
| Volumes ^a (cubic yards) | 14,000 | 4,400 | 1,500 | 190 | 20,000 |

^a In situ volumes. Because much material will be soil and debris, which will “swell” upon removal, and because of packaging inefficiencies, as-shipped volumes will be somewhat larger than in situ volumes.

Note: To convert cubic yards to cubic meters, multiply by 0.76456. Because numbers have been rounded, the sums may not equal the indicated totals.

Cover materials estimated for the two TA-49 contaminated areas are summarized in **Tables I-50** and **I-51**.

Table I-50 Cover Assumptions for Technical Area 49 Contaminated Areas (cubic yards)

| <i>Landfills and Areas</i> | <i>Assumed Cover Area</i> | | <i>Minimum Cover Thickness (3 feet of Tuff)</i> | | | <i>Maximum Cover Thickness (8.2 feet of Tuff)</i> | | |
|-----------------------------|---------------------------|---------------------------------|---|----------------------------|--------------|---|----------------------------|--------------|
| | <i>Acres</i> | <i>Square Feet ^a</i> | <i>Tuff</i> | <i>Additional Material</i> | <i>Total</i> | <i>Tuff</i> | <i>Additional Material</i> | <i>Total</i> |
| Area 6, TA-49 ^a | 5 | 218,000 | 29,000 | 2,400 | 31,000 | 79,000 | 6,600 | 86,000 |
| Area 12, TA-49 ^a | 0.3 | 13,000 | 1,700 | 150 | 1,900 | 4,800 | 400 | 5,200 |

TA = technical area.

^a Cover area estimated (Stephens 2005).

Note: To convert cubic yards to cubic meters, multiply by 0.7646; acres to hectares, multiply by 0.405; square feet to square meters, multiply by 0.0929. Because numbers have been rounded, the sums may not equal the indicated totals.

Table I-51 One-Way Shipments for Technical Area 49 Contaminated Areas

| <i>Landfills and Areas</i> | <i>Minimum Cover Thickness (3 feet of Tuff)</i> | | | <i>Maximum Cover Thickness (8.2 feet of Tuff)</i> | | |
|-----------------------------|---|----------------------------|--------------|---|-------------|--------------|
| | <i>Tuff</i> | <i>Additional Material</i> | <i>Total</i> | <i>Additional Material</i> | <i>Tuff</i> | <i>Total</i> |
| Area 6, TA-49 ^a | 2,300 | 190 | 2,500 | 6,200 | 520 | 6,700 |
| Area 12, TA-49 ^a | 140 | 11 | 150 | 370 | 31 | 400 |

TA = technical area.

^a Cover area estimated (Stephens 2005).

Note: Because numbers have been rounded, the sums may not equal the indicated totals.

MDA H. Remediation of MDA H has been addressed in corrective measure investigations and evaluations, as well as NEPA analyses (DOE 2004b). The remedy selected by NMED is encapsulation of shafts, installation of an engineered evapotranspiration cover, and installation of a soil vapor extraction system (see Section I.3.3.2.2.4) (NMED 2007a). The final evapotranspiration cover for MDA H (DOE 2004b) would require 2,185 cubic meters (2,860 cubic yards) of bulk materials obtained from onsite or local sources. Assuming a gross material density of 1.3 tons per cubic yard, 22-ton trucks, and 20 percent material swell, transporting 2,860 cubic yards of bulk materials over an estimated period of 5 months would require roughly 200 one-way shipments. Shipments of encapsulation material (grout or micro-concrete) and equipment would also be required. Assuming that remediation occurs during the time period covered in this SWEIS, bulk material volumes and shipments projected in this section could be augmented by those summarized above.

I.3.3.2.2.3 Hydraulic Barriers

An option for some MDAs may be to install hydraulic barriers to restrict lateral movement of moisture and contamination. The design and installation of hydraulic barriers at any MDA would be integrated with the design for its final configuration and would be based on a site-specific analysis that considered the environmental processes affecting the MDA, including surface and subsurface water dynamics. Two example installations are described below.

Using MDA A as an example, a hydraulic barrier could nominally be a high-density polyethylene (HDPE) sheet installed in a slit trench and backfilled with bentonite slurry. The barrier would extend along the north and east sides of the final cap, or about 800 feet (244 meters). The depth of the barrier would range from 20 to 30 feet (6.1 to 9.1 meters), assuming that the barrier is seated 5 feet (1.5 meters) into the bedrock. The average depth may be closer to 20 feet (6.1 meters), because a paleochannel at the west side of the cap forms the deeper limit and has limited lateral extent (LANL 2006a).

Sheet pile cutoff walls are installed by driving interlocking steel or HDPE sheets into the ground. The joints between individual sheets are typically plugged using clay slurry (steel sheets) or an expanding gasket (HDPE sheets). The steel sheets can be driven directly into the ground; the HDPE sheets are driven using a steel backing that is removed once the sheet is in place. Slurry walls can be constructed using a trench backfilled with a slurry mixture of bentonite and native materials, or a vibrating beam, where a steel plate is forced into the ground, and, as the plate is removed, bentonite is injected to fill the space of the beam. A typical slurry wall installed by trenching is 1.5 to 6.5 feet (0.5 to 2 meters) wide. It can be installed to 50-foot (15-meter) depths. Slurry walls using the vibrating beam method are narrower and typically installed at shallower depths (NFESC 2005).

An HDPE barrier installed by trenching may be conservative in terms of materials. An 800-foot (240-meter) wall would require 20,000 square feet (1,900 square meters) of HDPE, assuming an average depth of 25 feet (7.6 meters). Assuming a trench width of 3.3 feet (1 meter), 2,430 cubic yards (1,860 cubic meters) of bentonite and native materials would be needed.

Using MDA T as an example, a hydraulic barrier could again nominally be sheet HDPE installed in a slit trench and backfilled with bentonite slurry. The barrier would extend along the north

and west sides of the cap, or 1,150 feet (350 meters). The depth of the barrier would range from 20 to 30 feet (6.1 to 9.1 meters), assuming the barrier is seated 5 feet (1.5 meters) into the bedrock. The average depth may be closer to the 20-foot (6.1-meter) depth, because a paleochannel at the west side of the cap forms the deeper limit and has limited lateral extent (LANL 2006a).

Assuming a length of 1,150 feet (350 meters) and an average depth of 25 feet (7.6 meters), about 28,750 square feet (2,670 square meters) of HDPE sheeting would be required, plus 3,500 cubic yards (2,700 cubic meters) of bentonite and native materials, assuming a trench width of 3.3 feet (1 meter).

I.3.3.2.2.4 Soil Vapor Extraction Systems

Soil vapor extraction systems are contemplated for several MDAs. The investigation work plans to be implemented for these MDAs are intended, in part, to determine the extent of volatile organic compound plumes detected beneath the MDAs (see LANL 2003k, 2003m, 2004c). Alternatives for addressing the plumes will be developed based on these investigations.

An often-used technology for removing soil vapors is an active soil vapor extraction system. A mechanical blower applies a vacuum to a well screened in the vadose zone, causing vapor surrounding the open interval of the well to be drawn to the surface. An active system was constructed and tested near the outer boundary of the volatile organic compound plume under MDA L. Two boreholes were constructed to depths of 215 feet (66 meters) in the immediate vicinity of two source zones. Volatile organic compounds removed from the plume were treated using granular activated carbon to absorb the chemical contaminants. The results from the pilot study will be used to evaluate the potential of soil vapor extraction systems for remediating the MDA L plume and to assess system design criteria. The results of the study will be considered as part of the corrective measure evaluation for the MDA (LANL 2005f, 2006d).

Active soil vapor extraction systems reach a point of limited contaminant flow where the cost per mass of contaminant removed, including operator attention, system maintenance, and a power source, is increased (LANL 1999e). Passive vapor extraction systems become useful as a polishing effort after active systems (or other methods) have reduced existing concentrations, or for situations where the existing concentrations in soil are too low for effective removal using active systems.

Passive soil vapor extraction, also known as barometric pumping, uses differences between atmospheric pressure and subsurface pressures to move contaminants from the vadose zone to the soil surface. Passive soil vapor extraction wells function like active air injection or extraction wells but do not use mechanical pumps. At any time, the atmospheric pressure at the surface and the soil gas pressure in the subsurface are different. If these two zones are connected by a vadose zone well, the pressure differential results in flow either into or out of the well. When atmospheric pressure is higher than subsurface pressure, air flows through wells into the subsurface. But when atmospheric pressure is lower than subsurface pressure, air flows out of the wells into the atmosphere, taking the volatile organic compounds in the gas phase (Initiatives 2001).

The system functions through a series of extraction wells set into the polluted area. Removal efficiency is improved through placement of one-way valves at the tops of the wells, allowing flow only out of the wells. Valves are small and inexpensive. A Baroball[®] valve is a small housing containing a ping-pong ball in a conical seat, permitting gas flow in one direction and needing minimal pressure (1 millibar) to lift the ball from the seat. Volatile organic compounds flowing out of the well can be captured and treated, commonly by passing the gases through a passive carbon absorption system. Incineration, catalytic oxidation, or condensation may be used depending on the contaminant (Initiatives 2001). Passive soil vapor extraction systems have been used at Hanford (Initiatives 2001) and Savannah River (WSRC 1997, 2000).

Whether active or passive, soil vapor extraction systems are unobtrusive. Although active systems require a source of power, the equipment is portable. Passive systems project only a small distance above the ground. Either system could probably be installed and used without interrupting procedures for final site cover.

I.3.3.2.2.5 Grouting the General's Tanks in Material Disposal Area A

Once used to store solutions containing plutonium, the two 50,000-gallon (189,000-liter) tanks in MDA A contain sludge containing transuranic isotopes (LANL 1991). One option is to solidify some or all of the sludge in place, using a system that achieves a final waste form that is reasonably homogenous. A jet grout system is assumed as a typical decontamination and solidification process. It can wash the interiors of tanks, mix tank contents before removing samples or introducing grout or other stabilization agents, or remove sludge from the tanks. It has been applied to a tank in LANL's TA-50 and to tanks at Oak Ridge National Laboratory. It can be used in tanks having interior obstructions (DOE 1999d).

Pipes are extended from a charge vessel into the sludge and supernatant covering the bottom of a tank. Existing pipes may be used or ones that are inserted. Water is added to the tanks, as needed, as well as chemicals (such as acids) to dissolve the sludge and remove material adhering to surfaces. A jet pump draws a vacuum into a charge vessel, sucking material into the charge vessel. When the mixture reaches a predetermined level in the charge vessel, the jet pump is switched from vacuum to pressure mode. The fluid is forced from the charge vessel into the tank, mixing the contents. The system may be vented to depressurize the charge vessel. The process is repeated until the sludge and supernatant are mixed. Then samples of the mixture can be obtained or grout introduced and mixed with the sludge and supernatant to provide a final solidified waste form. Otherwise, the mixture can be withdrawn, treated, and solidified. Secondary waste streams from jet mixer operations would include small volumes of personal protective equipment, contaminated equipment and hardware, plastic sheeting and containers, and structured steel support and platforms. Decontamination and reuse of some equipment may be possible (DOE 1999d).

Operational Elements. Operational elements for tank grouting include:

- Design, planning, permitting, and developing authorization documents and work orders and providing notifications to regulators or others as needed.
- Training of personnel, as needed.

- Demolishing or relocating existing fences or structures, as needed.
- Identifying utilities such as gas lines, as needed to maintain safety, and, as needed, providing additional utilities (for example, water or electricity).
- Mobilizing equipment.
- Performing preliminary characterization and analyses, including an initial criticality review.
- Preparing the site, including any needed excavations to provide access to the tanks, and installing safety and environmental detection equipment.
- Performing initial entry into the tanks and sampling and stabilizing the atmosphere within the tanks.
- Fabricating and installing equipment into the tanks for mixing, sampling, waste removal, and grouting.
- Sampling and analyzing tank contents and developing grout mix formulations from bench scale testing.
- Stabilizing the tank contents (mixing, grouting, removing, and solidifying material, as needed).
- Managing the small quantities of liquid or solid wastes generated from operations.
- Decontamination of equipment, as needed, and demobilization.
- Final stabilization of the site (for example, backfilling excavations and installing a final cover).

Equipment to be mobilized largely already exists at LANL. The major modules of the system are (AEAT 2004):

- Charge vessel skid (contains the charge vessel, de-mister, jet pumps, piping, and main process valves).
- Control hut (contains a valve rack and the system control panel).
- In-tank charge vessel with wash nozzle module and hydraulic power pack.
- Offgas skid (used to achieve a slight negative pressure on the system, it contains air treatment capacity such as high-efficiency particulate air [HEPA] filters).

After any initial excavation needed to access the tanks, and installation of platforms or scaffolding needed to support equipment, initial operations will focus on accessing the tanks at up to three locations in each tank. All activities will be in accordance with approved documented safety analyses. Because the tanks have been sealed for many years, hydrogen or other gases may have built up within the tanks. The atmosphere within the tanks must be stabilized; depending

on the results of sampling and as authorized, the gas may be vented or treated. Following tank atmosphere stabilization, sludge samples will be obtained and analyzed for radioactive and chemical materials. If the sample results indicate RCRA constituents of concern, NMED would be notified and an appropriate path forward negotiated. Next, mixing, sampling, and benchscale testing of grout mixtures will be performed. The grout mixture may contain additives such as fly ash or bentonite. A hot-cell facility may be needed for sampling analysis. Once a final grout mixture is developed, and after any needed additional fabrication or modification of equipment, final stabilization of the tanks will take place consistent with established plans, authorizations, and all safety and environmental reviews and analyses.

Final stabilization of the tank may involve solidification of all material in place or may involve removal of some material and solidifying the remaining material in place.

Assuming that the radioactive material would be all solidified in place, a small concrete batch plant could be installed convenient to the MDA and grout produced as needed. Following these and other preliminary activities, the system would be initially operated to mix the sludge and the supernatant, and then grout would be introduced in a manner achieving a mixture of sludge and grout within the tanks. One approach would be to first mix and solidify the sludge (heel), and then use clean grout to fill the remaining void. The process for each tank could require about 250 cubic yards (190 cubic meters) of grout per tank.

Assuming that the jet grout system is first used to remove most of the sludge from the tank before stabilization, the removed sludge would be treated and solidified. Experience at three 50,000-gallon (189,000-liter) tanks at Oak Ridge National Laboratory demonstrated a removal efficiency ranging from 96 to 98 percent. The ratio of liquid to sludge volume in the material removed from each tank ranged from 2.4 to 9 (DOE 1999d).

The volume of sludge remaining in the General's Tanks is uncertain. Because most of the liquid was removed from the tank, there may be little remaining supernatant. The General's Tanks Characterization Activities Documented Safety Analysis estimates a sludge volume of 3.22 cubic yards (2.46 cubic meters) (LANL 2003j). Assuming that roughly 6 times as much liquid would be added as the original sludge volume, about 22.5 cubic yards (17.2 cubic meters) of mixture would be generated from each tank.⁵¹ Assuming 95 percent removal efficiency, the mixture from the west tank would contain about 45.65 curies of alpha-emitting transuranic isotopes, while the east tank would contain about 11.6 curies. Assuming these mixtures at an increase in volume of about 50 percent results in a final waste volume of about 34 cubic yards (26 cubic meters) from each tank.

It is expected that waste solidification could take place using a mobile waste treatment system temporarily located at the site. Alternatively, existing LANL waste treatment and solidification capacity may be used, depending on the characteristics of the removed sludge. Removed mixture would be pumped from the system charge vessel into containers for safe transfer to the treatment facility.

⁵¹ A document prepared by AEA Technology indicates that optimum mixing is achieved with a supernatant-to-sludge ratio of about 2 to 1 (AEAT 2004). A 6 to 1 ratio was assumed based on experience at Oak Ridge (DOE 1999d) and because the sludge has been left in place for several years.

Waste from either tank was assumed to be transuranic waste. Assuming use of 55-gallon (208-liter) drums at a 90 percent packing efficiency and 20 percent contingency, the solidified mixture would require about 8 one-way shipments to WIPP, assuming the waste can be contact handled.⁵²

The heel left in the tanks after removal would be solidified as discussed above. About the same volume of grout would be required as before.

I.3.3.2.2.6 Schedules

Schedules for capping MDA G and MDA L are provided in Sections I.3.3.2.1.2.4 and I.3.3.2.1.3, respectively. For MDAs A, B, C, T, U, and AB, it was assumed that work periods for stabilization and capping schedules are completed by the schedules for submittals of their respective remedy completion reports. The assumed start and completion dates, and work periods, are listed in **Table I-52**.

Work periods for MDAs A, B, C, T, U, and AB were assumed by extrapolating from published estimates for MDAs G, L, and H (LANL 2005k, DOE 2004b). Work periods would depend on the volumes of capping materials emplaced, operational difficulties and constraints (such as existing nearby structures), economies of scale, funding, and other considerations. For simplicity, a thicker cap was assumed to require the same installation time as a thinner cap.

Stabilization and capping the remaining small MDAs (F, Q, N, Z, R, D, E, AA, and Y) and additional landfills may be carried out, if needed. Consistent with Consent Order schedules, remediation is assumed to start in FY 2007 and continue through FY 2016.

Table I-52 Temporal Assumptions for Capping Large Material Disposal Areas

| <i>Material Disposal Area</i> | <i>Assumed Start of Stabilization and Capping</i> | <i>Assumed Completion of Stabilization and Capping</i> | <i>Assumed Work Time (months)</i> |
|-------------------------------|---|--|-----------------------------------|
| A | 1/11/2010 | 3/11/2011 | 14 |
| B ^a | 2/23/2010 | 6/23/2011 | 16 |
| T | 6/19/2009 | 12/19/2010 | 18 |
| U ^b | 5/6/2011 | 11/6/2011 | 6 |
| AB | 6/1/2014 | 1/31/2015 | 8 |
| C | 11/5/2008 | 9/5/2010 | 22 |
| G | 10/1/2010 | 12/28/2015 | 40 |
| L | 4/30/2010 | 6/30/2011 ^c | 14 |

^a Current plans call for complete removal of waste from MDA B. In January 2007, NMED approved the revised Investigation and Remediation Work Plan for MDA B that addresses removal (NMED 2007b). The Capping Option is retained in this Appendix for completeness.

^b The Capping Option for MDA U is conservatively retained for completeness. NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b).

^c The current schedule for MDA L remediation calls for submittal of a remedy completion report by July 9, 2011.

⁵² This waste was conservatively included for the Capping Option.

I.3.3.2.3 Sources of Bulk Materials for Stabilizing Material Disposal Areas

Materials required for placing a final cover of the MDAs could include fill material such as crushed tuff, gravel, cobbles and angular boulders, concrete reinforced block or similar dry-stack rock, sand, clay, top soil or rooting media, soil amendment, or compost. Additional bulk materials for stabilizing the MDAs may include barrier wall material such as HDPE sheets and bentonite or similar material. Grout would be needed to stabilize the General's Tanks.

To minimize costs and environmental impacts, bulk materials should be acquired close to the point of use. The *MDA Core Document* (LANL 1999b) and Stephens report (Stephens 2005) documented several sources within and local to LANL for bulk materials such as rocks, clay, or soil amendment. Information from the U.S. Geological Survey and the State of New Mexico confirms the extensive production of nonfuel minerals in New Mexico. The state was a significant producer of construction sand and gravel and dimension stone (USGS 2003). A 2001 reference lists roughly 300 mines, mills, and quarries in New Mexico (Pfeil et al. 2001). Production of masonry cement in 1996 was roughly 100,000 tons (WERC 2002).

The capping material needed in largest quantity is crushed tuff or other fill. The Borrow Source Survey (Stephens 2005) pointed out the potential for stockpiling fill and other material from construction projects, and that two sediment retention and flood control structures built at LANL following the 2000 Cerro Grande Fire could be removed by 2010 as watersheds become revegetated. These structures may provide a source of material for cover construction, perhaps up to 50,000 cubic yards (38,250 cubic meters) (Stephens 2005). But the most significant onsite source would be the existing LANL borrow pit in TA-61.

TA-61 Borrow Pit. Also known as the East Jemez Site, TA-61 is a long, narrow, and relatively small site created from a portion of TA-3 when LANL redefined its TAs in 1989 (LANL 1999d). It contains physical support and infrastructure facilities. In addition to the borrow pit next to East Jemez Road and east of the Royal Crest Manufactured Home Community, TA-61 contains the county landfill, which, when closed, would be the site of a solid waste transfer station.

TA-61 is bordered by TA-43, TA-41, and TA-02 to the north, TA-53 to the east, TA-60 to the south, and TA-3 to the east. Access to TA-61 is via East Jemez Road, a high-traffic publicly used two-lane thoroughfare traversing TA-61 lengthwise in an east-west orientation.⁵³

The setting of TA-61 within LANL, and its topography, can be visualized in **Figure I-21**, which shows major physiographic features, the surrounding TAs, and the conceptual geologic model of Operable Unit 1114 (LANL 1993e). The ground slopes upward from east to west. TA-61 is bounded on the north by Los Alamos Canyon and on the south by Sandia Canyon, which is about 400 feet (120 meters) wide and 40 to 140 feet (12 to 43 meters) deep at TA-61 (LANL 1999d). The distance to the regional aquifer is 1,300 feet (396 meters) (LANL 2005a).

⁵³ *The entrance to the borrow pit is near a steep hill, and there is little room for an acceleration lane (LANL 2003j).*

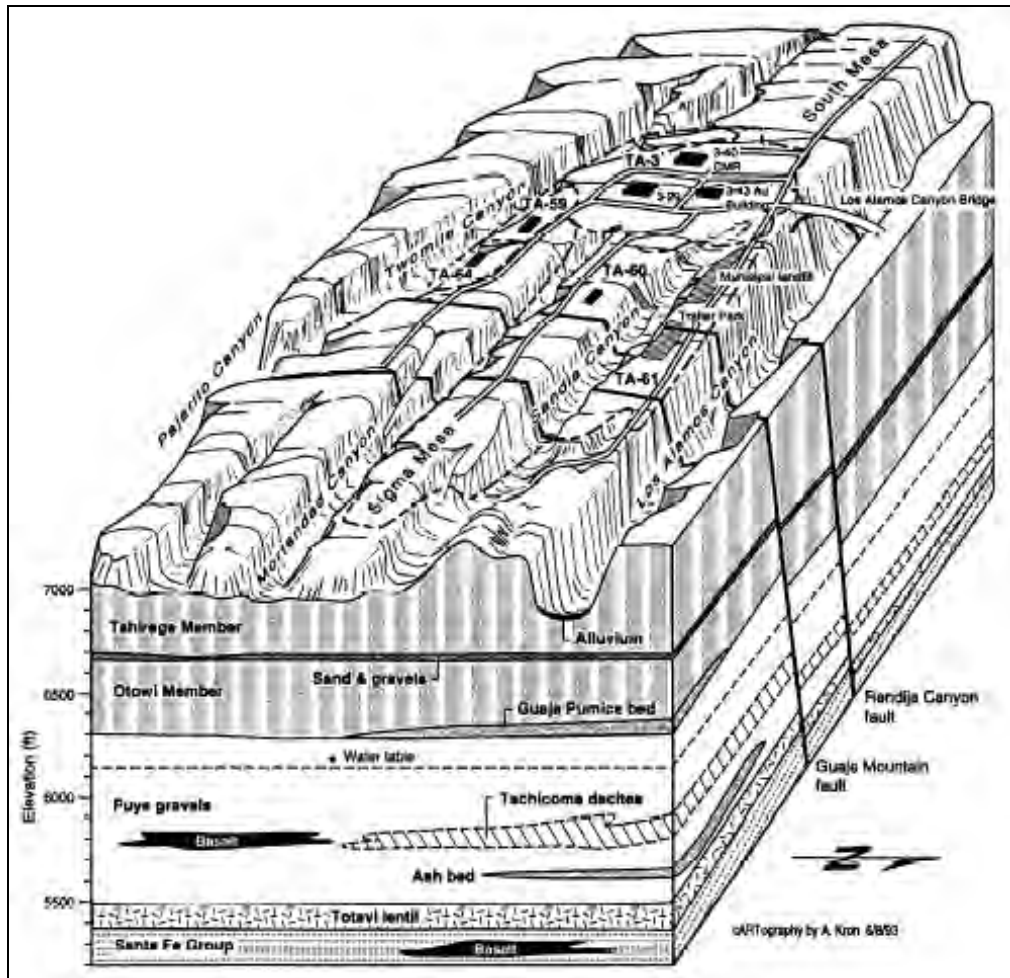


Figure I-21 Conceptual Geologic Model of Operable Unit 1114

Used for soil and rubble storage and pickup, the borrow pit is within a 43-acre (17-hectare) site (LANL 2003a). It is on the south side of East Jemez Road across from its intersection with La Mesita Road, which provides access to the Los Alamos Neutron Science Center (LANSCE). The borrow pit is 2 miles (3.2 kilometers) from the county landfill, a few thousand feet to the east of the trailer park, and across Sandia Canyon from TA-60, Sigma Mesa. A natural gas line is to the west (LANL 2004b, 2005a).

Figure I-22 is an aerial photograph of the triangular-shaped clearing in the forest that comprises the borrow pit (LANL 2003a). **Figure I-22** shows the jog in the stream in Sandia Canyon that occurs at the borrow site.⁵⁴ **Figure I-23** is a view from within the pit looking to the east (LANL 2003a). The knoll to the left (north) in the figure shields the pit from visibility from East Jemez Road.

⁵⁴ This suggests that if the borrow pit is expanded to the southwest, measures would have to be taken to ensure that drainage does not cause surface water quality problems

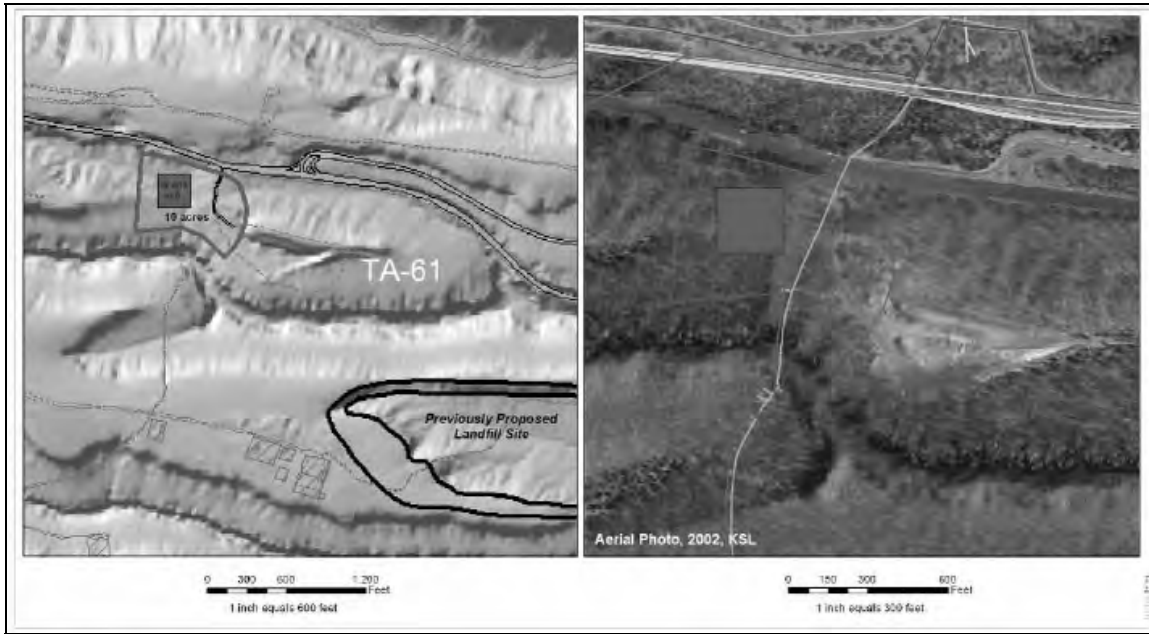


Figure I-22 Aerial Illustrations of Borrow Pit



Figure I-23 View to the East from within the Technical Area 61 Borrow Pit

I.3.3.2.4 Removal Option

Removals are difficult to characterize. Information is still being acquired through corrective measure investigation programs. Simplifying assumptions are made based on studies and experience at LANL and other DOE sites.

I.3.3.2.4.1 Operational Elements

Operational elements associated with removing any of the MDAs are summarized in the text box.

MDA Removal Operational Elements

- *Design, Planning, and Permitting* – Includes planning for site operations, including equipment and personnel coordination. Includes health and safety plans, site security plans, erosion control plans, etc. Includes permits and authorizations.
- *Demolishing/Relocating Existing Operations, Structures, or Materials* – Includes moving, demolishing, or relocating existing structures or operations.
- *Rerouting/Modifying Utilities, Pipelines, or Similar* – Includes rerouting or modifying water, electrical, telephone, or other underground or overhead lines as needed to preclude damage. Includes removal or rerouting of liquid waste or chemical piping to preclude damage.
- *Mobilization* – Includes mobilization and initial site placement of equipment such as cranes, backhoes, dump trucks, water trucks, and graders. Includes installation of a site management trailer. Includes site storage of equipment and initial mobilization of the workforce.
- *Site Preparation* – Includes explorations needed to determine the specific locations of disposed wastes, as well as other site-specific studies and tests. Includes clearing of existing vegetation. Includes the removal of asphalt or other existing covers over disposal units, such as topsoil and the top layer of crushed tuff over the MDAs. Includes removal and disposal of existing security fencing.
- *Perform Special Activities* – Includes activities unique to a specific MDA.
- *Exhumation* – Includes waste exhumation, sorting, characterizing, classifying, packaging as necessary, and shipping for treatment, storage, or disposal.
- *Regrading/Revegetation* – Includes spreading and fine-grading of topsoil, compaction using construction equipment, watering for dust abatement, and watering of planted areas for vegetation germination at approved levels.
- *Demobilization* – Includes demobilization of equipment, including removal of a site management trailer.
- *Health and Safety* – Includes developing a site health and safety plan; performing surface sampling and confirmation of nonhazardous site conditions; monitoring site activities; and conforming to standard construction health and safety policies, laws, and procedures.
- *Project Management* – Includes an onsite project manager or foreman, who reports daily site progress, as well as site office support. Includes specialists such as explosives experts.

Excavation would be preceded by extensive planning and site investigations to confirm the dimensions of the disposal units and the presence of other contamination and buried objects. Other preliminary site work could include permitting; demolishing or relocating existing operations, structures, or materials (as needed); rerouting or modifying utilities or pipelines (as needed); mobilization of equipment; and initial site preparation. Preliminary work may generate wastes requiring treatment and disposal.⁵⁵ It is assumed that a management area would be established near the MDA for heavy equipment and vehicles. A trailer or similar structure would be sited for management of operations. The size of the management area may depend on the size of the MDA and the complexity of removal operations, but, for most MDAs, would probably not exceed a few thousand square feet. An area for parking personal vehicles would be needed; in most cases; existing nearby parking lots or areas nearby the MDA could be used. Utilities would be made available, for example, by hooking up to existing utilities in the vicinity of the MDA. Water may need to be delivered by truck at some MDAs. Portable toilets would be installed in the staging area, and sanitary waste from the toilets would be trucked to a disposal location either on or offsite.

Preliminary work would include development of areas supporting waste removal. The scope and size of support operations would depend on the amount of waste to be removed from the MDAs and the hazards that the waste presents. Support operations could include:

- Capacity for storing and managing exhumed wastes and for decontaminating equipment, as needed
- Capacity for storing bulk materials such as excavation spoils, final cover materials, or demolition debris
- Capacity for preliminary classification of exhumed materials by hazard and staging for further management
- Capacity to process waste as needed for shipment for treatment or disposal
- Capacity to characterize the waste for its organic, inorganic, and radioactive material content

It is expected that this support capacity would be sized to support multiple activities, such as those proposed to support MDA remediation and DD&D at TA-21 (see Section I.3.3.2.7). For large operations, such as that proposed for TA-21, or for removal of large MDAs, support areas could cover several acres. Areas for managing exhumed wastes or stockpiling overburden or other bulk material removed as part of initial preparation would be protected from erosion or runoff, airborne dispersion, and possible cross-contamination. There may be a need to construct temporary roads between the MDAs and the support areas.

Excavation and removal of uncontaminated topsoil or tuff can be performed using conventional equipment such as backhoes and bulldozers. On average, the top 3 feet (0.9 meters) of topsoil and existing cover soil was assumed to be removed from the existing MDA covers and

⁵⁵ *It was assumed that generation of solid waste, chemical waste, and low-level radioactive waste during site preparation would be the same as that for the Capping Option.*

stockpiled at a location as close as reasonably possible considering topography, best management practices, or the proximity of other facilities. The actual volume of the existing cover soil that would be removed will depend on the thickness of cover over each MDA. Maximum, minimum, and average thicknesses can vary considerably within each MDA and over all MDAs. A 3-foot (0.9-meter) thickness for nearly all MDAs was assumed as an average approximation. It represents all the preliminary work at the MDAs that requires movement of soil.

Some removed material may be contaminated. Soil exceeding screening levels would be disposed of as waste. Otherwise, soil meeting screening levels may still be contaminated. Soil not disposed of as waste was assumed to be stockpiled and returned to the excavation along with additional backfill obtained from a local borrow. After backfilling and compaction, topsoil, and related materials would be imported, and the thickness of this final cover would be about 6 inches (15 centimeters).

Only small portions of an MDA would be excavated and backfilled at one time.

Exhumation may take place within an enclosure such as a tension support dome when the waste contains materials that may present a significant inhalation hazard or when removal would be performed within close proximity to operating facilities at LANL or to members of the public. The enclosure would be moved as needed to each successive work area (see Section I.3.3.2.6).

Material would be excavated using heavy equipment. Depending on the hazard presented by the waste, excavation may be possible using conventional equipment such as tracked backhoes, or may require use of specialized equipment such as remotely operated or heavily shielded excavators. Procedures to screen, sort, and classify the removed material would also depend on the hazard presented by the waste. The rates of excavation, sorting, and classification of contaminated materials can vary greatly, depending on the hazard presented by the materials. Materials presenting an external or inhalation hazard would require more time to excavate, sort, and classify. If the material presents an external hazard, then remote operations may be required. If the material presents an inhalation hazard, then use of high-level personal protection equipment may significantly improve work efficiency.

Excavating many of the MDAs considered in this section would generate large quantities of contaminated materials containing hazardous constituents and radionuclides. The materials may present significant handling hazards (for example, external radiation or inhalation concerns) or may otherwise require special consideration because of security concerns. Procedures and equipment may be needed, for example, to contain exhumed compressed gas cylinders or other problematic wastes awaiting sampling and disposal, treatment of gases that cannot be transferred to another container or be transported on highways, hot-tapping of compressed gas cylinders, or excavation or removal of explosives. Remote-operated, shielded facilities may be needed to characterize, treat, and package wastes having high surface radiation levels.

Excavating shafts may be difficult. Removal of the material in shafts could be conducted in many cases using the trenching approach described in Section I.3.3.1.3.2 for MDA H. Many of the shafts in the MDAs have been drilled to roughly similar depths (about 60 feet [18 meters]). In other cases, cranes or specialized equipment may be required.

Volumes of uncontaminated soil removed and temporarily stockpiled during exhumation depend on the method assumed for exhumation, whether all waste is removed or only portions, the depth of excavation, and the configuration of the site.

Once exhumed, waste must be characterized and classified by type. Different types of waste have significantly different requirements for treatment, packaging, and disposal. It was assumed that recovered high explosives would be safely burned at a suitable location within LANL. For other types of radioactive and nonradioactive solid wastes, the total volume of contaminated material excavated from each MDA was estimated, and then the volume was distributed among the different waste types based on available information. It was assumed that the volumes implied by the nominal dimensions of the pits, trenches, and shafts give the total volume of contaminated material.⁵⁶ Backfill placed with the waste when disposed of was conservatively assumed to be contaminated. To assist in waste groupings, radionuclide inventories of the larger MDAs were assessed to provide a sense of radionuclide concentrations and external radiation levels that may be associated with exhumed wastes.

A June 2000 DOE study was used to estimate the volumes of transuranic and alpha-contaminated low-level radioactive wastes that might result from exhuming the MDAs.⁵⁷ This DOE study developed its estimates through surveys of DOE national laboratories. Estimates for LANL MDAs are summarized in **Table I-53** (DOE 1999g, 2000a). Note that “alpha-contaminated low-level radioactive waste” does not represent an official DOE classification of waste. Distinctions among low-level radioactive waste subtypes (such as low-activity radioactive waste, alpha-contaminated low-level radioactive waste, and others) were considered in this appendix to enable enhanced analyses of possible impacts of radioactive waste transportation.⁵⁸

After classification and sorting, waste must be treated and disposed of or stored. Solid and chemical wastes would be sent to authorized treatment facilities or landfills. Low-level radioactive waste that is not mixed could be either disposed of onsite or sent to another site. No onsite disposal capacity now exists for mixed low-level radioactive waste.

⁵⁶ *The as-built dimensions of the pits, shafts, and trenches, often not documented, may be different from the nominal (design) dimensions. The waste volume and potentially contaminated backfill placed in the disposal units would be actually somewhat smaller than that implied by the nominal disposal unit dimensions, because of ramps and sloping walls within pits and trenches. Also, the waste was not placed all the way to the tops of the disposal units. Assuming the disposal unit dimensions, however, accounts for the likelihood of movement of small amounts of contamination laterally and (particularly) vertically downward outside the nominal boundaries of the disposal units after initial waste displacement.*

⁵⁷ *The great bulk of this transuranic-contaminated material was disposed of before operational distinctions between low-level radioactive and transuranic wastes were made at DOE sites.*

⁵⁸ *The estimated total volume of material that may meet the current definition of transuranic waste (22,100 cubic yards [16,900 cubic meters]) is somewhat larger than that assumed for the 1997 WIPP Disposal Phase Final Supplemental Environmental Impact Statement (about 18,300 cubic yards (14,000 cubic meters) of buried contact-handled transuranic waste and 157 cubic yards (120 cubic meters) of buried remote-handled transuranic waste) (DOE 1997a).*

Table I–53 Volumes of Transuranic-Contaminated Materials Estimated to be Within Los Alamos National Laboratory Material Disposal Areas

| Technical Area | Material Disposal Area | Transuranic-Contaminated Material Buried in Pits or Absorption Beds (cubic meters) | | Transuranic-Contaminated Material Buried in Shafts (cubic meters) | | Total Transuranic-Contaminated Material in Pits, Absorption Beds, and Shafts (cubic meters) | |
|----------------|------------------------|--|---|---|---|---|---|
| | | Transuranic Waste ^a | Alpha-Contaminated Low-Level Radioactive Waste ^b | Transuranic Waste ^a | Alpha-Contaminated Low-Level Radioactive Waste ^b | Transuranic Waste ^a | Alpha-Contaminated Low-Level Radioactive Waste ^b |
| 21 | A | 700 | 13,300 | – | – | 700 | 13,300 |
| 21 | B | 525 ^c | 20,475 ^{c,d} | – | – | 525 ^c | 20,475 ^c |
| 50 | C | 2,600 | 100,400 ^e | 70 | 70 | 2,670 | 100,470 |
| 54 | G | 4,785 | 179,215 | 6 | 1,044 | 4,791 | 180,259 |
| 21 | T | 162 | 2,538 | 3,610 | 190 | 3,772 | 2,728 |
| 49 | AB | – | – | 4,400 | – | 4,400 | – |
| 21 | V ^f | – | 4,300 ^f | – | – | – | 4,300 ^f |
| Total | | 8,772 | 320,228 | 8,086 | 1,304 | 16,858 | 321,532 |

^a For the DOE study, this material was assumed to meet the current DOE definition of transuranic waste.

^b For the DOE study, this material was assumed to meet the current DOE definition of low-level radioactive waste, but would contain alpha-emitting transuranic isotopes having half-lives exceeding 20 years and in concentrations between 10 and 100 nanocuries per gram. “Alpha-contaminated low-level radioactive waste” is not an official DOE waste category, but was considered for this appendix to enable enhanced analysis of possible impacts from radioactive waste transportation.

^c More recent analyses of waste in MDA B (LANL 2006i) suggest that these estimates of transuranic and alpha-contaminated low-level radioactive waste volumes in MDA B may be over-conservative.

^d The DOE database (DOE 1999g) estimates that 5,000 cubic meters of the alpha-contaminated low-level radioactive waste in MDA B may be mixed waste.

^e The DOE database (DOE 1999g) estimates that 25,100 cubic meters of the alpha-contaminated low-level radioactive waste in MDA C may be mixed waste.

^f The transuranic content of this waste was over-estimated. None of the material from MDA V removal (completed in May 2006) exceeded 10 nanocuries of transuranic radionuclides per gram of waste (LANL 2006a).

Note: To convert cubic meters to cubic yards, multiply by 1.308.

Sources: DOE 1999g, 2000a.

I.3.3.2.4.2 Waste and Bulk Material Requirements for Removal of Large Material Disposal Areas

This section summarizes estimates of wastes and bulk material requirements for removal of MDAs A, B, T, U, AB, C, G, and L. Summaries of waste generation and shipment of solid wastes from these MDAs are in **Table I–54**. Summaries of volumes and shipments of bulk materials such as soil and backfill are in **Table I–55**. Summaries for liquid wastes are in **Table I–56**, based on information from LANL (LANL 2006a).

The listed volumes include wastes from preliminary site work such as destruction of fencing and removal of concrete and asphalt slabs over portions of the MDAs. Listed volumes for both wastes and materials are in situ volumes. Shipment estimates for wastes and bulk materials reflect the assumption of 20 percent swell of soil once removed from the ground. This swell assumption is applied to removed waste because much of it will be soil and debris.

Table I-54 Waste Volumes and Shipments for Removal of Material Disposal Areas A, B, C, G, L, T, U, and AB

| Material Disposal Area | Solid | Chemical ^a | Low-Level Radioactive Waste | | | | | | Transuranic Waste | | Total |
|------------------------------|--------|-----------------------|-----------------------------|--------------------|---------|-------------|----------------|----------------------|-------------------|----------------|---------|
| | | | Low Activity | Mixed Low Activity | Alpha | Mixed Alpha | Remote Handled | Mixed Remote Handled | Contact Handled | Remote Handled | |
| Volumes (cubic yards) | | | | | | | | | | | |
| A | 1,200 | 440 | 1,800 | 130 | 16,000 | 1,700 | – | – | 1,100 | – | 22,000 |
| B ^b | 10,000 | 3,100 | 9,800 | 1,000 | 20,000 | 6,500 | – | – | 690 | – | 51,000 |
| C | 22,000 | 10,000 | 22,000 | 2,700 | 99,000 | 33,000 | 6.6 | 0.7 | 3,400 | 46 | 190,000 |
| G | 1,500 | – | 620,000 | 69,000 | 210,000 | 24,000 | 1,200 | 140 | 6,300 | 3.9 | 940,000 |
| L | 54 | 3,300 | – | – | – | – | – | – | – | – | 3,400 |
| T | 43 | – | 230 | 32,000 | – | 3,600 | – | – | 4,900 | – | 41,000 |
| U | 20 | – | 570 | 12 | – | – | – | – | – | – | 600 |
| AB | 13 | 1,600 | 2,900 | 3,700 | – | – | – | – | 5,800 | – | 14,000 |
| One-Way Shipments | | | | | | | | | | | |
| A | 95 | 37 | 130 | 10 | 1,200 | 140 | – | – | 120 | – | 1,800 |
| B ^b | 760 | 260 | 690 | 82 | 1,600 | 520 | – | – | 80 | – | 4,000 |
| C | 1,700 | 850 | 1,500 | 220 | 7,900 | 2,600 | 3 | 1 | 400 | 70 | 15,000 |
| G | 110 | – | 44,000 | 5,500 | 17,000 | 1,900 | 590 | 66 | 730 | 6 | 70,000 |
| L | 4 | 280 | – | – | – | – | – | – | – | – | 280 |
| T | 3 | – | 16 | 2,600 | – | 280 | – | – | 570 | – | 3,400 |
| U ^c | 2 | – | 40 | 1 | – | – | – | – | – | – | 42 |
| AB | 1 | 130 | 200 | 300 | – | – | – | – | 670 | – | 1,300 |

^a Includes wastes regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for disposal in a sanitary landfill.

^b These volumes and shipments are based on conservative assumptions about the quantities and radiological characteristics of waste from complete removal of waste from MDA B. Most recent projections of waste from MDA B removal are in Section I.3.3.2.7. Total volumes of waste from these more recent estimates are smaller than those presented in this table.

^c These volumes and shipments are based on conservative assumptions about the waste's resulting from complete removal of MDA U. NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b).

Note: Volumes are in situ volumes. As-shipped volumes would be larger because of swell of excavated material and packing efficiencies being smaller than 100 percent.

Volumes include waste from preliminary site work such as fencing removal but not DD&D of structures. To convert cubic yards to cubic meters, multiply by 0.76456.

Because numbers have been rounded, the sums may not equal indicated totals.

Table I-55 Volumes and Shipments of Bulk Materials for Removal of Material Disposal Areas A, B, C, G, L, T, U, and AB

| <i>Material Disposal Area</i> | <i>Cover Removed</i> | <i>Additional Soil Removed</i> | <i>Total Stockpiled Soil Returned</i> | <i>Additional Fill</i> | <i>Topsoil</i> | <i>Total</i> |
|-------------------------------|----------------------|--------------------------------|---------------------------------------|------------------------|----------------|--------------|
| Volumes (cubic yards) | | | | | | |
| A | 6,100 | 12,000 | 18,000 | 21,000 | 1,100 | 58,000 |
| B ^a | 19,000 | 12,000 | 32,000 | 48,000 | 3,200 | 110,000 |
| C | 57,000 | 340,000 | 390,000 | 190,000 | 9,500 | 990,000 |
| G ^b | 220,000 | 2,900,000 | 3,200,000 | 930,000 | 36,000 | 7,300,000 |
| L | 4,800 | 9,500 | 14,000 | 3,300 | 810 | 33,000 |
| T | – | 270,000 | 230,000 | 41,000 | 3,200 | 540,000 |
| U ^c | 480 | 610 | 1,100 | 580 | 81 | 2,800 |
| AB | 6,800 | 12,000 | 18,000 | 14,000 | 1,100 | 52,000 |
| One-Way Shipments | | | | | | |
| A | 430 | 840 | 1,300 | 1,500 | 78 | 4,100 |
| B ^a | 1,400 | 870 | 2,200 | 3,400 | 230 | 8,100 |
| C | 4,000 | 24,000 | 28,000 | 14,000 | 670 | 70,000 |
| G ^b | 15,000 | 210,000 | 220,000 | 66,000 | 2,600 | 520,000 |
| L | 340 | 670 | 1,000 | 230 | 57 | 2,300 |
| T | – | 19,000 | 16,000 | 2,900 | 230 | 38,000 |
| U ^c | 34 | 43 | 78 | 41 | 6 | 200 |
| AB | 480 | 830 | 1,300 | 990 | 80 | 3,700 |

^a These volumes and shipments are associated with conservative assumptions about the quantities of waste resulting from complete removal of waste from MDA B. Removal of smaller volumes of waste from MDA B, as projected in Section I.3.3.2.7, should result in smaller volumes of bulk materials moved.

^b Capping the remain disposal units in the existing Area G footprint following MDA removal is projected, depending on whether a thick or thin cap would be installed, to require from 190,000 to 510,000 cubic yards (140,000 to 390,000 cubic meters) of crushed tuff, and 160,000 cubic yards (120,000 cubic meters) of additional material. One-way shipments of crushed tuff would range from 15,000 to 40,000, with 12,000 shipments of additional material.

^c The volume and shipments are based on conservative assumptions about removal of waste from MDA U. NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b). Note: To convert cubic yards to cubic meters, multiply by 0.76456. Because numbers have been rounded, the sums may not equal the indicated totals.

MDA A

This MDA consists of the two relatively long and narrow Eastern Pits, a large Central Pit, and the two General's Tanks containing contaminated sludge. Challenges include: (1) the uncertain waste inventory; (2) its location between DP East and DP West; (3) the proximity of TA-21 to populated areas; and (4) the General's Tanks.

The same buildings, piping, and other structures assumed to be removed as part of capping MDA A (Section I.3.3.2.2.1) would be removed before site exhumation.

Table I-56 Liquid Waste Volumes and Shipments from Large-Material-Disposal-Area Exhumation

| <i>Material Disposal Area</i> | <i>Industrial</i> | <i>Hazardous</i> | <i>Low-Level Radioactive</i> | <i>Mixed Low Level</i> | <i>Total</i> |
|--------------------------------------|-------------------|------------------|------------------------------|------------------------|----------------|
| Volumes (gallons) | | | | | |
| A | – | – | 75 | – | 75 |
| B ^a | 2,000 | – | 450 | – | 2,450 |
| C | 55 | – | – | – | 55 |
| G | – | – | – | – | – |
| L | – | 10,000 | – | – | 10,000 |
| T | – | – | – | – | – |
| U | – | – | – | – | – |
| AB | – | – | – | – | – |
| One-Way Shipments^a | | | | | |
| A | – | – | 1 ^b | – | 1 ^b |
| B ^a | 3 | – | 1 ^b | – | 3 |
| C | 1 ^b | – | – | – | 1 ^b |
| G | – | – | – | – | – |
| L | – | 13 | – | – | 13 |
| T | – | – | – | – | – |
| U | – | – | – | – | – |
| AB | – | – | – | – | – |

^a More recent estimates of liquid waste from removal of MDA B (Section I.3.3.2.7) are smaller than those presented in this table.

^b Indicates less than a full shipment.

Note: To convert gallons to liters, multiply by 3.78533.

Pits. The two Eastern Pits are each 125 by 18 by 13 feet deep (38 by 5.5 by 4.0 meters deep). The site was assumed to be initially graded, resulting in the removal of 0.2 acre (0.08 hectare) to an average depth of 3 feet (0.9 meters). About 970 cubic yards (742 cubic meters) of soil would be stockpiled for reuse. Excavation was assumed to resemble a general prismatoid, having walls sloping at angles of 45 degrees. This assumption results in an excavation having dimensions of 82 by 151 feet (25 by 46 meters) on the surface and 56 by 125 feet (17 by 38 meters) at the base of the excavation. The total amount of waste removed (before sorting) was estimated to be 2,200 cubic yards (1,700 cubic meters). In addition, 50 cubic yards (38 cubic meters) of contaminated soil was assumed to be removed from the former drummed storage area⁵⁹ (LANL 2006a).

Assuming the distance between the pits is 20 feet (6.1 meters), the total amount of clean soil removed (before bulking) is 2,400 cubic yards (1,900 cubic meters). This material was assumed to be stored and returned to the excavation, along with the material originally removed, and 2,200 cubic yards (1,700 cubic meters) (as compacted) of additional backfill. Topsoil and materials to promote vegetation would total 161 cubic yards (123 cubic meters).

The Central Pit has a depth of 22 feet (6.7 meters) and a total capacity of 18,700 cubic yards (14,300 cubic meters). The waste mass was assumed to have a surface area of 23,000 square feet (2,140 square meters); the length of this surface area (assumed to be a square) was 152 feet (46 meters). About 0.9 acre (0.36 hectare) of soil having an average thickness of

⁵⁹ The soil was contaminated from leaking drums of stable iodine in a NaOH solution.

3 feet (0.9 meters) would be initially removed (4,360 cubic yards [3,330 cubic meters]). The total volume of waste and soil then excavated would be 24,800 cubic yards (19,000 cubic meters), of which 6,060 cubic yards (4,600 cubic meters) would be soil meeting screening levels. This soil, as well as the top cover initially removed, would be stored and then returned to the excavation after waste removal, along with 18,700 cubic yards (14,300 cubic meters) of additional soil (as compacted in place). Topsoil and other growth media would be added and compacted, sufficient to cover an area of about 0.9 acre (0.36 hectare).

It was assumed that removal of contaminated material from the MDA pits would result in 916 cubic yards (700 cubic meters) of contact-handled transuranic waste and 17,400 cubic yards (13,300 cubic meters) of alpha-contaminated low-level radioactive waste (DOE 1999g, 2000a). These volumes represent in situ volumes and may be overestimates. It was assumed that the transuranic and alpha-low-level waste referenced in the DOE database was entirely contained in the Central Pit. The Eastern Pits were used during the 1940s, while the Central Pit was used during the 1970s, when programs generating transuranic-contaminated wastes were more extensive. Also, the projected total volume of waste from the Eastern Pits is much smaller than the total quantity of transuranic and alpha-contaminated low-level wastes, (18,300 cubic yards [14,000 cubic meters]) projected in the DOE database (DOE 1999g). It was assumed that 10 percent of the alpha-contaminated low-level radioactive waste would be mixed.

The remaining 425 cubic yards (325 cubic meters) of waste from removal of the Central Pit was assumed to be 40 percent solid waste, 15 percent chemical waste, 40 percent low-activity low-level radioactive waste, and 5 percent mixed low-activity low-level radioactive waste. (As reported in 1989 by Gerety, Nyhan, and Olive, the Central Pit in MDA A received waste from operations in TA-21, as well as plutonium-contaminated debris from the demolition of Building TA-21-12, a two-story frame and masonry building, after which it continued to receive waste through 1977 [LANL 1989]). A similar distribution was assumed for the 2,170 cubic yards (1,660 cubic meters) removed from the Eastern Pits. The 50 cubic yards (38 cubic meters) of contaminated soil removed from the former drummed storage area was assumed to be chemical waste. It was added to the chemical waste projected from the Eastern Pits.

General's Tanks. The General's Tanks have each been placed on four concrete piers and buried in two pits. The tanks are parallel to one another and about 20 feet (6.1 meters) apart. An 8-inch (70-centimeter) concrete slab was poured above both tanks (see Figure I-6), and soil was mounded above the concrete slab to about 5 feet (1.5 meters) above grade. A vent extends above one end of each tank. At the other end of each tank, a fill pipe leads to a concrete box on the surface.

Because the tanks are large and may be of questionable structural integrity, it was assumed that the tanks could not be removed intact. Rather, it was assumed that the tanks would be exposed and cut into sections for disposal. Removing the tanks in this manner is expected to be difficult, requiring extensive controls to protect health, safety, and the environment.

To expose the tanks, the soil mounded above the concrete slab above the tanks would be removed, as would the concrete slab. From Section I.2.5.2.1, it was estimated that the slab covers 3,860 square feet (360 square meters), and with the earth cover 10 percent more, for a total of 4,250 square feet (400 square meters). About 790 cubic yards (600 cubic meters) of soil

cover would thus be removed and stored, and 95 cubic yards (73 cubic meters) of solid waste would be generated from removal of the concrete slab.

The excavation would likely extend to the bottom of the concrete piers and somewhat to the sides of the tanks. The depth of excavation was assumed to be 14 feet (4.3 meters); the surface area at the base of the excavation was assumed to be 6,000 square feet (560 square meters); and the excavation footprint at the top of the excavation was assumed to be 11,300 square feet (1,050 square meters). After the tanks were removed, the total excavated void would be 4,400 cubic yards (3,370 cubic meters).

Waste from removal of the tanks would include the eight concrete piers (33 cubic yards [26 cubic meters]), the two fill boxes (2.6 cubic yards [2.0 cubic meters]), some piping, contaminated soil, and contaminated metal scrap from cutting apart the tanks. The piping should be very small in volume. Contaminated soil volume was estimated by assuming a 3-foot-thick (0.9-meter-thick) contaminated band around the outsides of both tanks. This volume would be 700 cubic yards (530 cubic meters). It was assumed that all of this waste except for the sectioned tanks would be low-activity low-level radioactive waste.

It was assumed that before the tanks were dismantled, as much contamination would be removed as reasonably practical. In so doing, the inside walls and support structures would be washed using remotely operated equipment and available technologies such as the jet grout system discussed in Section I.3.3.2.2.5. The inventory within the tank would be then fixed in place to minimize dispersion during cutting.

As the tank is cut into sections, the sections would be placed into containers for disposal. Assuming that the tanks have an average thickness of 0.5 inches (1.3 centimeters), and assuming an average steel density of 0.286 pounds per cubic inch, about 54 tons (49 metric tons) of contaminated steel would be generated. This mass was increased by 10 percent to account for internal and ancillary structures, totaling 59 tons (53 metric tons). The tanks were in use for about 30 years before the stored material was removed, and about 30 years have passed since this removal occurred. The distribution of contamination within interior tank surfaces is unknown. Therefore, all of the waste from sectioning the tanks was assumed to be contact-handled transuranic waste. Each standard waste box for WIPP can contain 63 cubic feet (1.8 cubic meters) of waste, having a maximum weight of 4,000 pounds (1.8 metric tons). Assuming 4,000 pounds per box, this implies a transuranic waste volume of about 68 cubic yards (52 cubic meters). However, operational restrictions would probably reduce the amount of waste that could be shipped per container. Consistent with the approach taken for other wastes in this analysis (see Section I.3.5), the as-shipped volume was assumed to be somewhat larger.

The soil initially removed over the top of the tanks would be used as backfill. Some of the soil removed as part of exposing the tanks for dismantlement would be returned as well. About 210 cubic yards (160 cubic meters) of topsoil and other growth media would be spread on top of the backfill.

MDA B

The configuration and inventory of radioactive and hazardous constituents within MDA B is not well known. Additional challenges include: (1) the site is large and relatively close to the Los Alamos community; (2) the only paved road access to TA-21 lies immediately north of and parallels the site; (3) businesses exist on the other side of this road opposite to MDA B; and (4) the topography to the south of MDA B falls off quickly to BV Canyon.

LANL personnel plan an investigation and remediation program at MDA B that will remove all waste. For this appendix, a conservative analysis was performed on the quantities of waste that could result from complete removal of MDA B. This analysis resulted in larger quantities of wastes than those estimated by LANL for the investigation and remediation program (see Section I.3.3.2.7).

From the 2004 Investigation Work Plan for MDA B (LANL 2004d) the total volume of waste from MDA B removal was assumed to be 47,900 cubic yards (35,600 cubic meters). It was assumed that all waste in and about MDA B could be represented as a single trench having dimensions of 2,000 by 52 feet (610 by 16 meters). Assuming an average soil cover of 3 feet (0.9 meters), this corresponds to an average depth of the representative trench of 15.5 feet (4.7 meters) (including 12.5 feet [3.8 meters] of waste and backfill).

Soil was assumed to be removed to a depth of 3 feet (0.9 meters) over an area of 4 acres (1.6 hectares), which covers the footprint of the assumed representative trench (about 2.4 acres [0.97 hectare]) plus a small space (a little over 15 feet [4.6 meters]) around it. This results in an initial top cover removal of 19,400 cubic yards (14,800 cubic meters). A pit was assumed having an average depth of 12.5 feet (3.8 meters), sides sloping back at 45 degrees, a base of about 2,000 by 52 feet (610 by 16 meters), and a top footprint of 2,025 by 77 feet (617 by 23 meters). About 60,100 cubic yards (46,000 cubic meters) of waste and soil would be exhumed, of which 12,200 cubic yards (9,330 cubic meters) would be soil meeting screening levels. This soil would be temporarily stored. The remaining 47,900 cubic yards (36,600 cubic meters) of excavated material was assumed to be waste.

Using the DOE database for buried transuranic-contaminated waste (DOE 1999g, 2000a), it was assumed that complete removal of MDA B would generate 686 cubic yards (525 cubic meters) of contact-handled transuranic waste, 20,240 cubic yards (15,475 cubic meters) of alpha low-level radioactive waste and 6,540 cubic yards (5,000 cubic meters) of mixed alpha low-level radioactive waste. This assumption may be a significant overestimate.⁶⁰ A precise determination of the quantities of transuranic-contaminated materials buried in MDA B will result from the MDA B investigation and remediation program described in Section I.3.3.2.7.

The remaining 20,400 cubic yards (15,600 cubic meters) of waste was distributed as follows: 40 percent industrial solid waste, 15 percent chemical waste, 40 percent low-activity low-level radioactive waste, and 5 percent mixed low activity low-level radioactive waste. A relatively large fraction of the waste was assumed to contain hazardous constituents because it was an early

⁶⁰ Average transuranic concentrations within MDA B were estimated based on projected radionuclide inventories, total waste volumes as assumed above, and a density of 1.6 grams per cubic centimeter. The average transuranic concentration was 0.4 nanocuries per gram.

disposal site (1945 to 1948) used for disposal of all types of waste. The MDA received chemicals from laboratories and may include chemical waste disposal pits.

After waste is removed, the stored clean soil would be returned and backfilled, along with 47,900 cubic yards (36,600 cubic meters) (as compacted) of clean soil from a local borrow and 3,230 cubic yards (2,470 cubic meters) of materials intended to support revegetation.

MDA T

This MDA consists of four absorption beds plus 62 shafts used for disposal of higher-activity waste. The depths of contamination beneath the absorption beds are not well known.

Contamination under Absorption Bed 1 has been found at 100 feet (30 meters) below ground surface. The shaft depths range to 60 feet (18 meters) below the ground surface. In addition to these challenges: (1) MDA T is located nearby existing structures in TA-West; (2) several buried pipes and utilities are in the vicinity of MDA T; (3) the North Perimeter Road runs along the northern side of MDA T; and (4) the land slopes steeply down to DP Canyon to the north of MDA T.

Removal would follow actions needed to relocate or remove nearby buildings, structures, and underground piping and utilities at risk (see Section I.3.3.2.2.1). DD&D of buildings and structures in the vicinity of MDA T is addressed in Appendix H, Section H.2.

Although the total volume comprising the four absorption beds is 2,100 cubic yards (1,630 cubic meters), the volume of contaminated material will be larger because water and liquid waste was discharged to the beds. For at least one absorption bed (Bed 1), contamination may extend to a depth of 100 feet (30 meters).

For this appendix, it was assumed that contamination moved vertically from all beds to a depth of 100 feet (30 meters). This assumption was considered conservative because it extends contamination to greater depths than may be realistic for all beds. This assumption results in a total contaminated volume beneath the beds of 35,600 cubic yards (27,200 cubic meters). Using the DOE transuranic waste database, it was assumed that removal of the beds would generate 212 cubic yards (162 cubic meters) of transuranic waste and 3,320 cubic yards (2,538 cubic meters) of alpha-contaminated low-level radioactive waste (DOE 1999g, 2000a). Because the beds received metals and organic and inorganic chemicals, much of this alpha-contaminated low-level radioactive waste may be mixed waste. For conservatism it was assumed that all would be mixed. It was also assumed the remaining 32,000 cubic yards (24,500 cubic meters) of waste would be mixed low-activity low-level radioactive waste.

The total volume of waste to be removed from the shafts was assumed to be equivalent to the envelope volume of the shafts, which is 5,200 cubic yards (3,990 cubic meters).⁶¹ From the DOE database, it was assumed that complete removal of the shafts would generate 4,720 cubic yards (3,610 cubic meters) of transuranic waste and 250 cubic yards (190 cubic meters) of alpha-contaminated low-level radioactive waste (DOE 1999g, 2000a). Because the cement paste

⁶¹ The shafts were not filled to the top with waste. Nonetheless, use of the envelope volume of the shaft to estimate waste volumes should offset the unknown extent to which contamination may have moved beneath and laterally from the shafts. Because the larger shafts, at least, were lined with asphalt, lateral movement may be small.

placed in the shafts probably contained most of the same chemicals discharged to the beds, most of both types of waste may be mixed. For conservatism, it was assumed that all would be mixed. It was also assumed that all transuranic waste resulting from shaft removal would be contact-handled transuranic waste.

The remaining waste volume implied by the shaft dimensions, 252 cubic yards (193 cubic meters) was assumed to be 90 percent low-activity low-level radioactive waste and 10 percent mixed low-activity low-level radioactive waste. It was assumed that this waste would consist mainly of contaminated backfill and asphalt.

Excavation of the bed contamination and the shafts was assumed to have base dimensions of 150 by 300 feet (46 by 92 meters) and a depth of 100 feet (30 meters). This size should be sufficient for all absorption beds plus the shafts. The sides for the top 20 feet (6.1 meters) of the excavation, which is soil, were assumed sloped at an angle of 3 horizontal to 1 vertical. The sides for the bottom feet of the excavation, which is rock, were assumed sloped at an angle of 0.5 horizontal to 1 vertical. These assumptions result in a surface footprint of 175,000 square feet (16,300 square meters) and a total removed volume of 266,000 cubic yards (203,000 cubic meters) of soil, rock, and waste (LANL 2006a).⁶² Subtracting waste, 225,000 cubic yards (172,000 cubic meters) of uncontaminated soil would be stockpiled. This material would be returned to the excavation along with 40,800 cubic yards (31,200 cubic meters) of additional fill (as compacted) from a local borrow. The top of the excavation would be replanted, requiring 3,240 cubic yards (2,480 cubic meters) of additional material.

MDA U

MDA U consists of two absorption beds, each having lengths of 80 feet (24 meters), widths of 20 feet (6.1 meters), and depths of 6 feet (1.8 meters) below the original ground surface. A portion of the contamination in the absorption beds was removed in 1985 by excavating a 20- by 100- by 4-to 13-foot (6.1 by 30 by 1.2 to 4.0 meter) trench. For this appendix, the remaining contamination was assumed to be a volume of material 60 by 20 by 13 feet deep (18 by 6.1 by 4 meters deep), or 578 cubic yards (442 cubic meters).⁶³

It was assumed that the top 3 feet (0.9 meters) of soil would be removed over an area of 2,630 square feet (244 square meters), which covers the 60- by 20- foot (18- by 6.1-meter) area addressed above plus 15 feet (4.6 meters) on all sides. This would result in the initial removal of 480 cubic yards (370 cubic meters) of soil cover. Excavating the waste was then modeled as a pit having a base dimension of 60 by 20 feet (18 by 6.1 meters), a surface footprint of 86 by 46 feet (26 by 14 meters), and a volume of 1,190 cubic yards (910 cubic meters). This volume was assumed to comprise 580 cubic yards (440 cubic meters) of waste and 610 cubic yards (470 cubic meters) of soil meeting screening action levels. This soil would be stockpiled for later return to the excavation.

⁶²Uncontaminated topsoil (such as that over the shafts) is included in this volume.

⁶³The 2006 Investigation Report for MDA U concluded that neither additional corrective action nor further characterization was required and that the land use be maintained as industrial (LANL 2006e). NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006a). The Removal Option is herein considered for completeness.

The waste removed from MDA U was assumed to consist of low-activity and mixed low-activity low-level radioactive waste. This assumption is consistent with that for excavation of MDA V (LANL 2004j), which comprises a set of absorption beds used to receive liquid wastes from a laundry. Similar to MDA V, it was assumed that 98 percent would be low-activity low-level radioactive waste and 2 percent would be mixed low-activity low-level radioactive waste.⁶⁴

After waste removal, the 1,090 cubic yards (840 cubic meters) of removed topsoil and clean soil from the excavation would be returned and compacted. An additional 580 cubic yards (444 cubic meters) (as compacted) of clean soil would be delivered, as would 81 cubic yards (62 cubic meters) of materials to support vegetation.

MDA AB

The hydronuclear and support shafts at Areas 1, 2, 2A, 2B, and 4 in MDA AB contain large inventories of plutonium, uranium, beryllium, and lead and are at depths to 142 feet (43 meters) below ground surface. Shafts at Area 3 in MDA AB have much smaller levels of contamination to depths of 57 to 142 feet (43 meters). Wastes resulting from exhumation of MDA AB were assumed to consist of two groups: concentrated waste from the bottoms of the shafts, and lower-activity material, including surface contaminated metals and other wastes that were placed in dump and test shafts.

Regarding the first group of wastes, because large quantities of lead and beryllium were used in the tests, all of the wastes possibly generated from exhuming the wastes at the bottom of the shafts were assumed to be either mixed waste or chemically hazardous waste. The DOE database on buried transuranic-contaminated material (DOE 1999g, 2000a) estimates that the bottoms of the shafts contain 5,755 cubic yards (4,400 cubic meters) of material that would meet current definitions of transuranic waste. This estimate is consistent with an assumption that the bulk of the contamination is within a radius of about 10 feet (3 meters) from the detonation points in the 37 shafts (LANL 1992b) where plutonium was used in the tests. Regarding the other test shafts, 6 shots used uranium-235, 7 shots used uranium-238, 11 shots used tracers, and 11 shots were containment shots (LANL 1992b). Possible waste volumes from exhuming the contamination from these shots were estimated by determining the volumes represented by 10-foot-radius (3-meter-radius) spheres of contamination at the bottoms of the shafts. The uranium and tracer shot contamination was assumed to be mixed low-activity low-level radioactive waste. The containment shot contamination was assumed to be chemical waste.

Regarding the second group of wastes, it is difficult to project those shafts that may contain contaminated material and the depths to which the material was placed before backfilling.⁶⁵ The summed depth of all test shafts is 5,070 feet (1,550 meters). Assuming 6-foot-diameter (1.8-meter-diameter) shafts, on average, a total volume in the shafts of 5,310 cubic yards (4,060 cubic meters) is implied. Assuming that, on average, the bottom half of all shafts would

⁶⁴ The MDA U beds probably received organic and inorganic chemicals, plus acids and oils, implying that much of the waste originally in the beds may have been mixed. However, most of the original contamination has been removed, and the extent to which removal of residual contamination may generate mixed waste is unknown.

⁶⁵ Burial depth may be highly variable. Waste was dumped in the test holes and in an unknown number of shallow holes of small diameter.

be contaminated, 2,660 cubic yards (2,030 cubic meters) of low-activity low-level radioactive waste would be generated. It was assumed that 10 percent of this waste would be mixed.

Excavating the waste presents a challenge because of the depth of the contamination and because of the contaminated metal and other materials disposed of in the shafts. Excavation might be accomplished partly using conventional excavators such as backhoes and partly using remote techniques such as suspending excavating tools from cranes.

It was assumed that the top 3 feet (0.9 meters) of soil would be removed over the six main areas composing MDA AB. Assuming a total surface area over these six areas of 1.4 acres (6.6 hectares), the total volume of earth removed would be 6,780 cubic yards (5,180 cubic meters). Assuming that about 3 feet (0.9 meters) around each existing 6-foot-diameter (1.8-meter-diameter) shaft would be removed (that is, 12-foot-diameter (3.7-meter-diameter) shafts would be excavated), then 25,600 cubic yards (19,600 cubic meters) of waste and soil would be removed before sorting between waste and clean soil. This would result in 11,700 cubic yards (8,950 cubic meters) of material meeting screening levels and 13,900 cubic yards (10,600 cubic meters) of waste. The material meeting the screening levels would be placed back into the holes, as well as other stored material. About 13,900 cubic yards (10,600 cubic meters) of clean crushed tuff would be imported from a local borrow, as well as 1,130 cubic yards (864 cubic meters) of materials intended to promote vegetation growth.

MDA C

MDA C is a large disposal area consisting of six large radioactive waste pits, a smaller chemical pit, and 108 shafts. Both the shafts and the pits contain a variety of chemicals, some of which may be reactive. The shafts were usually used for disposal of wastes presenting an external radiation hazard. MDA C is immediately south of structures associated with TA-50 waste management operations.

Removal would follow actions needed to relocate or remove nearby buildings, structures, and underground piping and utilities at risk.

The physical relationship of the various rows of shafts with respect to the pits presents safety concerns. Assuming excavation of Pit 3, which has an as-built depth of 25 feet (7.6 meters), there may be concern about the potential for sidewall collapse leading to exposure of the contamination in Shaft Group 2. Assuming excavation of Pits 1 through 4, there may be concerns about end-wall collapse leading to exposure of contamination in Shaft Group 3. A retaining wall may be needed between Shaft Group 1 and Pit 5, or a wall between Shaft Group 3 and the ends of Pits 1 through 4.

From the nominal dimensions of the shafts and pits, the projected volumes of wastes are:

- Pits: 190,830 cubic yards (145,900 cubic meters)
- Shafts: 198 cubic yards (151 cubic meters)

This results in a total waste generation of about 191,000 cubic yards (146,000 cubic meters).

Assuming a surface area of 11.8 acres (4.8 hectares) (Stephens 2005), a volume of 57,100 cubic yards (43,660 cubic meters) of surface soil would be removed and stockpiled.

Excavation was assumed to occur in two groups: one group is Pit No. 6 and the chemical pit, and the second is the remaining pits plus the shafts. Regarding the first group, assuming the excavation walls slope at angles of 45 degrees from the pits, and assuming an average excavation depth of 25 feet (7.6 meters), removing Pit 6 and the chemical pit would excavate 48,800 cubic yards (37,300 cubic meters) of waste and 17,200 cubic yards (13,140 cubic meters) of clean soil.⁶⁶ Regarding the second group, assuming that removal of the pits would include excavating the spaces between the pits, the area covered by the footprint of these pits and shafts would cover 10.5 acres (4.2 hectares). Assuming the soil on all sides of this footprint would be sloped at 45-degree angles, and assuming an average excavation depth of 25 feet (7.6 meters), 318,000 cubic yards (243,000 cubic meters) of clean soil would be excavated along with 142,000 cubic yards (109,000 cubic meters) of waste.

From the DOE database on buried transuranic contamination (DOE 1999g, 2000a), it was assumed that exhuming the MDA C pits would generate about 3,400 cubic yards (2,600 cubic meters) of transuranic waste (including 880 cubic yards [675 cubic meters] of mixed transuranic waste) and 131,240 cubic yards (100,400 cubic meters) of alpha-contaminated low-level radioactive waste, of which 32,810 cubic yards (25,100 cubic meters) would be mixed waste. It was assumed that transuranic waste generated from exhuming pits would be contact-handled waste. Assuming a total waste volume of 191,000 cubic yards (146,000 cubic meters), then the remaining radioactive waste would amount to 54,300 cubic yards (41,500 cubic meters). Exhuming the chemical pit was assumed to generate 2,000 cubic yards (1,530 cubic meters) of hazardous waste. The remaining waste from pit exhumation was assumed to consist of 40 percent solid waste, 15 percent chemical waste, 40 percent low-activity low-level radioactive waste, and 5 percent mixed low-activity low-level radioactive waste. These distributions were assumed because the pits were used mostly in the 1950s, and disposal logbooks as well as other information suggest that the pits were used for disposal of hazardous constituents as well as general trash and demolition waste (see Section I.2.5.4).

From the DOE database on buried transuranic-contaminated material (DOE 1999g, 2000a), it was assumed that exhumation of the MDA C shafts would generate 92 cubic yards (70 cubic meters) of transuranic waste and 92 cubic yards (70 cubic meters) of alpha-contaminated low-level radioactive waste. Similar to the assumptions for waste resulting from exhuming MDA G shafts (see below), it was assumed that half of the transuranic waste would be remote-handled waste. It was assumed that 10 percent of the alpha-contaminated waste would be mixed waste.

The total volume of waste implied by the shaft dimensions is 197 cubic yards (151 cubic meters). Subtracting the transuranic and alpha-contaminated low-level radioactive waste leaves 14 cubic yards (11 cubic meters) of waste. This waste was assumed to be low-level radioactive

⁶⁶Assuming a pit having walls sloping at a 1:1 ratio and an average depth of 25 feet (7.6 meters), the surface area on the bottom of the excavation would be 109 by 505 feet = 55,000 square feet (5,110 square meters). The surface area at the top of the excavation would be 159 by 555 feet = 88,245 square feet (8,200 square meters). This provides a conservative estimate of soil and waste that may be removed from the excavation. However, shoring may be required along the northern edge of the excavation to avoid damage to structures, utilities, and piping. Shoring could reduce excavated volumes by roughly 0.5 (25 by 25 by 505 feet) = 160,000 cubic feet (4,530 cubic meters).

waste. A conservative analysis of the MDA G shafts, which were used during a time that overlapped the use of shafts at MDA C, suggests that up to 50 percent of the originally emplaced waste in MDA G may be remote-handled waste. This estimate was applied to the waste in the MDA C shafts. Therefore, it was assumed that half of the remaining 14 cubic yards (11 cubic meters) of waste from shaft removal would be remote-handled low-level radioactive waste and half would be low-activity low-level radioactive waste. Similar to assumptions for other MDAs, it was assumed that 10 percent of both the remote-handled and low-activity low-level radioactive wastes would be mixed wastes.

After waste removal, the stockpiled soil meeting screening levels would be returned to the excavation, along with 191,000 cubic yards (146,000 cubic meters) of additional backfill and about 9,520 cubic yards (7,280 cubic meters) of material promoting vegetation growth.

MDA G

This MDA is located within Area G, which contains active waste disposal units. Current waste management facilities and operations at Area G will be removed or relocated as addressed in Appendix H, Section H.3. It was conservatively assumed there would be extensive removal of the disposal units in MDA G to bound impacts that may result from MDA G remediation. As an upper-bound case, it was assumed that removal would involve all pits through 37, all four trenches used for transuranic waste storage,⁶⁷ and 194 shafts. The total volume of waste to be generated from pit removal was assumed to correspond to the field-measured volumes for the pits as given in the Historical Investigation Report for MDA G (LANL 2004c). (For other MDAs, because field-measured volumes were generally unavailable, envelope volumes implied by nominal pit dimensions were assumed.) The total volume of waste thus assumed to be generated from MDA G removal was 931,000 cubic yards (712,000 cubic meters) from the pits and trenches and 3,880 cubic yards (2,970 cubic meters) from the shafts.

It was assumed that the excavation footprint for MDA G removal could be approximated by a 40-acre (16-hectare) rectangle having sides of 4:1. It was assumed that exhumation would be nominally preceded by removal of the top 3 feet (1 meter) of soil over about 45 acres (18 hectares). Assuming an average excavation depth of 60 feet, and assuming an excavation having walls sloping at 45-degree angles, then exhumation would remove about 3,875,000 cubic yards (2,962,000 cubic meters) of waste and soil. After separating waste, about 2,940,000 cubic yards (2,248,000 cubic meters) of soil meeting screening levels would be removed and stockpiled near MDA G for backfilling into the excavation.

Although disposal operations began at MDA G in 1957, it was used later than most of the other MDAs considered in this section. Therefore, it was assumed that MDA G was not used as a general depository for all types of waste, but was used exclusively for radioactive wastes, some of which contained RCRA-constituents.

From the DOE database on buried transuranic contamination (DOE 1999g, 2000a), it was assumed that removal of the MDA G pits would generate 6,260 cubic yards (4,785 cubic meters) of transuranic waste and 234,400 cubic yards (179,215 cubic meters) of alpha-contaminated low-

⁶⁷ The transuranic waste in Trenches A–D will be removed and shipped to WIPP, as addressed in Appendix H, Section H.3. The backfill in these trenches was conservatively assumed to be contaminated and was thus included in the removal volumes.

level radioactive waste. The radioactive inventory within the pits composing MDA G was estimated using information from the Area G Performance Assessment and Composite Analysis (LANL 1997). Analysis of this inventory suggested that little, if any, of the transuranic waste that would be generated from MDA G removal would be remote handled. Hence, all was assumed to be contact-handled. About 10 percent of the alpha-contaminated low-level radioactive waste was assumed to be mixed waste. The remainder of the waste that would be generated from MDA G pit removal was assumed to be low-activity and remote-handled low-level radioactive waste.

This remaining low-level radioactive waste consists of originally emplaced waste and backfill that was assumed to be contaminated. An analysis of the originally emplaced waste suggests that up to 107 cubic yards (81.5 cubic meters) of this waste could be remote-handled low-level radioactive waste. The remaining originally emplaced waste and backfill was assumed to be low-activity low-level radioactive waste. Ten percent of the remote-handled and low-activity low-level radioactive waste was assumed to be mixed waste.

From the DOE database on buried transuranic contamination (DOE 1999g, 2000a), it was assumed that removal of the MDA G shafts would generate 7.8 cubic yards (6 cubic meters) of transuranic waste and 1,370 cubic yards (1,044 cubic meters) of alpha-contaminated low-level radioactive waste. A conservative analysis of the radionuclide inventories in the shafts indicated that up to about 50 percent could be remote-handled. Therefore, half of the transuranic waste from postulated removal of the shafts was assumed to be remote handled. About 10 percent of the alpha-contaminated low-level radioactive waste was assumed to be mixed waste.

The remaining 2,510 cubic yards (1,920 cubic meters) of the waste generated from shaft removal was assumed to be low-level radioactive waste. Similar to the assumption above for transuranic waste, it was assumed that half would be remote handled low-level radioactive waste and half would be low-activity low-level radioactive waste. It was assumed that about 10 percent of both types of waste would be mixed waste.

It was assumed that the remaining disposal units within the existing Area G footprint would be capped using either a thin or thick cap as addressed in Section I.3.3.2.1.2.3. But the cap was assumed to cover 25 acres (10.2 hectares) rather than 65 acres (26.3 hectares). Projected volumes and shipments of bulk capping materials are in a footnote to Table I-55.

MDA L

MDA L is a relatively small site once used for disposal of chemical waste. It is contained within Area L, which is currently used for authorized storage of RCRA, PCB, and mixed waste. It was assumed that all waste to be generated from MDA L removal would be hazardous waste. Disposal units subject to corrective action are listed in Table I-39. Decisions about remediation of MDA L disposal units (pursuant to the Consent Order or for other reasons) will be made in the future. For conservatism, it was assumed that all disposal units would be removed. The total waste volume from its pit, impoundments, and shafts was estimated to be 3,280 cubic yards (2,505 cubic meters).

In addition to structures removed as addressed in Appendix H, Section H.3, it was assumed that the fence near the working area would be removed and disposed of as solid waste, and a temporary security fence would be emplaced at a distance from the work area and tied into the remaining fence around MDA L. About 80 cubic yards (61 cubic meters) of asphalt would also be removed, of which half was assumed to be solid waste and half chemical waste. It was assumed that about 1 acre (0.4 hectare) of land would then be removed at a depth of about 3 feet (0.9 meters), resulting in 4,840 cubic yards (3,700 cubic meters) of soil for temporary storage.

Excavation may be difficult, particularly for shafts, because of their proximity to nearby structures and LANL operations. The pits were dug to depths of 10 to 12 feet (3.0 to 3.7 meters), and could possibly be exhumed using standard construction equipment. But the shafts have been drilled to 60-foot (18-meter) depths, and their excavation may require use of cranes. Shoring and specialized removal techniques may be needed. An excavation having sloping walls was assumed for the pit and impoundments. The base was assumed to be 80 by 300 feet (24 by 91 meters), the top footprint 324 by 104 feet (99 by 32 meters), and the depth 12 feet (3.7 meters). This results in a total excavated volume of 12,800 cubic yards (9,770 cubic meters), of which 3,280 cubic yards (2,505 cubic meters) would be waste and 9,500 cubic yards (7,260 cubic meters) would be soil meeting screening levels. This excavated soil would be stockpiled at a nearby location for replacement into the excavation. Additional crushed tuff would be backfilled. A final cover would be emplaced, requiring about 810 cubic yards (620 cubic meters) of material. An alternate proposal involving a larger amount of excavated material was submitted to NMED in January 2008 (LANL 2008a).

I.3.3.2.4.3 Wastes and Materials for Removal of Remaining Material Disposal Areas

Waste volumes from removal of several additional small MDAs are summarized in **Tables I-57**, while shipments are presented in **Table I-58**. Additional materials excavated and returned, as well as additional backfill and cover material, are presented in **Tables I-59** and **I-60**.

Less information exists about these remaining MDAs compared with previous MDAs. Waste volumes from removal of each MDA were assumed to be given by the nominal volumes of all disposal units composing the MDA (length by width by average depth). Unless the MDA includes aboveground debris (MDAs Z and R), it was assumed that 3 feet (0.9 meters) of topsoil would be removed and stored. The waste and soil then removed was represented as a general sigmatoid having walls sloping at 45-degree angles. The waste would be sorted into waste type, and clean soil would be returned along with additional fill from a LANL or local borrow pit. An additional 0.5 feet (15 centimeters) of topsoil, soil amendment, and other material would be delivered and emplaced.

The waste removed from the excavation was assumed to be distributed among different types of waste based on information from LANL (LANL 2006a). Estimates of liquids that may be generated during removal were based on LANL information (LANL 2006a).

Table I-57 Waste Projections for Removing Remaining Material Disposal Areas

| Nonliquid Wastes (cubic yards) ^a | | | | | |
|--|-------------------------|------------------------------------|---|---|---------------------------|
| <i>Material Disposal Area</i> | <i>Solid Waste</i> | <i>Chemical Waste ^b</i> | <i>Low-Level Radioactive Waste ^b</i> | <i>Mixed Low-Level Radioactive Waste ^b</i> | <i>Total Waste Volume</i> |
| F ^c | – | – | 11,000 | – | 11,000 |
| Q ^d | 3,600 | 18 | – | – | 3,600 |
| N ^e | 10,000 | 330 | 2,700 | 330 | 13,000 |
| Z ^f | 3,000 | 1,100 | 3,000 | 370 | 7,400 |
| R ^g | 26,000 | 7,700 | – | – | 33,000 |
| D ^h | 12,000 | – | 12,000 | – | 24,000 |
| E and K ⁱ | 1,800 | 2.2 | 440 | 1.1 | 2,200 |
| AA ^j | 1,300 | 380 | 2,100 | – | 3,800 |
| Y ^k | 5,300 | – | – | – | 5,300 |
| Liquid Wastes (gallons) | | | | | |
| <i>Material Disposal Area</i> | <i>Industrial Waste</i> | <i>Hazardous Waste</i> | <i>Low-Level Radioactive Waste</i> | <i>Mixed Low-Level Radioactive Waste</i> | <i>Total Waste Volume</i> |
| F | – | – | – | – | – |
| Q | – | 25 | – | – | 25 |
| N | – | – | – | 100 | 100 |
| Z | – | 55 | 500 | – | 555 |
| R | – | 5 | – | – | 5 |
| D | – | – | 100 | – | 100 |
| E and K | – | 5 | 55 | – | 60 |
| AA | – | – | – | 100 | 100 |
| Y | – | 110 | 100 | – | 210 |

^a In situ volumes reduced to two significant figures. As-shipped volumes would be larger because of swell of excavated material and packaging inefficiencies.

^b Low-level and mixed low-level radioactive wastes were assumed to be low-activity wastes. Chemical waste was assumed to include material regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

^c Assumed two pits 50 by 150 by 20 feet (15 meters by 46 meters by 6.1 meters) deep pits and four shafts 6 by 6 by 6 feet (1.8 by 1.8 by 1.8 meters).

^d Assumed one pit covering 90 by 90 by 12 feet (27 by 27 by 3.7 meters).

^e Assumed one pit covering 100 by 300 by 12 feet (30 by 91 by 3.7 meters).

^f Partly above-ground debris pile, about 20 by 200 feet (6.1 by 61 meters), with one side approximately 15 feet (4.6 meters) high and the other side at grade. Unknown depth. Assumed a virtual subsurface disposal facility 20 feet (6.1 meters) deep.

^g Shallow trash pile, comprising three 75-square-foot bermed pits. Waste was bulldozed into pits and likely spread in the vicinity. Some waste has been removed. Assumed to be 300 by 300 by 10 feet (91 by 91 by 3 meters).

^h Assumed one large excavation to remove buried chamber and elevator shaft. Assumed a 0.3-acre (0.12-hectare) footprint, 50 feet deep.

ⁱ For MDA E, assumed Pit 3 has same dimensions as largest of four pits. For the buried chamber, assumed a contaminated footprint (244 square feet [23 square meters]) describing the area of the elevator shaft (48 square feet [4.5 square meters]) and the buried chamber (approximately 196 square feet [18 square meters]). For MDA K, assumed two surface disposal piles 15 by 15 by 12 feet (4.6 by 4.6 by 3.7 meters); and 10 by 20 by 12 feet (3.0 by 6.1 by 3.7 meters).

^j Assumed two trenches, one 80 by 40 by 15 feet (24 by 12 by 4.6 meters) and a second 120 by 30 by 15 feet (37 by 9.1 by 4.6 meters).

^k Assumed three pits having dimensions estimated from the RFI Work Plan for Operable Unit 1132 (LANL 1993b).

Note: To convert cubic yards to cubic meters, multiply by 0.76456; gallons to liters, multiply by 3.785, feet to meters, multiply by 0.3048; square feet to square meters, multiply by 0.0929. Because numbers have been rounded, the sums may not equal the indicated totals.

Table I–58 One-Way Shipments from Exhuming Remaining Material Disposal Areas

| Nonliquid Wastes | | | | | |
|-------------------------------|--------------------------------|-----------------------------------|--|--|--------------------------|
| <i>Material Disposal Area</i> | <i>Solid Waste^a</i> | <i>Chemical Waste^a</i> | <i>Low-Level Radioactive Waste^a</i> | <i>Mixed Low-Level Radioactive Waste^a</i> | <i>Total^a</i> |
| F | – | – | 790 | – | 790 |
| Q | 270 | 2 | – | – | 280 |
| N | 760 | 28 | 190 | 27 | 1,000 |
| Z | 230 | 93 | 210 | 30 | 560 |
| R | 2,000 | 640 | – | – | 2,600 |
| D | 940 | – | 830 | – | 1,800 |
| E and K | 140 | – | 31 | – | 170 |
| AA | 100 | 32 | 150 | – | 280 |
| Y | 400 | – | – | – | 400 |
| Liquid Wastes | | | | | |
| <i>Material Disposal Area</i> | <i>Industrial Waste</i> | <i>Hazardous Waste</i> | <i>Low-Level Radioactive Waste</i> | <i>Mixed Low-Level Radioactive Waste</i> | <i>Total^a</i> |
| F | – | – | – | – | – |
| Q | – | 1 ^b | – | – | 1 ^b |
| N | – | – | – | 1 ^b | 1 ^b |
| Z | – | 1 ^b | 1 ^b | – | 1 ^b |
| R | – | 1 ^b | – | – | 1 ^b |
| D | – | – | 1 ^b | – | 1 ^b |
| E and K | – | 1 ^b | 1 ^b | – | 1 ^b |
| AA | – | – | – | 1 ^b | 1 ^b |
| Y | – | 1 ^b | 1 ^b | – | 1 ^b |

^a Low-level and mixed low-level radioactive wastes were assumed to be low-activity wastes. Chemical waste was assumed to include materials regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

^b The shipment contains less than a full load.

Note: Because the numbers have been rounded, the sums may not equal the indicated totals.

Table I–59 Soil and Similar Materials for Removal of Remaining Material Disposal Areas (cubic yards)

| <i>Material Disposal Area</i> | <i>Soil Cover and Initial Preparation</i> | <i>Clean Soil Exhumed</i> | <i>Stockpiled Material Returned</i> | <i>Additional Backfill</i> | <i>Topsoil and Soil Amendment</i> | <i>Total</i> |
|-------------------------------|---|---------------------------|-------------------------------------|----------------------------|-----------------------------------|--------------|
| F | 1,700 | 6,800 | 8,500 | 11,000 | 660 | 29,000 |
| Q | 900 | 1,000 | 1,900 | 3,600 | 240 | 7,700 |
| N | 3,300 | 2,200 | 5,600 | 13,000 | 740 | 25,000 |
| Z | – | 4,100 | 4,100 | 7,400 | 400 | 16,000 |
| R | – | 2,300 | 2,300 | 33,000 | 1,900 | 40,000 |
| D | 1,400 | 27,000 | 29,000 | 24,000 | 850 | 82,000 |
| E and K | 720 | 9,900 | 11,000 | 2,100 | 520 | 24,000 |
| AA | 760 | 2,600 | 3,300 | 3,800 | 310 | 11,000 |
| Y | 1,300 | 3,100 | 4,400 | 5,300 | 480 | 14,000 |

Note: To convert cubic yards to cubic meters, multiply by 0.7646. Because numbers have been rounded, the sums may not equal the indicated totals.

Table I-60 One-Way Shipments of Soil and Similar Materials for Removal of Remaining Material Disposal Areas

| <i>Material Disposal Area</i> | <i>Soil Cover and Initial Preparation</i> | <i>Clean Soil Exhumed</i> | <i>Stockpiled Material Returned</i> | <i>Additional Backfill</i> | <i>Topsoil and Soil Amendment</i> | <i>Total</i> |
|-------------------------------|---|---------------------------|-------------------------------------|----------------------------|-----------------------------------|--------------|
| F | 120 | 480 | 600 | 790 | 47 | 2,000 |
| Q | 64 | 70 | 140 | 260 | 17 | 550 |
| N | 240 | 160 | 390 | 950 | 53 | 1,800 |
| Z | – | 290 | 290 | 530 | 28 | 1,100 |
| R | – | 160 | 160 | 2,400 | 130 | 2,800 |
| D | 100 | 1,900 | 2,000 | 1,700 | 60 | 5,800 |
| E&K | 51 | 700 | 750 | 150 | 37 | 1,700 |
| AA | 54 | 180 | 240 | 270 | 22 | 760 |
| Y | 93 | 220 | 310 | 370 | 34 | 1,000 |

Note: Because numbers have been rounded, the sums may not equal the indicated totals.

MDA H. In November 2007, NMED selected a corrective remedy for MDA H involving complete encapsulation of the nine MDA H waste shafts, installation of an engineered evapotranspiration cover, and installation of a soil vapor extraction system (NMED 2007a). Implementation of this corrective remedy could produce small quantities of waste. Although uncontaminated cuttings from boreholes installed as part of the encapsulation process would be stockpiled for use in the evapotranspiration cover, contaminated drill cuttings (if any) would be properly disposed. Routine monitoring and maintenance activities may produce a very small amount of operational wastes (DOE 2004b).

I.3.3.2.5 Schedules for Material Disposal Area Removal

Schedules for removal of eight large MDAs are provided in **Table I-61**. It was generally assumed that, depending on the MDA, roughly 12 to 18 months would be needed to complete a corrective measure evaluation for an MDA. Planning for removal of an MDA would require from 4 to 8 months. Then removal would take place, with the goal of completing operations by the (adjusted) remedy completion dates in the Consent Order.

Table I-61 Temporal Assumptions for Removing Large Material Disposal Areas

| <i>Material Disposal Area</i> | <i>Assumed Start of Removal Operations</i> | <i>Assumed Completion of Removal Operations</i> | <i>Assumed Work Time (months)</i> |
|-------------------------------|--|---|-----------------------------------|
| A | 6/11/2009 | 3/11/2011 | 21 |
| B | 10/1/2008 ^a | 10/1/2010 ^a | 24 ^a |
| T | 12/19/2008 | 12/19/2010 | 24 |
| U ^b | 1/6/2011 | 11/6/2011 | 10 |
| AB | 1/1/2013 | 1/31/2015 | 24 |
| C | 11/5/2008 | 9/5/2010 | 22 |
| G | 2/6/2009 | 12/6/2015 | 82 |
| L | 5/30/2011 | 6/30/2011 | 37 |

^a This schedule is based on Revision 1 to the 2006 Investigation/Remediation Work Plan for MDA B (LANL 2006i). NMED approved the plan with modifications January 2007 (NMED 2007b).

^b The Removal Option is conservatively assumed for this appendix, although NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b).

The schedules presented in Table I–61 result in conservative estimates of waste generation and environmental impacts and are consistent with Consent Order requirements. However, if removal of a significant quantity of waste is actually contemplated for several MDAs, then schedules for completion of corrective measures at these MDAs may be difficult to meet.

If any or all of the remaining MDAs were removed, schedules would need to be developed consistent with the Consent Order. Removal of some or all of these MDAs was assumed to occur at any time starting in FY 2007 and extending through FY 2016.

I.3.3.2.6 Use of Enclosures for Material Disposal Area Removal

Enclosures may be used for removal of waste from some MDAs. The enclosures would be modular, possibly constructed of fabric over metal frames. Similar enclosures have long been used at LANL for temporary storage of transuranic waste, have been used at Rocky Flats, and are now used at Idaho National Laboratory for retrieval of waste from Pit 4 at Idaho National Laboratory's Radioactive Waste Management Complex. Contamination at the dig face would be controlled using soil fixing agents or other techniques. The enclosures would be held at a slight negative air pressure, and air from the enclosures would be exhausted through an air treatment system incorporating a minimum of a prefilter and one or more HEPA filters.

Enclosures can be conceptually configured to meet the specific situation at any MDA. Enclosure sizes and accessory equipment would be designed on an MDA-specific basis, considering the area to be covered, depth of contamination, types of hazards unearthed at the excavation, topography, other nearby structures, and costs. For some MDAs, a single large enclosure (to be moved as needed) may be cost-effective. For other MDAs, two or more enclosures may be cost-effective.

Fabric-covered domes have been used at LANL to support waste recovery efforts. As part of the LANL Transuranic Waste Inspectable Storage Project, drums of stacked transuranic waste that had been stored under a layer of crushed tuff at Area G were recovered under a fabric-covered dome constructed to meet Performance Category 2 wind-loading and seismic events. The dome was supplied with a ventilation system exhausting to a prefilter and a HEPA filter bank. A dome was not used, however, for subsequent retrievals of stored transuranic waste (LANL 2002d).

A decision about the use of an enclosure for removal of waste from an MDA would depend on the hazards represented by the waste. Like the other aspects of the contemplated removal, the design and use of the enclosure would be subject to review and approval by DOE and NMED. Optimum numbers, sizes, configurations, and relocation schedules would be determined as part of these reviews.

I.3.3.2.7 Material Disposal Area B Investigation and Remediation Program

LANL staff initially planned an investigation, remediation, and restoration program for MDA B that would excavate trenches perpendicular to the length of the MDA as well as numerous test pits. For this purpose, MDA B was divided into 10 study sections as summarized in **Figure I-24** (LANL 2005p). Current plans call for removal of all waste buried in MDA B as addressed in the October 2006 *Investigation/Remediation Work Plan for MDA B, Revision 1* (LANL 2006i). The volumes of waste estimated in this work plan are summarized in **Table I-62** (LANL 2006i). Total waste volumes from the work plan are bounded by those estimated for this SWEIS in Section I.3.3.2.4.2.

Achieving the principal objectives of the MDA B investigation and remediation program (see Section I.2.5.2.2) will require LANL to directly excavate into the MDA B disposal trenches, remove the historical content of MDA B, and remediate the site to residential cleanup levels for chemicals and screening action levels for radionuclides. Following excavation, LANL will prepare a sampling and analysis plan (if necessary) for NMED approval to define and nature and extent of any residual contamination at MDA B. This would be accomplished by sampling directly beneath former waste disposal trenches after the waste was removed, and possibly also by drilling subsurface boreholes (LANL 2006i).

Excavation will be performed inside an enclosure to provide site access control, help control offsite environmental impacts, reduce exposure to the public, and protect the excavation operations from environmental factors. The enclosure will provide access for equipment and waste containers that need to be moved in or out during the excavation. A fresh air circulation system will continuously replace air in the enclosure and eliminate combustion gases at a determined rate. Waste inspection and segregation will be performed inside a separate area of the excavation enclosure or within an additional enclosure (LANL 2006i).

Excavations will be completed using a hydraulic excavator to carefully expose and remove trench contents for inspection, identification, and removal. Excavator attachments such as a grappler or shears may be used. Only a small quantity of waste will be exposed and removed at any time (see Section I.5.12.1). If the proximity of waste trenches to DP Road on the north side precludes side sloping of the excavation, shoring or other methods may be used as needed to ensure excavation stability. Equipment, procedures, and administrative controls will be used to ensure safety and environmental protection during the investigation and remediation program. Several monitoring or remote sensing tools will be used for continuous monitoring for radiation, volatile organic compounds, gases, heat of trench contents, pyrophoric materials, or other hazardous conditions. If warranted, excavated wastes may be transferred to a new container or over-packed (LANL 2006i). For example, compressed gas cylinders, if found in the excavation, may be placed within overpacks designed to safely contain the contents of the cylinder if it leaks or fails during transport (IES 2005).

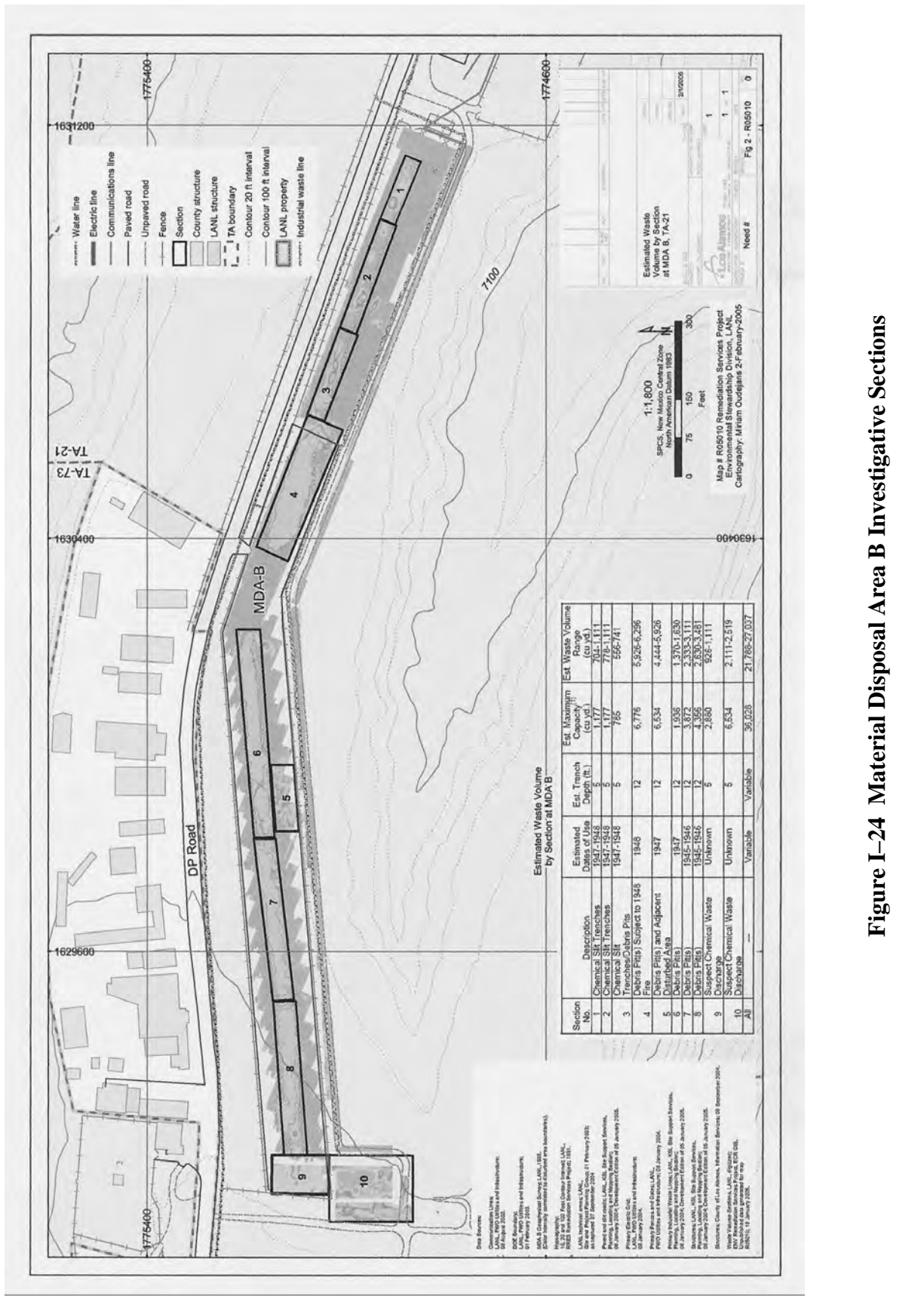


Figure I-24 Material Disposal Area B Investigative Sections

Table I-62 Summary of Investigation-Derived Waste from MDA B Removal

| <i>Waste Stream</i> | <i>Expected Waste Type</i> | <i>Estimated Volume (cubic yards)</i> |
|-------------------------------------|--|---------------------------------------|
| Drill cuttings | LLW, MLLW, hazardous, or solid/industrial waste | 60 |
| Spent personal protective equipment | LLW, MLLW, hazardous, or solid/industrial waste | 20 |
| Disposable sampling supplies | LLW, MLLW, hazardous, or solid/industrial waste | 20 |
| Decontamination fluids | LLW, MLLW, hazardous waste, or nonhazardous wastewater | 500 gallons |
| Material from trenches | Solid/industrial | 2,590 |
| | RCRA hazardous waste | 7,189 |
| | LLW | 10,800 |
| | MLLW | 4,028 |
| Trench spoils | Return to excavation site if nonhazardous and meets screening criteria; or LLW, MLLW, hazardous, or solid/industrial waste | 14,000 |

LLW = low-level radioactive waste, MLLW = mixed low-level radioactive waste, RCRA = Resource Conservation and Recovery Act.

Note: To convert cubic yards to cubic meters, multiply by 0.76456; from gallons to liters, multiply by 764.54.

Source: LANL 2006i.

Removal operations would include verification sampling; implementation of stabilization and surface water diversion measures; implementation of final restoration measures, including the placement and compaction of backfill; placement of a topsoil and native seed mix; and placement of additional barriers, roads, and paths as needed. Volumes of backfill and other bulk materials (and associated shipments) needed for removal operations are bounded by the analysis in Section I.3.3.2.4.2.

The investigation and remediation program would be integrated with other DD&D and PRS remediation activities at TA-21. Preliminary work would include similar operational elements as those described in Section I.3.3.2.4.1, including (LANL 2006f):

- Clearing and grubbing of vegetative material, debris, and obstructions;
- Installation of new fencing and removal of old fencing;
- Preparation of equipment and material staging areas;
- Modification of existing haul and access roads;
- Construction of a decontamination area;
- Installation of administrative facilities;
- Installation of run-on diversion structures to minimize stormwater impacts to the site and prevent migration of site contaminants;
- Completion of pre-fieldwork surveys, including land surveys, radiological surveys, and biological surveys;
- Collection of supplemental background samples for comparison of underlying tuff contaminant concentrations;

- Installation of area and perimeter monitoring systems, alarms, and communication equipment; and
- Execution of mockup drills and emergency response drills with MDA B site personnel.

A haul road has been created on the southern side of MDA B to divert operations traffic from the DP Road business area. Power will be needed to provide utility power for the enclosure, emergency backup generators, and health-and-safety trailers along that area (LANL 2006i).

It is expected that several temporary support capabilities will be needed for the investigation and remediation program. Support capabilities may include those for definitive identification of waste contents, sorting, temporary storage of waste and excavation spoil, project management, vehicle decontamination, waste processing or analysis, or other needs. It is expected that none of these temporary capabilities would intrude on habitat or buffer areas of protected wildlife. The capabilities may be located partly within the excavation closure and partly or wholly at separate temporary facilities such as those conceptually described below (LANL 2006a). Other permutations of these capabilities may be implemented as needed.

The *Definitive Identification Facility (DIF)* and storage area would encompass an area of a few acres. This storage area would be enclosed within chain-link fencing with a central temporary “Sprung” type dome enclosure as the major feature. The dome would enclose several other temporary buildings, such as a Permacon®-type building⁶⁸ that will house the DIF itself. Pre-DIF staging areas within the DIF storage area would store preliminarily hazard-categorized materials awaiting sampling or repackaging by DIF personnel. Post-DIF staging areas would temporarily store materials until verified analytical results determine waste disposition. In all staging areas, hazardous materials would be segregated according to known incompatibilities (for example, oxidizers, flammables, explosives). The DIF would be used to inspect and evaluate containers to determine their contents. Activities could range from removing a “bung” from a drum to sample its contents to “hot-tapping” compressed gas cylinders, which requires drilling into the sides of the containers. Depending upon regulatory controls, gases within some cylinders may be released to the environment (for example, hydrogen), whereas other gases may need treatment or transfer to another container. Exhaust air from the DIF, along with its enclosing dome would be HEPA-filtered and passed through an activated carbon absorption system. Fire protection systems would be used as required to reduce or mitigate accidental releases of hazardous materials to the environment.

The *Waste Processing Facility*, if constructed, would support all MDA and DD&D activities on DP Mesa. This facility would be a chain-link enclosed “yard” or laydown area for the accumulation of waste materials prior to shipment offsite. Some temporary buildings would house administrative activities. Various other structures may be necessary to store RCRA and radioactive materials before shipment. The Waste Processing Facility would be located at the end of DP East and comprise an area of less than 10 acres (4 hectares) of previously disturbed land. The facility would be used to package or repackage waste materials. The Waste Processing Facility would require areas for truck parking, turnaround, and loading by use of cranes, boomtrucks, forklifts, or other suitable heavy equipment. Incompatible materials would be segregated as required and stipulated by regulation. This facility would comply with all

⁶⁸ A Permacon® unit is a type of modular containment system (NFS RPS 2005).

RCRA regulations as it will function as a treatment, storage, or disposal facility. The Waste Processing Facility would likely include a truck decontamination pad along with a hazardous materials screening area for screening prior to offsite transport. Radioactive materials would be removed as required and shipped to on- or offsite locations for disposal. Roads would be improved or constructed to allow for the additional truck traffic. If the Waste Processing Facility is not constructed, waste processing and packaging would take place within the MDA B area of concern. After waste processing and manifesting, filled waste containers may be staged at other locations within the TA-21 boundary prior to transport and disposal (LANL 2006a).

DP Mesa Field Office and Laboratory Facilities. The facilities would comprise several transportable buildings housing analytical capabilities and offices to support MDA investigation and remediation and TA-21 DD&D activities. It is likely that at least three and maybe four transportable buildings would be required to provide the analytical chemistry capability for organic, inorganic, and radioactive material analysis. A fifth building may be required for administrative activities. The buildings and associated parking areas would fit on less than 2 acres (0.8 hectare) of previously disturbed lands. This facility would provide analytical data of sufficient quality to meet waste disposition manifesting and disposal requirements. It would include a treatment, storage, or disposal facility for RCRA waste accumulation.

Office trailers would be needed to support subcontractor and LANL administration. The area selected would require access using roads that would allow staff to reach work areas without crossing potentially controlled work areas. Extension of utilities from the existing utility grid would be required. To the extent practicable, a centralized area would be developed to minimize support utility requirements. The area of disturbance for administrative support would be limited to less than 2 acres (0.8 hectare).

Spoil Staging Areas. It is expected that clean and suspected-clean soils and construction debris staging areas would be placed as necessary at several locations around the DP Mesa. This would generally take place in locations near the point of their generation or intended use. These spoil piles would be protected from erosion or airborne dispersion by keeping them wet or covered as necessary. Appropriate runoff controls would be implemented. These could total many acres in size and would be located in previously disturbed areas when possible, but may require additional land at the east end of DP Mesa.

The total affected area from TA-21 DD&D and MDA remediation is expected to involve about 80 acres (32 hectares) of previously disturbed area and up to 30 acres (12 hectares) of undisturbed mesa top. Another 20 acres (8.1 hectares) of previously undisturbed canyon wall or bottom may also be partially disturbed (LANL 2006a).

I.3.3.2.8 Characterization and Treatment Capacity for Waste from Material Disposal Area Removal

If large-scale removal of waste from the MDAs is required, LANL capacity to characterize and repackage waste may be insufficient. One option to address this problem would be to construct a dedicated facility for waste separation, characterization, treatment, packaging, and staging for shipment. The size, cost, and environmental impacts associated with such a facility would depend on the quantities and characteristics (e.g., radioactive material content) of the exhumed

waste, which would depend on remediation decisions to be made in the future. A second option would be to site a number of smaller facilities at strategic LANL locations providing specific services similar to those contemplated for the MDA B investigation and remediation program (see Section I.3.3.2.7). This option could be combined as needed with an upgrade and expansion of existing waste management capacity in TA-54 or other technical areas.

A facility for processing exhumed transuranic waste was considered as part of an early LANL study addressing options for future disposition of buried waste in LANL MDAs A, B, C, G, T, and V (LANL 1981). The facility envisioned in this study would cover 40,550 square feet (3,765 square meters), with an additional 17,570 square feet (1,630 square meters) dedicated to support areas. The envisioned facility would be capable of accommodating remote-handled waste. Its design throughput would be 1 million cubic feet (28,320 cubic meters) of waste over 15 years (1,900 cubic meters per year) (LANL 1981). A facility for treatment of contact handled waste exhumed from Idaho National Laboratory disposal facilities has also been envisioned (INEEL 2002a). Waste would be transferred to the facility from a lag storage area covering 70,000 square feet (6,500 square meters) and capable of storing 6,400 cubic yards (4,900 cubic meters) of waste. Waste introduced into the treatment facility would be handled remotely using manipulators, conveyors, and gloveboxes. The two-story facility was projected to address 18,800 cubic yards (14,400 cubic meters) of waste per year and would have a surface area of 130,000 square feet (12,100 square meters) (INEEL 2002a).

Assuming extensive exhumation, annual waste generation rates from exhuming the LANL MDAs could be on the order of a hundred thousand cubic meters of low-activity low level radioactive waste, several thousand cubic meters of alpha-contaminated low-level radioactive waste, a few hundred cubic meters of high-activity low-level radioactive waste, and up to a few thousand cubic meters of transuranic waste. A facility receiving such a volume of waste could cover a few hundred thousand square feet. Assuming that funding was approved, several years may be required to design the facility and additional years to construct and test.

The second option would be to develop several facilities for waste handling at appropriate LANL locations as needed consistent with future decisions about MDA remediation. The facilities would be temporary, using modular equipment as available and appropriate, and could be moved to new locations consistent with remediation schedules. Similar to those described in Section I.3.3.2.7, facilities could include capacity for safety inspections of removed containers, waste processing and storage, radioactive and chemical analyses, and other support services. Facilities would be transportable or consist of modular glovebox or similar systems covered by domed enclosures. Shielded, remotely operated systems may be needed for processing some wastes. The designs of the facilities and their capabilities would depend on the characteristics of the wastes to be addressed, which would be different for different MDAs, and on the acceptance criteria for the treatment or disposal facilities receiving the wastes.

This option could be combined with the expanded use of existing LANL waste management capacity. Existing LANL capabilities for management of waste in TA-54 are described in Section H.3 of Appendix H, along with the environmental impacts of alternatives for relocation, replacement, or augmentation of this capacity. As needed, additional, augmented, or mobile waste management equipment or facilities could be developed at LANL similar to those

described in Section H.3.2.2. Use of existing LANL capabilities for remotely handling radioactive material could be also considered.

Although several such facilities may be required, depending on future remediation decisions, the impacts of siting and operating the facilities would be temporary.

I.3.4 Remediation of PRSs other than Material Disposal Areas

In addition to the MDAs addressed in Section I.3.3, numerous PRSs such as firing sites, outfalls, or areas of contaminated soil or sediment must be addressed. The volumes of wastes that may be generation from remediating these PRSs are uncertain, as is the timing for waste generation.

Section I.3.4.1 reviews possible treatment technologies. Section I.3.4.2 characterizes waste generated from remediation of representative PRSs. For the Capping and Removal Options, estimates from Section I.3.4.2 were added to projections of wastes from the No Action Option to address the PRSs that may be remediated through FY 2016 (see Section I.3.4.3).

I.3.4.1 Possible Treatment Technologies

Numerous treatment technologies could be used, depending on the contaminant and the contaminated media. As observed in the Federal Remediation Technologies Roundtable's Screening Matrix and Reference Guide, the three primary strategies that may be used separately or in conjunction to remediate most sites are destruction or alteration of contaminants, extraction or separation of contaminants from environmental media, and immobilization of contaminants. Treatment technologies capable of contaminant destruction by altering their chemical structure include thermal, biological, and chemical treatment methods applied either in or ex situ to contaminated media. Treatment technologies commonly used for extraction and separation of contaminants from environmental media include soil treatment by thermal desorption, soil washing, solvent extraction, and groundwater treatment using phase separation, carbon absorption, air stripping, ion exchange, or some combination of technologies. Immobilization technologies include stabilization, solidification, and containment technologies such as disposal in a landfill or construction of slurry walls. Because generally no single technology can remediate an entire site, several treatment technologies may be combined at a single site to form a treatment train. As noted, many treatment technologies require removal of the contaminated media, which, after treatment, may be returned or disposed of as waste. Descriptions of treatment technologies are provided in **Table I-63** (FRTR 2005). Other sources of information about treatment technologies include the Interstate Technology and Regulatory Council and, for groundwater contamination, the Ground-Water Remediation Technologies Analysis Center (GWRTAC 2005).

Treatment technologies used either individually or in combination at any PRS would be applied as needed and as approved by NMED. More complex and involved remedies might include requirements for staging areas and moderate augmentation of infrastructure (such as plumbing for extracted water or other wastes) to support the operational aspects of the remedy. If large volumes of wastewater are generated, there could be an increase in truck traffic to transport the wastewater to (generally onsite) treatment facilities.

Table I-63 Treatment Group Examples

| <i>Treatment Groups</i> | <i>Comments</i> |
|---|--|
| Soil, Sediment, and Sludge | |
| In situ biological treatment | Technologies include bioventing, enhanced biodegradation, and phytoremediation. Bioremediation technologies have been used to remediate soils, sludges, and groundwater contaminated by petroleum hydrocarbons, solvents, pesticides, wood preservatives, and other organic chemicals. |
| In situ physical/chemical treatment | Uses the physical properties of the contaminants or contaminated medium to chemically convert, separate, or contain the contamination. Treatment technologies include electrokinetic separation, fracturing, soil flushing, soil vapor extraction, and solidification/stabilization. |
| In situ thermal treatment | Thermally enhanced soil vapor extraction uses temperature to increase the volatility of soil contaminants. In situ vitrification uses heat to melt soil, destroying some organic compounds and encapsulating inorganics. |
| Ex situ biological treatment (assuming excavation) | Technologies include biopiles, composting, landfarming, and slurry-phase biological treatment. |
| Ex situ physical/chemical treatment (assuming excavation) | Technologies include chemical extraction, chemical reduction/oxidation, dehalogenation, separation, soil washing, and solidification/stabilization. |
| Ex situ thermal treatment (assuming excavation) | Technologies include hot-gas decontamination, incineration, open burn/open detonation, pyrolysis, and thermal desorption. |
| Containment | Containment includes capping of landfills or contaminated areas. |
| Other treatment processes | Other technologies include excavation, retrieval, and on- and offsite disposal. |
| Groundwater, Surface Water, and Leachate | |
| In situ biological treatment | Technologies include enhanced biodegradation (nitrate and oxygen enhancement with either air sparging or hydrogen peroxide), natural attenuation, and phytoremediation of organics. |
| In situ physical/chemical treatment | Technologies include air sparging, bioslurping, directional wells, dual-phase extraction, thermal treatment, hydrofracturing, in-well air stripping, and passive/reactive treatment walls. |
| Ex situ biological treatment (assuming pumping) | Contaminated groundwater, surface water, and leachate may be pumped from its location and treated. Treated water may be returned or disposed of as waste. Treatment technologies include bioreactors and constructed wetlands. |
| Ex situ physical/chemical treatment (assuming pumping) | Contaminated groundwater, surface water, and leachate may be pumped from its location and treated. Treated water may be returned or disposed of as waste. Biological treatment technologies include adsorption/absorption, advanced oxidation processes, air stripping, granulated activated carbon/liquid-phase carbon adsorption, groundwater pumping, ion exchange, precipitation/coagulation/flocculation, separation, and sprinkler irrigation. |
| Containment | Containment technologies include physical/biological barriers and deep-well injection. |
| Air Emissions/Offgas Treatment | |
| Air emissions/offgas treatment | Several technologies have been applied for removal of volatile organic compounds from offgas streams, including biofiltration, high-energy destruction, membrane separation, nonthermal plasma, oxidation, scrubbers, and vapor-phase carbon adsorption. |

Source: FRTR 2005.

I.3.4.2 Remediation of Representative PRSs

Firing Site E-F. This firing site in TA-15 is described in Section I.2.3.1 and contains scattered surface contamination plus small piles of debris. Surveys showed that most uranium was concentrated within the top 10 to 12 inches (25 to 30 centimeters) of soil and that uranium

concentrations dropped by a factor of 23 within 1,000 feet (300 meters) of the firing point. Two piles of debris were each 8 feet (2.4 meters) in diameter and 2 feet (0.6 meters) high.⁶⁹

Waste volumes for this appendix were estimated by assuming that material would be removed from an area having a radius of 1,000 feet (300 meters) to an average depth of 1 inch (2.5 centimeters) and adding the waste from the two debris piles. This results in 9,700 cubic yards (7,420 cubic meters) of waste. Similar to the waste distribution for removal of MDA Z (see Section I.3.3.2.4.3), this waste was assumed to be 40 percent solid waste, 15 percent chemical waste, 40 percent low-activity low-level radioactive waste, and 5 percent mixed low-activity low-level radioactive waste.

Firing Site R-44. This firing site in TA-15 is described in Section I.2.3.2, and contains scattered surface contamination plus some small debris piles. After the Cerro Grande fire, much exposed debris was recovered and disposed.

Waste volumes for this appendix were estimated by assuming that material would be removed from an area having a radius of about 500 feet (152 meters) to an average depth of 1 inch (2.5 centimeters), or 2,420 cubic yards (1,850 cubic meters) of waste. Similar to the waste distribution for removal of MDA Z (see Section I.3.3.2.4.3), this waste was assumed to be 40 percent solid waste, 15 percent chemical waste, 40 percent low-activity low-level radioactive waste, and 5 percent mixed low-specific-activity low-level radioactive waste.

260 Outfall. SWMU 16-21(c)-99 is described in Section I.2.7.5. It is an inactive outfall from Building 260 in TA-16 where machine turnings and high explosive washwater were discharged. An interim measure has been performed to remove contaminated soil. Three areas of contamination remain: (1) the outfall source area (excluding the settling pond and surge beds); (2) the outfall settling pond and surge beds; and (3) canyon springs and alluvium. After completing Phase I, Phase II, and Phase III RFIs, and the interim measure, a corrective measures study has been issued establishing corrective measure alternatives (LANL 2003I). The corrective measure alternatives are listed in **Table I-64** (LANL 2003I).

The final remedy for the 260 Outfall was selected by NMED on October 13, 2006. The selected remedy is a combination of alternatives from the corrective measures study:

- Soil removal and offsite treatment and disposal;
- Pressure grouting the surge beds and extending the existing cap; and
- Installing permeable reactive barriers and stormwater filters to treat sediment, surface water, and alluvial groundwater.

⁶⁹ *Firing Site E-F was used more extensively than Firing Site R-44. Some of the debris currently deposited on Firing Site R-44 originated from firing operations at Firing Site E-F.*

Table I-64 Alternative Corrective Measures for the 260 Outfall

| <i>Site Area</i> | <i>Alternative Number^a</i> | <i>Description</i> | <i>Estimated Waste Generation</i> |
|---|---------------------------------------|--|---|
| Outfall source area (excluding settling pond) | I.1 | Soil removal and offsite treatment and disposal | 131 cubic yards of solid waste |
| Outfall source area, settling pond, and 17-foot surge bed | II.1 | Excavation and offsite disposal of the 17-foot surge bed and replacement/maintenance of the existing cap | 52 cubic yards of solid waste |
| | II.2 | In situ grouting of the 17-foot surge bed and maintenance of the existing cap | |
| | II.3 | Maintenance of existing cap and no action for the surge beds | |
| Canyon springs and alluvial system | III.1 | Sediment excavation and offsite disposal, with stormwater filters for springs | 13,080 cubic yards of solid waste and 13,080 cubic yards of hazardous waste |
| | III.2 | Natural flushing of sediments coupled with permeable reactive barrier (zero valent iron or granulated activated carbon and calcium sulfate) alluvial groundwater treatment and stormwater filter treatment for springs | |
| | III.3 | Natural/induced flushing of sediments and recovery of spring and groundwater (by interceptor trenches) and treatment in a central treatment system | |

^a NMED selected a final remedy for the 260 Outfall in October 13, 2006. The selected remedy is a combination of the alternatives proposed by LANL staff.

Note: To convert cubic yards to cubic meters, multiply by 0.76456; from feet to meters, multiply by 0.3098.

Source: LANL 2003i.

TA-21 Outfall. This SWMU (21-011(k)) was an inactive NPDES-permitted outfall for liquid waste from former wastewater treatment plants at DP West (see Section I.2.7.6). A voluntary corrective measure was planned to excavate and dispose of contaminated wastes as low-level radioactive waste, excavate and solidify tuff and sediment from hot spots, and place the solidified material in a stabilization cell to be dug near the center of the SWMU (LANL 2002f). The voluntary corrective measure was projected to generate 25 cubic yards (19 cubic meters) of solid waste and 65 cubic yards (50 cubic meters) of low activity low-level radioactive waste. Solidification and onsite stabilization of tuff and sediment were projected to involve 78 cubic yards (60 cubic meters) of material (LANL 2002f). The voluntary corrective measure was subsequently revised and material projected to be solidified onsite was removed. Removal occurred in 2003 (LANL 2003i).

SWMU 73-002 Incinerator Ash Pile. Remediation of the ash pile is complete, including removal of ash and debris waste (see Section I.2.7.11). It was estimated that the pile contained roughly 4,500 cubic yards (3,340 cubic meters) of waste (LANL 2005e). The Investigation Report for Consolidated Unit 73-002-99 and Corrective Action of Solid Waste Management Unit 73-002, at Technical Area 73 was submitted to and approved by NMED (LANL 2006a).

Canyons. Investigations and remediation within LANL canyons are expected to generate about 10 cubic yards (7.6 cubic meters) of solid low-level radioactive waste, 24 cubic yards (18 cubic meters) of mixed low-level radioactive waste, and 9,900 gallons (37,500 liters) of liquid radioactive waste (LANL 2006a).

Security Perimeter Road. Development of a security perimeter road in TA-3 was one of the FY 2005 facility integration projects at LANL that affected existing PRSs; in this case, an electrical equipment storage area (SWMU 61-002), two storage areas in TA-3 (AOC 3-001(i)), and a asphalt landfill (SWMU 03-029) (LANL 2005l). Generation of waste from this project was estimated as about 3,000 cubic yards (2,300 cubic meters) of solid waste and 500 cubic yards (380 cubic meters) of low-level radioactive waste (LANL 2006a). An accelerated corrective action completion report was submitted to NMED on December 15, 2005. Investigation and remediation work included the decontamination and decommissioning of the TA-3 Radio Shop, allowing access to residual petroleum hydrocarbon contamination found while remediating SWMU 61-002 (LANL 2006h). The Security Perimeter Road accelerated corrective action has been completed.

I.3.4.3 Waste Generation Estimates

Compliance with the Consent Order will cause remediation of a large number of PRSs from FY 2007 through FY 2016. There may be several options for remediation, including removing, treating, or stabilizing contamination at a site or controlling exposure to the contamination so risks posed are acceptable. It was assumed that remediation would occur annually, involve activities similar to those described in Section I.3.4.1, and generate similar types of waste as those summarized in Section I.3.4.2. As shown in **Table I-65**, an annual average waste generation rate of 5,200 cubic yards (4,000 cubic meters) was projected. This waste was distributed among different waste types based on consideration of the waste estimates discussed in Section I.3.4.2.

Table I-65 Additional Waste Generation from Remediating Potential Release Sites

| <i>Parameter</i> | <i>Solid Waste</i> | <i>Chemical Waste^a</i> | <i>Low-Activity Low-Level Radioactive Waste</i> | <i>Mixed Low-Activity Low-Level Radioactive Waste</i> | <i>Total Annual Waste</i> |
|---|--------------------|-----------------------------------|---|---|---------------------------|
| Annual Volume ^b (cubic yards) | 2,900 | 1,700 | 630 | 52 | 5,200 |
| Shipments | 220 | 140 | 44 | 4 | 410 |

^a The chemical waste category includes wastes regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

^b In situ volumes. As-shipped volumes would be larger because of swell of excavated material and packaging inefficiencies. Note: To convert cubic yards to cubic meters, multiply by 0.76456. Because numbers have been rounded, the sums may not equal the indicated totals.

I.3.5 Waste Transportation and Disposal Assumptions

After removal of waste from the ground, and following classification and sorting, waste must be placed within containers, treated if necessary, and disposed of. Because so much of the waste that would be generated from MDA exhumation and PRS remediation will be soil and debris, it was assumed that material would swell by about 20 percent following removal. That is, removed waste placed into containers was assumed to be 20 percent larger than the in situ volume.

Solid waste was assumed to be sent to a landfill within New Mexico, with a round-trip distance of 260 miles (418 kilometers). Chemical waste would be sent for treatment before disposal. Several treatment sites could be used depending on the hazardous constituents to be treated. A

typical site having a roundtrip distance of 332 miles (534 kilometers) was assumed. It was assumed that all contact-handled and remote-handled transuranic wastes would be sent to WIPP.

Low-level radioactive waste could be disposed of onsite or sent to another site. (Onsite disposal capacity for mixed low-level radioactive waste is not currently available.) It was assumed that low-level and mixed low-level radioactive wastes could be sent to any of a number of commercial or DOE sites for treatment or disposal. Two typical sites—one commercial and one DOE—were assumed, having round-trip distances of 1,378 miles (2,153 kilometers) and 1,550 miles (2,500 kilometers), respectively. It was assumed that low-level and mixed low-level radioactive wastes would be optionally all disposed of onsite (assuming an average one-way travel distance of 5.6 miles [9 kilometers]; all shipped to a different DOE site; or shipped partly to a DOE site and partly to a commercial site, consistent with waste acceptance criteria for the commercial site. (It was assumed that all low-level and mixed low-level radioactive wastes could be shipped to the DOE site, but only low-activity and mixed low-activity low-level radioactive waste could be shipped to the commercial site.)

Container and shipping assumptions are listed in **Table I-66** and summarized below.

An 80 percent packing efficiency (percent of container filled with waste) was assumed for solid waste because of short travel distances, relatively low transport and disposal costs, and to keep within assumed weight limit. A 90 percent packing efficiency was assumed for other nonliquid wastes because of much larger travel distances and transport, treatment, and disposal costs. An 80 percent packing efficiency was assumed for liquid wastes because it is expected that only small volumes would be generated from most remediated sites.

A maximum shipment weight of 20 tons (18 metric tons) for chemical, solid, and low-level radioactive waste, was estimated, assuming a waste density of up to 1.08 tons per cubic yard (1.28 metric tons per cubic meter), typical for dirt and rock, assuming 20 percent swell. Low-activity low-level radioactive waste was assumed to be shipped as low-specific-activity material, pursuant to U.S. Department of Transportation requirements, and placed within soft liners to be transported within Intermodals at two soft liners per Intermodal. Mixed low-activity and alpha-contaminated low-level radioactive waste were assumed to be transported in B-25 boxes. This waste may require treatment before disposal. Drums were assumed for all remote-handled transuranic waste.

For contact-handled transuranic waste, fourteen 55-gallon (0.21-cubic-meter) drums were assumed per TRUPACT-II (transuranic waste package transporter II) outer packaging (WIPP 2005) and three TRUPACT-II packages per shipment. Three TRUPACT-II outer packaging were assumed per contact-handled transuranic waste shipment. A shipped waste density of 1.08 tons per cubic yard results in contact-handled transuranic waste shipments comparable to maximum allowable shipment weights for TRUPACT-II packages (DOE 2004c). Remote-handled transuranic waste was assumed to be shipped in RH-72B casks at three drums per cask (Jensen, Devarakonda, and Biedscheid 2001).

Table I-66 Container and Shipment Assumptions

| <i>Waste</i> | <i>Container</i> | <i>Container Volume (cubic feet and cubic meters)</i> | <i>Packing Efficiency (percent)</i> | <i>Number of Containers per Truck</i> | <i>Volume per Shipment^a (cubic yards)</i> |
|---|----------------------------|---|---|---|--|
| Nonliquid Waste | | | | | |
| Solid | 20-cubic-yard rolloff | 540/15.3 | 80 | 1 | 16 |
| Chemical | 55-gallon drum | 7.35/0.21 | 90 | 60 | 14 |
| Low-level radioactive waste – low activity | Soft liners/ Intermodal | 260/7.3 | 90 | 2 | 17 |
| Low-level radioactive waste – alpha | B-25 box | 90/2.55 | 90 | 5 | 15 |
| Low-level radioactive waste – remote handled ^b | 55-gallon drum | 7.35/0.21 | 90 | 10 | 2.5 |
| Mixed low-level radioactive waste – low activity | B-25 box | 90/2.55 | 90 | 5 | 15 |
| Mixed low-level radioactive waste – alpha | B-25 box | 90/2.55 | 90 | 5 | 15 |
| Mixed low-level radioactive waste – remote handled ^b | 55-gallon drum | 7.35/0.21 | 90 | 10 | 2.5 |
| Contact-handled transuranic waste ^c | 55-gallon drum | 7.35/0.21 | 90 | 42 | 10 |
| Remote-handled transuranic waste ^d | 55-gallon drum | 7.35/0.21 | 90 | 3 | 0.8 |
| Mixed contact-handled transuranic waste ^c | 55-gallon drum | 7.35/0.21 | 90 | 42 | 10 |
| Mixed remote-handled transuranic waste ^d | 55-gallon drum | 7.35/0.21 | 90 | 3 | 0.8 |
| Liquid Waste | | | | | |
| Industrial ^e | 500-gallon tanks | 67/1.9 | 80 | 2 | 3.9 |
| Hazardous ^e | 500-gallon tanks | 67/1.9 | 80 | 2 | 3.9 |
| Low-level liquid radioactive waste ^e | 500-gallon tanks | 67/1.9 | 80 | 2 | 3.9 |
| Mixed low-level liquid radioactive waste ^e | 500-gallon tanks | 67/1.9 | 80 | 2 | 3.9 |

^a This assumed volume is applied after an in situ volume increase of 20 percent due to swell of removed material.

^b The quantity of waste that can be delivered in any single shipment will depend on container surface radiation levels and the design and availability of transportation packaging. Duratek cask capacity ranges from 1 to 21 drums (Duratek 2005). A shielded shipping box can contain up to 27 drums. Assumed 10 drums per shipment.

^c Assumed use of TRUPACT II [transuranic waste package transporter II] packaging.

^d Assumed use of RH-72B transportation cask.

^e Assumed liquids are treated at LANL.

Note: To convert cubic yards to cubic meters, multiply by 0.76456; cubic meters to cubic yards, multiply by 1.308; gallons to liters, multiply by 3.7854.

For remote-handled low-level and mixed low-level radioactive waste, a relatively large number of drums per cask (10) were assumed. It was assumed that most remote-handled wastes would not have surface exposure rates significantly above 200 millirem per hour. Duratek casks range in capacity from 1 to 21 drums, although about 40 percent of available casks can hold up to 14 (Duratek 2005). (The calculated weight [3.2 tons] is within the payload limits of typical casks.) The average number of drums per shipment, however, would be smaller than 14 because of operational, cost, and scheduling considerations. (Only a small amount of remote-handled low-level radioactive waste would be exhumed at any time, and it would be too expensive to rent a cask for long periods of time waiting for it to be completely filled before shipment.)

All liquids were assumed to be treated at LANL. Wastes requiring shipment offsite after this treatment should be comparatively small in volume.

It was assumed that once exhumed, solid, chemical, and low-activity and alpha-contaminated low-level and mixed low-level radioactive wastes would be loaded directly into final shipping containers and then loaded onto trucks for transport to a treatment or disposal facility. It was assumed that transuranic and remote-handled low-level radioactive wastes would require additional processing or repackaging before shipment. For example, transuranic wastes must be placed in package configurations compatible with the WIPP waste acceptance criteria. For processing operations, labor hours per unit volume of waste were assumed based on an analysis for the LANL Decontamination and Volume Reduction System (DOE 1999b). Worker radiation doses for waste processing were assumed based on LANL worker radiation experience for 2004 and 2005. Person-hours for loading containers into trucks were assumed based on a review of other analyses (INEEL 2002d, Wolf 2002), and radiation doses were assessed using the RADTRAN, Version 5, computer code (Weiner et al. 2006) based on assumed container surface radiation rates that were compatible with assumptions for waste transportation (see below). It was assumed that, depending on the type of waste, loading would be accomplished using crews of from 3 to 5 persons having average distances ranging from 3.3 to 16 feet (1 to 5 meters) from the waste package. Analytical support activities were also addressed.

Unit (per shipment) dose and risk estimates were then developed for shipments of waste to treatment and disposal facilities. The estimates were performed using the RADTRAN, Version 5, computer code (Weiner et al. 2006) in accordance with the assumptions in Table I-66. Incident-free radiation exposures to shipment crews (two crewmembers per shipment) were estimated assuming that exposure rates at shipment packaging surfaces were at regulatory limits. Population doses were calculated using comparable assumptions. Crew and population risks were calculated assuming a latent cancer fatality (LCF) rate of 0.0006 per person-rem of exposure.

Possible transportation accidents involving radioactive material were assessed assuming a source for different waste types developed from radioactive inventories within MDA G, the LANL MDA for which information is most complete. LCFs for a possible transportation accident were determined by first calculating the dose from an accident to an MEI, and then multiplying this dose by the probability of an accident and by an LCF rate of 0.0006 per person-rem of exposure. Nonradiological accidents (mechanical injury) were estimated using information about accident frequencies (see Appendix K, Section K.6.2, Accident Rates). For shipments of solid waste, a fatality accident rate for New Mexico was used (1.18 fatalities per 100 million kilometers traveled). For shipments of chemical waste, a fatality accident rate for an urban population zone was used (2.32 fatalities per 100 million kilometers traveled).

Transportation dose and risk assessment results are presented on a per shipment basis in **Table I-67**.

I.3.6 Waste, Materials, Shipment, and Personnel Projections Under Options

I.3.6.1 Waste Generation

No Action Option. **Table I-68** summarizes annual waste projections under the No Action Option starting in FY 2007 and continuing through FY 2016. These projections reflect LANL staff estimates of wastes from environmental investigation and remediation that were made before the March 1, 2005 issuance of the Consent Order. The volumes in this table essentially

represent in situ volumes of contaminated material. Because much material may consist of contaminated soil or debris, as-shipped volumes were assumed to be 20 percent larger to account for material swell following removal from the ground.

Table I-67 Transportation Dose and Risk Assessment Results ^a

| Typical Destination | Waste | Round-Trip Distance (kilometers) | Crew Dose and Risk | | Population Dose and Risk | | Accidents | |
|---------------------|------------------------------------|----------------------------------|--------------------|----------------------|--------------------------|----------------------|-----------------------------|------------------------------|
| | | | Person-Rem | LCF | Person-Rem | LCF | Radiological (LCF Fatality) | Nonradiological (fatalities) |
| DOE Site | Low-specific activity ^b | 2,500 | 0.0014 | 8.2×10^{-7} | 0.00027 | 1.6×10^{-7} | 1.3×10^{-8} | 0.000025 |
| DOE Site | LLW and MLLW ^c | 2,500 | 0.012 | 7.5×10^{-6} | 0.0039 | 2.4×10^{-6} | 1.7×10^{-8} | 0.000025 |
| DOE Site | RH-LLW and MLLW ^d | 2,500 | 0.011 | 6.5×10^{-6} | 0.0020 | 1.2×10^{-6} | 3.3×10^{-13} | 0.000025 |
| Commercial Site | Low-specific activity ^b | 2,153 | 0.0012 | 7.1×10^{-7} | 0.00023 | 1.4×10^{-7} | 9.6×10^{-9} | 0.000021 |
| Commercial Site | LLW and MLLW ^c | 2,153 | 0.011 | 6.4×10^{-6} | 0.0033 | 2.0×10^{-6} | 1.4×10^{-8} | 0.000021 |
| WIPP | CH-TRU ^e | 1,210 | 0.023 | 0.000014 | 0.0073 | 4.4×10^{-6} | 3.3×10^{-11} | 0.000014 |
| WIPP | RH-TRU ^e | 1,210 | 0.035 | 0.000021 | 0.0092 | 5.5×10^{-6} | 7.7×10^{-13} | 0.000014 |

LCF = latent cancer fatality, LLW = low-level radioactive waste, MLLW = mixed low-level radioactive waste, RH = remote-handled, WIPP = Waste Isolation Pilot Plant, CH = contact-handled, TRU = transuranic waste.

^a Results are for one-way distances except for nonradiological accidents, which are for round trips.

^b Waste shipped in Intermodals.

^c Waste shipped in B-25 boxes.

^d Waste shipped in drums.

Note: To convert kilometers to miles, multiply by 0.6213. Numbers have been rounded.

Table I-68 Annual Waste Generation Rates for No Action Option (cubic yards)

| Waste | Fiscal Year 2007 | Fiscal Year 2008 | Fiscal Year 2009 | Fiscal Year 2010 | Fiscal Year 2011 | Fiscal Year 2012 |
|--|------------------|------------------|------------------|------------------|------------------|------------------|
| Chemical Waste ^a | 2,000 | 1,400 | 190 | – | 50 | 36 |
| Low-Level Radioactive Waste ^b | 990 | 3,600 | 4,200 | 31 | – | – |
| Mixed Low-Level Radioactive Waste ^b | 130 | 200 | 20 | – | 300 | 89 |
| Transuranic Waste ^c | 100 | 100 | – | – | – | – |
| Total | 3,200 | 5,300 | 4,400 | 31 | 350 | 130 |
| Waste | Fiscal Year 2013 | Fiscal Year 2014 | Fiscal Year 2015 | Fiscal Year 2016 | Total | – |
| Chemical Waste ^a | 36 | 36 | 36 | 36 | 3,800 | – |
| Low-Level Radioactive Waste ^b | – | – | – | – | 8,800 | – |
| Mixed Low-Level Radioactive Waste ^b | 89 | 89 | 89 | 89 | 1,100 | – |
| Transuranic Waste ^c | – | – | – | – | 210 | – |
| Total | 130 | 130 | 130 | 130 | 14,000 | – |

^a Assumed an average waste density of 1 gram per cubic centimeter. Assumed to include waste regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

^b Assumed to be low-activity and mixed low-activity low-level radioactive waste.

^c Includes mixed transuranic waste.

Note: To convert cubic yards to cubic meters, multiply by 0.76456. Because numbers have been rounded, the sums may not equal the indicated totals.

Capping Option. Environmental remediation continues as assumed for the No Action Option. In addition, all MDAs are stabilized in place through installation of final evapotranspiration covers. The General's Tanks within MDA A are stabilized using a grout mixture, and other PRSs are remediated. The wastes associated with these assumptions are listed in **Table I-69**. These wastes represent:

- Wastes generated as part of the No Action Option (Table I-68).
- Wastes associated with capping large MDAs according to the schedule in Table I-52.
- Wastes associated with capping the remaining MDAs, assuming that wastes from capping these MDAs are generated in equal annual volumes from FY 2007 through FY 2016.
- Additional wastes associated with remediating PRSs. (Wastes listed in Table I-65 are annually generated.)

Removal Option. Environmental remediation continues as assumed for the No Action Option. In addition, all MDAs are exhumed and other PRSs are remediated. The wastes associated with these assumptions are listed in **Table I-70**. These wastes represent:

- Wastes generated as part of the No Action Option (Table I-68).
- Wastes associated with removing large MDAs according to the schedule presented in Table I-61.
- Wastes associated with removing the remaining MDAs, assuming that wastes from removing these MDAs are generated in equal annual volumes from FY 2007 through FY 2016.
- Additional wastes associated with remediating PRSs. (Wastes listed in Table I-65 are annually generated.)

Removing the MDAs would generate a significant quantity of waste. The largest annual waste generation would occur during FY 2010.

I.3.6.2 Transportation and Disposal of Waste

Annual shipments under the No Action Option are listed in **Table I-71**. Peak shipments of waste would occur in FY 2008.

Table I-69 Capping Option Annual Waste Generation Rates^{a, b}

| Waste (cubic yards) | Fiscal Year | | | | | | | | | | Total |
|-----------------------------------|-------------|--------|--------|-------|--------|-------|-------|-------|-------|-------|--------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | |
| Solid waste | 4,300 | 4,300 | 4,400 | 5,300 | 5,800 | 4,300 | 4,800 | 4,300 | 4,800 | 4,500 | 47,000 |
| Chemical waste ^c | 4,100 | 3,500 | 2,300 | 2,100 | 2,200 | 2,100 | 2,100 | 2,100 | 2,100 | 2,100 | 25,000 |
| Low-level radioactive waste | 1,800 | 4,400 | 5,000 | 1,600 | 2,100 | 780 | 1,100 | 780 | 1,100 | 900 | 20,000 |
| Mixed low-level radioactive waste | 200 | 270 | 90 | 71 | 370 | 160 | 160 | 160 | 160 | 160 | 1,800 |
| Transuranic waste | 100 | 100 | – | 42 | 26 | – | – | – | – | – | 280 |
| Total | 10,000 | 13,000 | 12,000 | 9,200 | 11,000 | 7,400 | 8,200 | 7,400 | 8,200 | 7,700 | 93,000 |

^a In situ volumes. As-shipped volumes are assumed to be 20 percent larger to account for material swell following removal from the ground.

^b In addition, about 1,000 gallons of liquid low-level radioactive waste is projected per year from LANL's environmental restoration project, to be shipped to treatment facilities generally on the LANL site.

^c Includes wastes regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

Note: To convert cubic yards to cubic meters, multiply by 0.76456. Because numbers have been rounded, the sums may not equal the indicated totals.

Table I-70 Removal Option Annual Waste Generation Rates ^a

| Waste | Fiscal Year | | | | | | | | | | Total |
|--|-------------|--------|---------|---------|---------|---------|---------|---------|---------|--------|-----------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | |
| Nonliquid Waste (cubic yards) | | | | | | | | | | | |
| Solid waste | 9,200 | 14,000 | 25,000 | 21,000 | 9,700 | 9,400 | 9,400 | 9,400 | 9,400 | 9,200 | 130,000 |
| Chemical waste ^b | 4,600 | 5,900 | 10,000 | 9,100 | 3,600 | 2,700 | 3,200 | 3,400 | 2,900 | 2,700 | 49,000 |
| Low-level radioactive waste | 4,700 | 12,000 | 83,000 | 110,000 | 96,000 | 95,000 | 96,000 | 96,000 | 95,000 | 20,000 | 710,000 |
| Mixed low-level radioactive waste | 250 | 830 | 21,000 | 28,000 | 14,000 | 10,000 | 12,000 | 12,000 | 11,000 | 2,100 | 110,000 |
| Alpha low-level radioactive waste | – | 10,000 | 81,000 | 90,000 | 35,000 | 31,000 | 31,000 | 31,000 | 31,000 | 5,700 | 350,000 |
| Mixed alpha low-level radioactive waste | – | 3,300 | 23,000 | 23,000 | 4,300 | 3,500 | 3,500 | 3,500 | 3,500 | 630 | 68,000 |
| Remote-handled low-level radioactive waste | – | – | 120 | 180 | 180 | 180 | 180 | 180 | 180 | 33 | 1,200 |
| Mixed remote-handled low-level radioactive waste | – | – | 13 | 20 | 20 | 20 | 20 | 20 | 20 | 4 | 140 |
| Contact-handled transuranic waste | 100 | 450 | 4,700 | 5,700 | 1,700 | 920 | 2,800 | 3,800 | 1,900 | 170 | 22,000 |
| Remote-handled transuranic waste | – | – | 23 | 24 | 0.57 | 0.57 | 0.57 | 0.57 | 0.57 | 0.11 | 50 |
| Total nonliquid waste | 19,000 | 47,000 | 250,000 | 280,000 | 160,000 | 150,000 | 160,000 | 160,000 | 160,000 | 41,000 | 1,400,000 |
| Liquid Waste (gallons) | | | | | | | | | | | |
| Industrial liquid waste | 0 | 1,000 | 1,000 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 2,100 |
| Hazardous liquid waste | 21 | 1,100 | 3,300 | 3,300 | 2,500 | 21 | 21 | 21 | 21 | 21 | 10,000 |
| Low-level radioactive liquid waste | 1,100 | 1,300 | 1,300 | 1,100 | 1,100 | 1,100 | 1,100 | 1,100 | 1,100 | 1,100 | 11,000 |
| Mixed low-level radioactive liquid waste | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 200 |
| Total liquid waste ^c | 1,100 | 3,400 | 5,600 | 4,400 | 3,600 | 1,100 | 1,100 | 1,100 | 1,100 | 1,100 | 24,000 |

^a In situ volumes. As-shipped volumes are 20 percent larger to account for material swell following removal from the ground.

^b Includes wastes regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

Note: To convert cubic yards to cubic meters, multiply by 0.76456; gallons to liters, multiply by 3.785. Because numbers have been rounded, the sums may not equal the indicated totals.

Table I-71 No Action Option Annual Waste Shipments

| <i>Waste</i> | <i>Fiscal Year</i> | | | | | | | | | | <i>Total</i> |
|--|--------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|
| | <i>2007</i> | <i>2008</i> | <i>2009</i> | <i>2010</i> | <i>2011</i> | <i>2012</i> | <i>2013</i> | <i>2014</i> | <i>2015</i> | <i>2016</i> | |
| Chemical waste ^a | 160 | 120 | 16 | 0 | 4 | 3 | 3 | 3 | 3 | 3 | 310 |
| Low-level radioactive waste ^b | 70 | 260 | 290 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 620 |
| Mixed low-level radioactive waste ^b | 10 | 16 | 2 | 0 | 24 | 7 | 7 | 7 | 7 | 7 | 87 |
| Transuranic waste ^c | 12 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| Total | 250 | 400 | 310 | 2 | 28 | 10 | 10 | 10 | 10 | 10 | 1,000 |

^a Assuming an average waste density of 1 gram per cubic centimeter. Includes wastes regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

^b Assumed to be low-activity and mixed low-activity low-level radioactive waste.

^c Includes mixed transuranic waste.

Note: Because numbers have been rounded, the sums may not equal the indicated totals.

Annual shipments under the Capping Option are listed in **Table I-72**, while annual shipments under the Removal option are listed in **Table I-73**. Peak shipments under the Capping Option would occur during FY 2008, and under the Removal Option during FY 2010.

I.3.6.3 Cover Materials, Excavated Soil, and Materials Transport

No Action Option. Materials and requirements for transporting these materials would be comparable to those seen in past years at LANL.

Capping Option. Volumes of capping materials, assuming two thicknesses of final cover, are indicated in **Table I-74**, along with total truck shipments through FY 2016. Sources for this cover material would be borrow areas within LANL or its vicinity. In the table, the “tuff” designation refers to fill material such as crushed tuff. The “additional material” designation refers to topsoil, soil amendment, gravel, and similar materials.

Additional materials may include instrumentation for cover infiltration monitoring, cement grout for stabilizing the General’s Tanks in place, fencing, or other miscellaneous materials.

Removal Option. The process of exhuming the MDAs would cause movement of large quantities of uncontaminated soil. Soil removed from the vicinity of the MDAs would be stockpiled and returned to the excavations. Additional backfill would be needed to account for the removed waste, plus a layer of topsoil and materials intended to promote vegetative growth. Remaining disposal units at the existing Area G footprint following MDA G removal are assumed to be covered with either a thin or thick cap, as are small contaminated areas or landfills in TA-49.

Material volumes and shipments are summarized in **Table I-75**. The table includes volumes and shipments of bulk material for MDA removal, for capping the remaining disposal units in the existing Area G footprint following MDA G removal, and for capping small landfills and areas of contamination in TA-49 (see Tables I-50 and I-51). In most cases, distances of shipments of material that would be removed, stockpiled, and returned to the excavations would be very short. The additional fill and topsoil could come from borrow areas either on or in the vicinity of LANL.

Table I-72 Capping Option Annual Waste Shipments

| Waste ^a | Fiscal Year | | | | | | | | | | Total |
|-----------------------------------|--------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | |
| Solid waste | 330 | 330 | 340 | 410 | 450 | 330 | 360 | 330 | 360 | 340 | 3,600 |
| Chemical waste ^b | 340 | 290 | 190 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 2,100 |
| Low-level radioactive waste | 120 | 310 | 350 | 110 | 150 | 55 | 80 | 55 | 80 | 63 | 1,400 |
| Mixed low-level radioactive waste | 16 | 21 | 7 | 6 | 30 | 13 | 13 | 13 | 13 | 13 | 140 |
| Transuranic waste | 12 | 12 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 0 | 32 |
| Total | 820 | 970 | 890 | 710 | 810 | 580 | 640 | 580 | 640 | 600 | 7,200 |

^a In addition, roughly 1,000 gallons of low-level liquid radioactive waste is projected to be generated per year from LANL's environmental restoration project, to be shipped to treatment facilities on the LANL site. This would be accomplished using less than two full shipments.

^b Includes wastes regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

Note: Because numbers have been rounded, the sums may not equal the indicated totals.

Table I-73 Removal Option Annual Waste Shipments

| Waste | Fiscal Year | | | | | | | | | | Total |
|--|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | |
| Nonliquid Waste | | | | | | | | | | | |
| Solid waste | 700 | 1,100 | 1,900 | 1,600 | 740 | 720 | 720 | 720 | 720 | 700 | 9,700 |
| Chemical waste ^a | 380 | 490 | 870 | 760 | 300 | 220 | 270 | 290 | 240 | 220 | 4,000 |
| Low-level radioactive waste | 330 | 870 | 5,900 | 7,600 | 6,800 | 6,700 | 6,800 | 6,800 | 6,700 | 1,400 | 50,000 |
| Mixed low-level radioactive waste | 20 | 66 | 1,700 | 2,200 | 1,100 | 820 | 920 | 970 | 870 | 160 | 8,900 |
| Alpha low-level radioactive waste | – | 810 | 6,500 | 7,200 | 2,800 | 2,500 | 2,500 | 2,500 | 2,500 | 450 | 28,000 |
| Mixed alpha low-level radioactive waste | – | 260 | 1,900 | 1,800 | 340 | 280 | 280 | 280 | 280 | 50 | 5,400 |
| Remote-handled low-level radioactive waste | – | – | 58 | 88 | 86 | 86 | 86 | 86 | 86 | 16 | 590 |
| Mixed remote-handled low-level radioactive waste | – | – | 6 | 10 | 10 | 10 | 10 | 10 | 10 | 2 | 66 |
| Contact-handled transuranic waste | 12 | 52 | 550 | 670 | 200 | 110 | 330 | 440 | 220 | 20 | 2,600 |
| Remote-handled transuranic waste | – | – | 35 | 37 | 1 | 1 | 1 | 1 | 1 | 1 ^b | 76 |
| Total nonliquid waste | 1,400 | 3,600 | 19,000 | 22,000 | 12,000 | 11,000 | 12,000 | 12,000 | 12,000 | 3,100 | 110,000 |
| Liquid Waste | | | | | | | | | | | |
| Industrial liquid waste | – | 1 | 1 | – | – | – | – | – | – | – | 3 |
| Hazardous liquid waste | – | 1 | 4 | 4 | 3 | | | | | | 13 |
| Low-level radioactive liquid waste | 1 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 14 |
| Mixed low-level radioactive liquid waste | 1 ^b | 1 ^b | 1 ^b | 1 ^b | 1 ^b | 1 ^b | 1 ^b | 1 ^b | 1 ^b | 1 ^b | 1 ^b |
| Total liquid waste | 1 | 4 | 7 | 6 | 5 | 1 | 1 | 1 | 1 | 1 | 30 |

^a Includes wastes regulated under RCRA, TSCA, or the New Mexico Solid Waste Act of 1990, or otherwise unacceptable for sanitary landfill disposal.

^b Shipment contains less than a full load.

Note: Because numbers have been rounded, the sums may not equal the indicated totals.

Table I-74 Materials and Shipments for Capping All Material Disposal Areas ^a

| Material | Fiscal Year | | | | | | | | | | Total |
|------------------------------|-------------|--------|---------|---------|---------|--------|---------|--------|---------|---------|-----------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | |
| Volumes (cubic yards) | | | | | | | | | | | |
| Minimum | | | | | | | | | | | |
| Tuff | 7,100 | 7,100 | 57,000 | 100,000 | 190,000 | 7,300 | 150,000 | 11,000 | 160,000 | 56,000 | 750,000 |
| Additional material | 590 | 590 | 6,600 | 11,000 | 130,000 | 610 | 120,000 | 930 | 120,000 | 41,000 | 430,000 |
| Rock armor | – | – | 230 | 810 | 170 | – | – | – | – | – | 1,200 |
| Retaining wall | – | – | 140 | 140 | – | – | – | – | – | – | 280 |
| Total material | 7,700 | 7,700 | 64,000 | 120,000 | 320,000 | 7,900 | 280,000 | 12,000 | 280,000 | 97,000 | 1,200,000 |
| Maximum | | | | | | | | | | | |
| Tuff | 19,000 | 19,000 | 120,000 | 250,000 | 520,000 | 20,000 | 420,000 | 30,000 | 430,000 | 150,000 | 2,000,000 |
| Additional material | 1,600 | 1,600 | 9,900 | 21,000 | 130,000 | 1,700 | 120,000 | 2,500 | 120,000 | 42,000 | 460,000 |
| Rock armor | – | – | 230 | 810 | 170 | – | – | – | – | – | 1,200 |
| Retaining wall | – | – | 370 | 380 | – | – | – | – | – | – | 750 |
| Total material | 21,000 | 21,000 | 130,000 | 270,000 | 660,000 | 22,000 | 540,000 | 33,000 | 550,000 | 190,000 | 2,500,000 |
| Shipments | | | | | | | | | | | |
| Minimum | | | | | | | | | | | |
| Tuff | 550 | 550 | 4,500 | 8,100 | 15,000 | 570 | 12,000 | 870 | 12,000 | 4,400 | 59,000 |
| Additional material | 46 | 46 | 510 | 870 | 9,900 | 48 | 9,600 | 72 | 9,600 | 3,200 | 34,000 |
| Rock armor | – | – | 14 | 48 | 10 | – | – | – | – | – | 72 |
| Retaining wall | – | – | 10 | 11 | – | – | – | – | – | – | 21 |
| Total material | 600 | 600 | 5,000 | 9,100 | 25,000 | 620 | 22,000 | 940 | 22,000 | 7,600 | 92,000 |
| Maximum | | | | | | | | | | | |
| Tuff | 1,500 | 1,500 | 9,500 | 20,000 | 41,000 | 1,600 | 33,000 | 2,400 | 34,000 | 12,000 | 150,000 |
| Additional material | 130 | 130 | 780 | 1,600 | 10,000 | 130 | 9,600 | 200 | 9,700 | 3,300 | 36,000 |
| Rock armor | – | – | 14 | 48 | 10 | – | – | – | – | – | 72 |
| Retaining wall | – | – | 28 | 29 | – | – | – | – | – | – | 57 |
| Total material | 1,600 | 1,600 | 10,000 | 21,000 | 51,000 | 1,700 | 42,000 | 2,600 | 43,000 | 15,000 | 190,000 |

^a Includes volumes and shipments for capping small areas in TA-49.

Note: To convert cubic yards to cubic meters, multiply by 0.765. Because numbers have been rounded, the sums may not equal the indicated totals.

Table I-75 Materials and Shipments for Removing All Material Disposal Areas

| Material | Fiscal Year | | | | | | | | | | |
|---|-------------|--------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | Total |
| Volumes (cubic yards) – MDA Removal plus Thin Cap at Area G^a | | | | | | | | | | | |
| Remove top layer | 850 | 11,000 | 62,000 | 67,000 | 36,000 | 33,000 | 35,000 | 36,000 | 34,000 | 6,700 | 320,000 |
| Remove additional soil | 5,200 | 12,000 | 560,000 | 750,000 | 470,000 | 440,000 | 440,000 | 440,000 | 440,000 | 84,000 | 3,600,000 |
| Stockpile return | 6,100 | 23,000 | 610,000 | 800,000 | 500,000 | 470,000 | 470,000 | 480,000 | 470,000 | 91,000 | 3,900,000 |
| Additional fill | 9,300 | 34,000 | 240,000 | 280,000 | 160,000 | 150,000 | 150,000 | 150,000 | 150,000 | 34,000 | 1,300,000 |
| Crushed tuff for capping. | 3,100 | 3,100 | 21,000 | 30,000 | 30,000 | 30,000 | 30,000 | 30,000 | 30,000 | 8,100 | 220,000 |
| Total tuff and fill | 12,000 | 37,000 | 260,000 | 310,000 | 190,000 | 180,000 | 180,000 | 180,000 | 180,000 | 42,000 | 1,600,000 |
| Additional material for MDA removal | 540 | 2,200 | 12,000 | 13,000 | 6,800 | 5,900 | 6,200 | 6,400 | 6,000 | 1,500 | 61,000 |
| Additional material for capping | 260 | 260 | 15,000 | 23,000 | 23,000 | 23,000 | 23,000 | 23,000 | 23,000 | 4,500 | 160,000 |
| Total additional material | 800 | 2,500 | 27,000 | 36,000 | 30,000 | 29,000 | 29,000 | 30,000 | 29,000 | 6,000 | 220,000 |
| Total material moved | 25,000 | 8,600 | 1,500,000 | 2,000,000 | 1,200,000 | 1,100,000 | 1,200,000 | 1,200,000 | 1,200,000 | 230,000 | 9,700,000 |
| One Way Shipments – MDA Removal plus Thin Cap at Area G^a | | | | | | | | | | | |
| Remove top layer | 60 | 780 | 4,400 | 4,700 | 2,500 | 2,300 | 2,500 | 2,600 | 2,400 | 470 | 23,000 |
| Remove additional soil | 370 | 880 | 40,000 | 53,000 | 33,000 | 31,000 | 31,000 | 31,000 | 31,000 | 6,000 | 260,000 |
| Stockpile return | 430 | 1,700 | 43,000 | 56,000 | 36,000 | 33,000 | 34,000 | 34,000 | 33,000 | 6,400 | 280,000 |
| Additional fill | 660 | 2,400 | 17,000 | 20,000 | 11,000 | 10,000 | 11,000 | 11,000 | 11,000 | 2,400 | 95,000 |
| Crushed tuff for capping | 240 | 240 | 1,600 | 2,400 | 2,400 | 2,400 | 2,400 | 2,400 | 2,400 | 630 | 17,000 |
| Total tuff and fill | 900 | 2,600 | 18,000 | 22,000 | 14,000 | 13,000 | 13,000 | 13,000 | 13,000 | 3,100 | 110,000 |
| Additional material for MDA removal | 39 | 160 | 850 | 940 | 480 | 420 | 440 | 460 | 430 | 110 | 4,300 |
| Additional material for capping | 20 | 20 | 1,200 | 1,800 | 1,800 | 1,800 | 1,800 | 1,800 | 1,800 | 350 | 12,000 |
| Total additional material | 59 | 180 | 2,000 | 2,700 | 2,300 | 2,200 | 2,200 | 2,300 | 2,200 | 460 | 17,000 |
| Total material moved | 1,800 | 6,100 | 110,000 | 140,000 | 87,000 | 81,000 | 83,000 | 83,000 | 82,000 | 16,000 | 690,000 |
| Volumes (cubic yards) – MDA Removal plus Thick Cap at Area G^a | | | | | | | | | | | |
| Remove top layer | 850 | 11,000 | 62,000 | 67,000 | 36,000 | 33,000 | 35,000 | 36,000 | 34,000 | 6,700 | 320,000 |
| Remove additional soil | 5,200 | 12,000 | 560,000 | 750,000 | 470,000 | 440,000 | 440,000 | 440,000 | 440,000 | 84,000 | 3,600,000 |
| Stockpile return | 6,100 | 23,000 | 610,000 | 800,000 | 500,000 | 470,000 | 470,000 | 480,000 | 470,000 | 91,000 | 3,900,000 |
| Additional fill | 9,300 | 34,000 | 240,000 | 280,000 | 160,000 | 150,000 | 150,000 | 150,000 | 150,000 | 34,000 | 1,300,000 |
| Crushed tuff for capping. | 8,400 | 8,400 | 57,000 | 83,000 | 83,000 | 83,000 | 83,000 | 83,000 | 83,000 | 22,000 | 600,000 |
| Total tuff and fill | 18,000 | 42,000 | 290,000 | 360,000 | 240,000 | 230,000 | 230,000 | 240,000 | 230,000 | 57,000 | 1,900,000 |
| Additional material for | 540 | 2,200 | 12,000 | 13,000 | 6,800 | 5,900 | 6,200 | 6,400 | 6,000 | 1,500 | 61,000 |

| Material | Fiscal Year | | | | | | | | | | | |
|---|-------------|--------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|------------|--|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | Total | |
| MDA removal | | | | | | | | | | | | |
| Additional material for capping | 700 | 700 | 16,000 | 24,000 | 24,000 | 24,000 | 24,000 | 24,000 | 24,000 | 4,900 | 160,000 | |
| Total additional material | 1,200 | 2,900 | 2,800 | 37,000 | 30,000 | 29,000 | 30,000 | 30,000 | 30,000 | 6,400 | 220,000 | |
| Total material moved | 31,000 | 92,000 | 1,600,000 | 2,000,000 | 1,300,000 | 1,200,000 | 1,200,000 | 1,200,000 | 1,200,000 | 240,000 | 10,000,000 | |
| One Way Shipments – MDA Removal plus Thick Cap at Area G^a | | | | | | | | | | | | |
| Remove top layer | 60 | 780 | 4,400 | 4,700 | 2,500 | 2,300 | 2,500 | 2,600 | 2,400 | 470 | 23,000 | |
| Remove additional soil | 370 | 880 | 40,000 | 53,000 | 33,000 | 31,000 | 31,000 | 31,000 | 31,000 | 6,000 | 260,000 | |
| Stockpile return | 430 | 1,700 | 43,000 | 56,000 | 36,000 | 33,000 | 34,000 | 34,000 | 33,000 | 6,400 | 280,000 | |
| Additional fill | 660 | 2,400 | 17,000 | 20,000 | 11,000 | 10,000 | 11,000 | 11,000 | 11,000 | 2,400 | 95,000 | |
| Crushed tuff for capping | 660 | 660 | 4,500 | 6,500 | 6,500 | 6,500 | 6,500 | 6,500 | 6,500 | 1,700 | 47,000 | |
| Total tuff and fill | 1,300 | 3,000 | 21,000 | 26,000 | 18,000 | 17,000 | 17,000 | 17,000 | 17,000 | 4,200 | 140,000 | |
| Additional material for MDA removal | 39 | 160 | 850 | 940 | 480 | 420 | 440 | 460 | 430 | 110 | 4,300 | |
| Additional material for capping | 55 | 55 | 1,200 | 1,800 | 1,800 | 1,800 | 1,800 | 1,800 | 1,800 | 380 | 13,000 | |
| Total additional material | 93 | 210 | 2,100 | 2,800 | 2,300 | 2,300 | 2,300 | 2,300 | 2,300 | 490 | 17,000 | |
| Total material moved | 2,300 | 6,600 | 110,000 | 140,000 | 91,000 | 86,000 | 87,000 | 87,000 | 86,000 | 18,000 | 720,000 | |

MDA = material disposal area.

^a Refers to capping the remaining disposal units in the existing 63-acre Area G footprint following MDA G removal. Includes small volumes and shipments of materials needed to optionally cap sites in Areas 6 and 12 of TA-49.

Note: To convert cubic yards to cubic meters, multiply by 0.765. Because numbers have been rounded, the sums may not equal the indicated totals.

MDA H. Assuming that remediation of MDA H occurs during the time period covered in this SWEIS, bulk material volumes and shipments projected in this section may be augmented as summarized in Sections I.3.3.2.2.2.

I.3.6.4 Equipment, Emissions, and Personnel Assumptions

This section addresses assumptions for equipment use, airborne emissions of machinery combustion products, personnel requirements for PRS remediation, personnel radiological exposures, and industrial accident risks. To do this, assumptions about hourly personnel and machinery use were developed from industrial cost, personnel, and equipment data provided in catalogs from the R.S. Means Company. In addition, the literature was reviewed for assumptions and experience at other remediation efforts such as those discussed in Section I.3.3.1.3.⁷⁰

Several case studies were developed using the Means data that were applicable to the different remediation efforts addressed in this appendix. For each case study, the Means cost data were used, along with other information in the Means catalogs, to estimate personnel hours and machinery use. The estimated personnel and machinery hours included contingency factor multipliers to account for special conditions at sites where radioactive material is involved. Projected personnel hours were used with assumptions about radiation environments associated with various remediation efforts to estimate personnel radiation doses and risks, as well as industrial accident risks. Projected equipment hours were used along with assumptions about hourly fuel requirements to determine gallons of fuel used. This information was then used with procedures and assumptions outlined in Section 3.3 (“Gasoline and Diesel Industrial Engines”) of AP 42, EPA’s compilation of air pollutant emission factors (EPA 1995), to estimate air emissions of nonradiological pollutants such as carbon monoxide and nitrogen oxides.

Table I–76 outlines each of the case studies and summarizes the results of the calculations using Means data for each study. In this table, equipment, personnel, and fuel use requirements are summarized on both a per-square-foot basis (as in square feet of area addressed) and on a per-cubic-yard basis (as in cubic yards of contaminated material removed). Contingency factor multipliers are also shown for each case study.

Total equipment hours and fuel use were determined for each of the case studies, and the total releases of pollutants associated with this fuel use (in tons released to the air) are summarized in **Table I–77**. **Table I–78** lists total personnel hours for each case study, as well as the calculated industrial risks resulting from these total personnel hours. Industrial risks for each case study were developed using 5-year-average DOE statistics for construction workers from the Computerized Accident and Incident Reporting System database (DOE 2004d) and information from the U.S. Department of Labor Statistics for the overall construction industry (DOL 2003). Information from these tables was used for each of the options in this appendix as discussed below.

⁷⁰ Remediation of MDA H has been addressed in previous NEPA analyses but may occur during the time period covered in this SWEIS. Estimates of equipment and personnel requirements and associated impacts for remediating MDA H were presented in this previous analyses (DOE 2004a).

Table I-76 Summary of Labor, Equipment Hours, and Fuel Use for Remediation Case Studies

| <i>Case Study</i> | <i>Area (acres)</i> | <i>Depth (feet)</i> | <i>Volume of Material (cubic yards)</i> | <i>Contingency Factor Assumed</i> | <i>Labor (hours per square foot)</i> | <i>Equipment (hours per square foot)</i> | <i>Fuel Use (gallons per square foot)</i> | <i>Labor (hours per cubic yard)</i> | <i>Equipment (hours per cubic yard)</i> | <i>Fuel Use (gallons per cubic yard)</i> |
|--|---------------------|---------------------|---|-----------------------------------|--------------------------------------|--|---|-------------------------------------|---|--|
| Case 1Aa – Small area, thin cap | 1 | 3 ^a | 6,300 | 1.5 | 0.085 | 0.052 | 0.32 | 0.59 | 0.36 | 2.2 |
| Case 1Ab – Small area, thick cap | 1 | 8.2 ^a | 17,000 | 1.5 | 0.17 | 0.11 | 0.64 | 0.43 | 0.27 | 1.6 |
| Case 1Ba – Large area, thin cap | 20 | 3 ^a | 130,000 | 1.5 | 0.075 | 0.046 | 0.28 | 0.52 | 0.32 | 1.9 |
| Case 1Bb – Large area, thick cap | 20 | 8.2 ^a | 340,000 | 1.5 | 0.15 | 0.090 | 0.55 | 0.37 | 0.23 | 1.4 |
| Case 2A – Removal of contaminated soil | 1 | 1 | 1,600 | 1.5 | 0.12 | 0.038 | 0.20 | 3.2 | 1 | 5.4 |
| Case 3A – Removal of shallow material from a small MDA | 1 | 15 | 24,000 | 1.5 | 1.6 | 0.52 | 2.7 | 2.9 | 0.93 | 4.9 |
| Case 3B – Removal of shallow material from a large MDA | 20 | 15 | 480,000 | 1.5 | 1.3 | 0.42 | 2.2 | 2.4 | 0.76 | 4 |
| Case 4A – Deeper soil or shaft removal | 1 | 60 | 48,000 | 2.0 | 32 | 12 | 72 | 29 | 11 | 64 |

MDA = material disposal area.

^a The reference for these case studies is to the thicknesses of the fill material for the caps. Additional materials that would be used for capping (fill for grading, topsoil, and other material) was considered for the estimates. The reference for the remaining case studies is to volume of material removed.

Note: To convert acres to hectares, multiply by 0.40469; feet to meters, multiply by 0.3048; cubic yards to cubic meters, multiply by 0.76459; square feet to square meters, multiply by 0.092903; gallons to liters, multiply by 3.78533. All numbers have been rounded.

Table I-77 Remediation Case Study Total Equipment and Fuel Use and Pollutant Emissions (tons released)

| <i>Case Study</i> | <i>Equipment Hours</i> | <i>Fuel Use (gallons)</i> | <i>Nitrogen Oxides</i> | <i>Carbon Monoxide</i> | <i>Sulfur Oxide</i> | <i>Particulate Matter^a</i> | <i>Carbon Dioxide</i> | <i>Aldehydes</i> | <i>Total Organic Carbon (TOC)</i> |
|--|------------------------|---------------------------|------------------------|------------------------|---------------------|---------------------------------------|-----------------------|------------------|-----------------------------------|
| Case 1Aa – Small area, thin cap | 2,300 | 14,000 | 3.7 | 9.4 | 0.24 | 0.26 | 150 | 0.065 | 0.70 |
| Case 1Ab – Small area, thick cap | 4,600 | 28,000 | 7.5 | 19 | 0.49 | 0.52 | 310 | 0.13 | 1.4 |
| Case 1Ba – Large area, thin cap | 40,000 | 240,000 | 66 | 170 | 4.3 | 4.6 | 2,700 | 1.1 | 12 |
| Case 1Bb – Large area, thick cap | 79,000 | 480,000 | 130 | 320 | 8.4 | 9.0 | 5,200 | 2.3 | 24 |
| Case 2A – Removal of contaminated soil | 1,600 | 8,700 | 2.3 | 5.9 | 0.15 | 0.16 | 95 | 0.041 | 0.44 |
| Case 3A – Removal of shallow material from a small MDA | 23,000 | 120,000 | 32 | 81 | 2.1 | 2.2 | 1,300 | 0.56 | 6.0 |
| Case 3B – Removal of shallow material from a large MDA | 370,000 | 1,900,000 | 520 | 1,300 | 34 | 36 | 21,000 | 9.1 | 98 |
| Case 4A – Deeper soil or shaft removal | 530,000 | 3,100,000 | 840 | 2,100 | 54 | 58 | 34,000 | 15 | 160 |

PM₁₀ = particulate matter having diameters smaller than 10 micron, MDA = material disposal area.

Note: To convert gallons to liters, multiply by 3.78533; tons to kilograms, multiply by 907.18. Numbers have been rounded.

Table I-78 Remediation Case Study Total Industrial Risks

| Case Study | Total Labor Hours | Safety – Construction Industry | | | Safety – DOE Construction | | |
|--|-------------------|--------------------------------|---------------|----------------------|---------------------------|----------------|------------|
| | | Recordable Injuries | Lost Workdays | Fatalities | Recordable Injuries | Lost Work Days | Fatalities |
| Case 1Aa – Small Area, Thin Cap | 3,700 | 0.16 | 1.7 | 3.8×10^{-4} | 0.042 | 0.14 | – |
| Case 1Ab – Small Area, Thick Cap | 7,500 | 0.32 | 3.4 | 7.8×10^{-4} | 0.085 | 0.28 | – |
| Case 1Ba – Large Area, Thin Cap | 65,000 | 2.8 | 30 | 6.8×10^{-3} | 0.74 | 2.5 | – |
| Case 1Bb – Large Area, Thick Cap | 130,000 | 5.4 | 59 | 0.013 | 1.5 | 4.8 | – |
| Case 2A – Removal of Contaminated Soil | 5,100 | 0.22 | 2.3 | 5.3×10^{-4} | 0.057 | 0.19 | – |
| Case 3A – Removal of Shallow Material from a Small MDA | 70,000 | 3.0 | 32 | 7.3×10^{-3} | 0.79 | 2.6 | – |
| Case 3B – Removal of Shallow Material from a Large MDA | 1,100,000 | 48 | 520 | 0.12 | 13 | 43 | – |
| Case 4A – Deeper Soil or Shaft Removal | 1,400,000 | 60 | 650 | 0.15 | 16 | 53 | – |

MDA = material disposal area.

Note: Numbers have been rounded.

Total personnel hours and radiation dose from MDA and PRS remediation are the sum of those associated with direct remediation efforts (addressed above) and those associated with remedial design and waste processing and loading onto trucks. Remedial design addresses work performed after the optimum remedial action alternative has been selected and prior to the onset of remedial construction. This work includes activities such as project planning, treatability or other studies, and preparation of design documents. A 10-percent factor for remedial design was assumed based on the range of complexity that would be associated with remediating the MDAs and PRSs. Assumptions for waste processing and loading onto trucks are addressed in Section I.3.5.

I.3.6.4.1 No Action Option

Under the No Action Option, a low level of remediation effort would take place. Personnel hours, air emissions, and industrial risks were estimated by determining ratios of waste volumes listed in Table I-68 to unit information derived for Case Study 2A, Removal of Contaminated Soil. (For example, nitrogen oxide [NO_x] emissions from removal of 1,000 cubic yards of soil as part of LANL’s environmental restoration project would be 1,000 cubic yards × 5.4 gallons per cubic yard × 2.3 tons per 8,700 gallons consumed, or 1.4 tons (1,300 kilograms) of nitrogen oxides released.)

Worker radiation exposures were determined by estimating total personnel hours engaged in remediation work (using the above methods) and multiplying these hours by an assumed radiation environment of 2.2×10^{-6} rem per hour (the same as the same hourly exposure rate for remediation of the combined PRS area discussed in Section I.3.6.4.3). Personnel hours and

radiation exposures for waste processing and truck loading were assessed as addressed in Section I.3.5.

I.3.6.4.2 Capping Option

Under this option, air emissions and personnel hours, exposure rates, and industrial safety risks were conservatively estimated as addressed for the No Action Option and through consideration of:

- Capping several MDAs
- Generating and handling wastes associated with capping the MDAs
- Generating and handling wastes associated with annually remediating several small PRSs such as Firing Site E-F or the 260 Outfall in various locations within LANL
- Generating crushed tuff in the TA-61 borrow pit for MDA capping

For capping, air emissions and personnel hours and industrial safety risks were proportioned to the nominal sizes of the MDAs and landfills using Case Study 1Aa, 1Ab, 1Ba, or 1Bb. Case Studies 1Aa and 1Ab were used for MDAs and landfills covering about 1 acre (0.4 hectare) or less. This included all MDAs (and the Area 12 landfill in TA-49) except for MDAs B, T, C, and G (and the Area 6 landfill in TA-49), for which Case Study 1Ba or 1Bb was used. The case studies imply the following approximate personnel hourly commitments per cubic yard of capping material:

- Case Study 1Aa: 0.6 hours per cubic yard
- Case Study 1Ab: 0.4 hours per cubic yard
- Case Study 1Ba: 0.5 hours per cubic yard
- Case Study 1Bb: 0.4 hours per cubic yard

These rates are within the range of those that have been estimated in the literature. For example, the environmental assessment for MDA H projected about 2.9 to 3.5 person-hours per cubic yard of emplaced material, assuming placement of 2,860 cubic yards of material over 0.4 acre (0.2 hectare) (DOE 2004b). Sandia projected from 0.4 to 0.49 person-hours per cubic yard of cover material added, assuming a cap covering about 2.6 acres (1.1 hectares) of a mixed waste landfill (SNL 2004). Idaho National Laboratory projected about 0.4 person-hour per cubic yard of material emplaced, assuming covering about 100 acres (40.5 hectares) of a legacy radioactive waste disposal site (INEEL 2002a, 2002b).

The radiation environment that may be expected for capping will vary depending on local levels of contamination, the materials disposed of in the MDAs, and other sources of radiation such as adjacent operational areas. The overall radiation environment for capping was assumed from measurements of external exposure rates at MDA T during 2003 (LANL 2004h). This measurement, taken from a TLD at the boundary of MDA T, was about 100 millirem per year

above background. This annual exposure rate is equivalent to an hourly exposure rate of 1.14×10^{-5} rem per hour. Using this exposure rate for all MDAs (except for MDA L and the landfills) should be conservative.

For generating and handling wastes associated with capping the MDAs and landfills, and annually remediating several PRSs, Case Study 2A was assumed. For both situations, the general radiation environment was assumed to be the same as for the combined PRS area (2.2×10^{-6} rem per hour; see Section I.3.6.4.3). Personnel hours and radiation exposures for waste processing and truck loading were assessed as addressed in Section I.3.5.

None of the case studies precisely correspond to borrow pit operation. The closest is Case Study 1Bb, placing a thick cap over a 20-acre (8.1-hectare) MDA. Hence, Case Study 1Bb was assumed to represent borrow pit operation.

I.3.6.4.3 Removal Option

Under this option, air emissions and personnel hours, exposure rates, and industrial safety risks were estimated as addressed for the No Action Option and through consideration of:

- Performing complete removal of several MDAs.
- Generating and handling wastes associated with annually remediating several small PRSs such as Firing Site E-F or the 260 Outfall in various locations within LANL. (Rates and risks were determined in the same manner as for the Capping Option.)
- Generating crushed tuff in the TA-61 borrow pit for backfilling MDAs.

Although removals have occurred at LANL and elsewhere, there is little experience with removals as challenging as those of many of the LANL MDAs. Several assessments have been published addressing removal operations at LANL and elsewhere. Most assessments were for postulated removals (DOE 2004b; INEEL 2002a, 2002d; SNL 2004; LANL 1981), while one addressed the completed removal of a chemical waste landfill (SNL 2003). Estimates of personnel requirements (and other factors) were quite variable.

For this appendix, emissions and personnel were estimated by scaling waste volumes removed for each MDA to unit volume factors for these parameters from Case Studies 3A, 3B, and 4A, as summarized in **Table I-79**. (Case Study 2A was again assumed for waste generated from preliminary MDA removal work and for annually remediating several PRSs.) Also shown are the assumed radiation environments associated with removal of the MDAs. Personnel hours and radiation exposure for waste processing and loading were assessed as addressed in Section I.3.5.

To estimate the general radiation environment for worker radiation dose assessments during MDA removal operations, RESRAD Version 6.3 calculations were performed for several MDAs assuming average waste radionuclide concentrations developed from the same inventories as those used for the air emissions assessment (see Section I.5.6.3.2). The primary value of these assessments is to compare options and to identify possible hazardous conditions. Actual removals would occur while using technical and administrative controls to maintain worker doses within prescribed limits and as low as reasonably achievable.

Table I–79 Case Studies Applied to Material Disposal Area Removal

| <i>Material Disposal Area</i> ^a | <i>Case Study</i> | <i>Radiation Environment (rem per hour)</i> | <i>Material Disposal Area</i> | <i>Case Study</i> | <i>Radiation Environment (rem per hour)</i> |
|--|-------------------|---|-------------------------------|-------------------|---|
| A (Eastern Pits) ^b | 3A | 0.000013 | L (Pits) ⁱ | 3A | Not applicable |
| A (Central Pit) ^b | 3A | 1.2×10^{-6} | L (Shafts) ⁱ | 4A | Not applicable |
| A (Tanks) ^b | 3A | 1.7×10^{-5} | F ^j | 3A | 2.2×10^{-6} |
| B ^c | 3B | 2.4×10^{-6} | Q ^k | 3A | 2.2×10^{-6} |
| T (Beds) ^d | 4A | 2.8×10^{-5} | N ^k | 3A | 2.2×10^{-6} |
| T (Shafts) ^d | 4A | 0.00025 | Z ^k | 3A | 2.2×10^{-6} |
| U (Beds) ^e | 3A | 0.00011 | R ^k | 3A | 2.2×10^{-6} |
| AB (shafts) ^f | 4A | 0.00025 | D ^k | 3A | 2.2×10^{-6} |
| C (Pits) ^g | 3B | 7.1×10^{-5} | E and K ^k | 3A | 2.2×10^{-6} |
| C (Shafts) ^g | 4A | 0.00025 | AA ^l | 3A | 2.2×10^{-6} |
| G (Pits) ^h | 4A | 3.6×10^{-5} | Y ^m | 3A | 2.2×10^{-6} |
| G (Shafts) ^h | 4A | 0.00025 | – | – | – |

^a For preliminary site work at any MDA, a radiation environment of 2.2×10^{-6} rem per person-hours was assumed using the radiation environment calculated for the combined potential release site area.

^b The worker exposure environment was assumed from RESRAD calculations.

^c The worker exposure environment was estimated from RESRAD calculations.

^d For MDA T beds, the working exposure environment was estimated from RESRAD calculations. For MDA T shafts, operations were assumed to be controlled to maintain individual exposures (assuming 2,000-hour work year) to levels smaller than 500 millirem in a year.

^e Exposure environment was assumed from RESRAD calculations.

^f Assumed the same exposure environment as that for the MDA T shafts.

^g Exposure environments were assumed from RESRAD calculations, with a maximum exposure rate of 0.00025 rem per hour to maintain individual exposures less than 500 millirem in a year.

^h MDA G pits contain pockets of small, high-activity waste containing cobalt-60 and cesium-137. Assumed that special measures would be taken for these pockets to maintain worker exposures to levels as low as reasonably achievable. Based the average radiation environment for MDA G pits on RESRAD calculations by excluding two small pockets of cobalt-60 and cesium-137. For MDA G shafts, assumed that worker exposure rates would be maintained to levels so that no individual receives more than 500 millirem in a year, assuming 2,000 work hours per year.

ⁱ MDA L should contain very little radioactive material, although precautions would be required for the presence of toxic and hazardous constituents.

^j Used the worker exposure environment estimated for the combined PRS area.

^k Assumed the same worker exposure environment as that for the combined PRS area.

^l Assumed the same worker exposure environment as that for the combined PRS area.

^m Worker exposure environment was estimated from RESRAD calculations.

If the radiation environment was not too high as determined from these calculations, the RESRAD calculations were assumed. However, DOE regulations prescribe an upper radiation dose limit of 5 rem (total effective dose equivalent) in a year. Special approval is required before allowing radiation doses to exceed 2 rem in a year, and administrative controls must be imposed to further reduce radiation exposures. The *DOE Standard Radiological Control Manual* indicates that an administrative control level of 500 millirem in a year (or less) should be challenging and achievable (DOE 1999c). Assuming 2,000 work hours per year and a 0.5-rem-per-year average dose level, worker radiation exposures would be limited to an average dose rate of 2.5×10^{-4} rem per hour. This average dose rate was the maximum assumed for removal of any MDA.

In addition, a radiation environment for worker radiation dose assessment (2.2×10^{-6} rem per hour) was estimated for the assumed annual remediation of several small PRSs and MDAs. This

radiation environment was determined using RESRAD Version 6.3 calculations assuming average radionuclide concentrations developed from the inventory assumed for the combined PRS area discussed in Section I.5.6.3.2.

Case Study 1Bb was again assumed to represent nonradiological releases and worker industrial risks from operations of the TA-61 borrow pit.

I.3.6.5 Affected Area Assumptions

Remediating the MDAs and PRSs will affect LANL property. In addition to the land area comprising the surface footprints of the MDAs and PRSs, additional area will be temporarily affected by operations supporting remediation. For example, capping an MDA may require temporary use of land for storage of bulk materials. Following completion of the task, the land would be restored. The amount of land that would thus be temporarily affected would depend on regulatory decisions, logistical considerations, and other factors.

MDAs. Temporary support areas associated with capping MDAs may include:

- A project management area, including a management trailer and space for staging equipment;
- An area for parking personal vehicles;
- An area for temporary management or storage of any wastes that may be generated; and
- An area for stockpiling bulk materials such as crushed tuff.

The size of a temporary project management area for any MDA may depend on the magnitude of the job, but should in most cases cover less than 1 acre (0.4 hectare). (The management area envisioned for remediating MDA H under any alternative covered only 0.2 acre (0.1 hectare) [DOE 2004b].) It is also expected that, for most MDAs, there should be no need to site additional personal vehicle parking infrastructure because sufficient nearby parking infrastructure should already exist.

For most MDAs, capping should not involve generation of significant quantities of waste. Hence, temporary waste management areas should (for most MDAs) be far smaller than 1 acre (0.4 hectare). Because most waste so generated will probably be either solid waste or low-activity low-level radioactive waste, storage time should be minimal. Roll-offs and Intermodals staged at a location for receipt of bulk waste would be present for the time required to fill them; when filled, they would be removed and replaced as needed by additional roll-offs and Intermodals. A 20-cubic-yard roll-off has typical dimensions of 8 by 20-22 by 4 feet tall (2.4 by 6.1-6.7 by 1.2 meters tall) (Burris 2005). Given packaging inefficiencies and swell of excavated waste, each roll-off is projected to contain about 13 cubic yards (10 cubic meters) of waste (see Table I-66). Assuming 10-foot (3-meter) side-to-side spacing and 5-foot (1.5-meter) end-to-end spacing, about 450 square feet (41.8 square meters) would be needed to temporarily store about 13 cubic yards (10 cubic meters) of low-activity waste. A site containing 10 roll-offs, or 130 cubic yards (100 cubic meters) of waste, would cover only about 0.1 acre (0.04 hectare).

The largest acreage may be dedicated to temporary storage of bulk materials. For many MDAs, much bulk material could be delivered directly to the worksite. But because of logistical or other considerations, it may be necessary to stockpile capping materials near the work area. Therefore, it was conservatively assumed that capping any MDA could require the temporary storage of 6 months' worth of capping materials.⁷¹ It was estimated by assuming a series of long, parallel rows of spoil piles, each pile roughly triangular in cross section. Because the material was assumed to be delivered and moved using trucks, loaders, and bulldozers, the piles were assumed to each be 10 feet (3 meters) high. The separation between piles was assumed to be 10 feet (3 meters). These assumptions result in an area commitment of 0.2 square feet per cubic foot (0.66 square meters per cubic meter) of stored spoil, considering a 20 percent swell of delivered material following initial excavation.

Temporary support areas associated with removing MDAs may include:

- A project management area, including a management trailer and space for staging equipment.
- An area for parking personal vehicles.
- An area for temporary management or storage of wastes.
- Capacity for storing bulk materials such as excavation spoils, final cover materials, or demolition debris.
- Possible capacity for preliminary classification of exhumed materials by hazard and for staging for further management.
- Possible capacity to process or package some wastes before shipment for further treatment or disposal.
- Possible capacity to characterize the waste in terms of organic, inorganic, and radioactive material content.

Similar to the assumption for capping MDAs, management areas associated with removal of most MDAs are assumed to cover less than 1 acre (0.4 hectare) for each MDA. (Additional areas may be needed for removal of waste from larger MDAs, or for decontaminating equipment.) It is also expected that, for most MDAs, there should be no need to site additional personal vehicle parking infrastructure because sufficient nearby parking infrastructure should already exist.

Areas needed for temporary management or storage of exhumed wastes would be larger than those for MDA capping. Depending on the MDA, waste management support areas may need to address a variety of wastes, including remote-handled waste. Shielded bunkers or similar facilities may be required, as may facilities for decontamination of equipment. However, because the bulk of the material removed from the waste would be very low-activity bulk material, it was again assumed that roughly 0.01 acre (0.004 hectare) would be required to store

⁷¹ Six months' capacity is assumed because, although work is expected to proceed in stages, there may be need for long-term storage of some materials.

about 13 cubic yards (10 cubic meters) of waste. Capacity for temporary storage and management of 3 months' generation of waste was assumed for each MDA.⁷²

A significant commitment of land may be associated with temporary storage of bulk materials such as overburden or backfill. Land requirements are assumed to be 0.2 square feet per cubic foot (0.66 square meters per cubic meter) of spoil (stockpiled overburden, removed clean fill, backfill, and topsoil), assuming a 6-month storage capacity and 20 percent material swell.⁷³

Additional land commitments may be needed for some MDAs for hazard classification of exhumed materials, waste processing or packaging of some wastes (for example, transuranic or remote handled wastes), or waste characterization (see Section I.3.3.2.8). Needed capacity would depend on regulatory decisions (for example, partial versus complete removal), volumes and characteristics of the exhumed wastes, and other factors. Assuming complete removal of all MDAs, capacity may be needed at several locations within LANL. Extrapolating from the sizes of facilities proposed for the investigation and remediation program for MDA B (Section I.3.3.2.7), complete MDA removal could temporarily involve up to 84 acres (34 hectares).⁷⁴

Additional PRSs. Support commitments for remediating other PRSs will generally be small and, again, temporary, but will vary depending on the PRS and the remediation decision. Temporary support areas may be needed for project management, temporary waste storage, equipment staging, or personal vehicle parking.

I.4 Affected Environment

This section provides summary descriptions of the natural and human environments possibly affected by the options considered in this appendix. Detailed descriptions of these environments within and near LANL are in Chapter 4 of this SWEIS.

I.4.1 Land Resources

Land resources include land use and visual resources. Land use is defined as the way land is developed and used in terms of the kinds of anthropogenic activities that occur (e.g., agriculture, residential areas, industrial areas) (EPA 2006). Visual resources are natural and manmade features that give a particular landscape its character and aesthetic quality. Landscape character is determined by the visual elements of form, line, color, and texture (DOI 1986).

I.4.1.1 Land Use

Land use at LANL is addressed in Chapter 4, Section 4.1.1, of this SWEIS. Existing land use is depicted in Figure 4-4. MDAs addressed in this appendix are listed in **Table I-80** along with

⁷² Three months' capacity was assumed because, in most cases, wastes would be stored for only a limited time before shipment and in consideration of RCRA storage requirements, which may be applicable for some wastes.

⁷³ These assumptions result in a calculated area for temporary storage of bulk materials from MDA H of about 1.3 acres (0.5 hectares), assuming 40 months of excavation, which is similar to the 1.2 acres (0.5 hectares) projected in the environmental assessment for MDA H (DOE 2004a).

⁷⁴ Assumed an additional five of each type of support facility (investigation facilities, waste processing facilities, and temporary laboratories). Assumed one each for removal of MDAs C and AB, one each for the remaining MDAs in TA-21, and two each for all MDAs in TA-54. As needed, the capacity could be used to support removal of the remaining small MDAs. From the proposed investigation and remediation of MDA B (Section I.3.3.2.7), this acreage is estimated as 6 (2 acres) + 6 (10 acres) + 6 (2 acres) = 84 acres (34 hectares).

their approximate sizes. The sizes of selected PRSs are also presented. A discussion of land use at each TA listed in Table I-80 is presented below, as well as at TA-61, which contains the principal LANL borrow pit.

Table I-80 Approximate Sizes of Material Disposal Areas and Selected Potential Release Sites

| <i>Technical Area</i> | <i>Material Disposal Area</i> | <i>Approximate Size of Material Disposal Area Site (acres)</i> | <i>Potential Release Site</i> | <i>Approximate Size of Potential Release Site (acres)</i> |
|-----------------------|-------------------------------|--|-------------------------------|---|
| 6 | F | 1.4 | – | – |
| 8 | Q | 0.2 | – | – |
| 15 | N | 0.28 | Site E-F | 11 |
| 15 | Z | 0.4 | Site R-44 | 6 |
| 16 | R | 11.5 | 260 Outfall (16-021(c) -99) | 0.7 |
| 21 | A | 1.25 | – | – |
| 21 | B | 6.0 | – | – |
| 21 | T | 2.2 | – | – |
| 21 | U | 0.2 | – | – |
| 33 | D | 0.03 | – | – |
| 33 | E | 1.4 | – | – |
| 33 | K | 1.0 | – | – |
| 35 | X ^a | 0.05 | – | – |
| 36 | AA | 1.4 | – | – |
| 39 | Y | 0.2 | – | – |
| 49 | AB | 0.45 | – | – |
| 50 | C | 11.8 | – | – |
| 54 | G | 63 ^b | – | – |
| 54 | L | 2.6 ^b | – | – |
| 73 | – | – | Ashpile | 1.2 |

^a Although MDA X has been recommended for no further action and will likely not require significant further remediation, it is near several other potential release sites in TA-35.

^b Listed acreage is for the areas containing the MDAs.

Note: To convert acres to hectares, multiply by 0.4047.

Technical Area 6. TA-6 covers 500 acres (202 hectares), of which only 1 percent is occupied by a gas cylinder staging facility, vacant buildings pending decommissioning, and a meteorological tower. It is south of TA-3, on a mesa between Twomile and Pajarito Canyons. Existing land use includes High-Explosive Research and Development and Reserve. MDA F is within the south-central portion of TA-6 in an area presently designated as Reserve. In the future, MDA F and the southern portion of the area could be redesignated as Experimental Science (LANL 2003f). According to the *Comprehensive Site Plan* for 2001, TA-6 is within the Anchor Ranch Planning Area. Future development is planned for the western half of the Planning Area; thus, development in the immediate vicinity of MDA F is unlikely (LANL 2001c).

Technical Area 8. Also known as the GT or Anchor West Site, TA-8 is at the western end of LANL. It covers 267 acres (108 hectares) and contains the Radiographic Testing Facility and MDA Q. The TA forms a portion of the Experimental Engineering Planning Area at LANL. Work includes high explosive research and development and testing (LANL 2001c). Current

land use designations include High-Explosive Research and Development and Reserve; future land use is not expected to change (LANL 2003f). MDA Q is within an area designated as Potential Infill (LANL 2001c).

Technical Area 15. Centrally located within LANL, TA-15 is largely on Threemile Mesa. It is bounded on the north by Pajarito Canyon and on the south by Water Canyon. The entire TA is designated as High Explosive Testing. The future land use designation is likely to remain the same (LANL 2003f). As determined by the *Comprehensive Site Plan* for 2001, MDAs N and Z and Firing Sites E-F and R-44 are within areas classified as Potential Infill (LANL 2001c).

Technical Area 16. TA-16 covers 1,950 acres (789 hectares) at the southwest corner of LANL; it is adjacent to Bandelier National Monument. Land use includes High-Explosive Research and Development, Public and Corporate Interface, Physical and Technical Support, and Reserve. Future land use is expected to remain largely unchanged except that the Public and Corporate Interface area in the western portion of the TA will increase in size and the Physical and Technical Support area will no longer exist (LANL 2003f). MDA R and the 260 Outfall (SWMU 16-021(c)-99) are within the northern portion of the area designated as High-Explosive Research and Development. According to the *Comprehensive Site Plan* for 2001, MDA R covers 11.5 acres (4.7 hectares) and falls within areas designated as Potential Infill and No Development Zone (Hazard). The 260 Outfall is within an area designated as No Development Zone (Hazard) (LANL 2001c).

Technical Area 21. TA-21 covers 312 acres (126 hectares) at the eastern end of DP Mesa, near the central business district of the Los Alamos Townsite. The airport is immediately north of TA-21 across DP Canyon. Much of the TA has been developed, mainly the west-central portion of the TA. Remaining portions consist of sloped areas, some of which would likely not accommodate development. Access to the TA is via DP Road.

TA-21 was identified for possible conveyance to Los Alamos County under Section 632 of Public Law 105-119 (see Chapter 4, Section 4.1.1, of this SWEIS). This TA has been divided into four subtracts for purposes of the land conveyance: TA-21-1 (West), which consists of two units, and TA-21-2 (East). (The subtracts have also been designated A-8, A-15-1, A-15-2, and A-16, respectively. Subtracts A-8, A-15-1, and A-15-2 cover 33.7 acres (13.6 hectares) and either have been or are scheduled to be conveyed to the county. Conveyance of the 252-acre (102-hectare) A-16 subtract has been withdrawn; MDAs A, B, T, and U are within this subtract.

Land use includes Waste Management, Service and Support, Nuclear Materials Research and Development, and Reserve. Future land use is slated as Reserve (LANL 2003f). The MDAs are within two areas designated as No Development Zone (Hazard).

Technical Area 33. Located in the southeastern corner of LANL and also known as the Hot Point Site, TA-33 covers 1,919 acres (777 hectares). It is bounded on the north by TA-70, on the southeast by the Rio Grande, and on the southwest by Bandelier National Monument and the Santa Fe National Forest. TA-33 is designated as Experimental Science and Reserve and is used for experiments that require isolation or do not require daily oversight. In the future, the area used for Experimental Science will likely increase and that for Reserve decrease (LANL 2003f). As determined by the *Comprehensive Site Plan* for 2001, TA-33 falls within the Rio Grande

Development Area. MDAs D, E, and K are all within areas classified as Potential Infill (LANL 2001c).

Technical Area 35. Also known as Ten Site, TA-35 is used for nuclear safeguards research and development; reactor safety research; optical science and pulsed-power system research; and metallurgy, ceramic technology, and chemical plating activities. TA-35 covers 150 acres (61 hectares) in the northern half of LANL on a finger mesa between Mortandad Canyon and Ten Site Canyon. Land use includes Nuclear Materials Research and Development, Experimental Science, Physical and Technical Support, and Reserve. Future land use is expected to be similar except that the Physical and Technical Support land use category will likely be absent (LANL 2003f). TA-35 is part of the Pajarito Corridor West Development Area, one of the most restricted areas at LANL. Infill development at TA-35 is possible to replace the small, temporary structures scattered throughout the area (LANL 2001c).

Technical Area 36. Also known as the Kappa Site, TA-36 has four active firing sites. The TA is in a remote area in the southeastern portion of LANL. The TA is part of the Dynamic Testing Planning Area at LANL, which is the largest LANL planning area, covering 2,777 acres (1,124 hectares) (LANL 2001c). Land use at the TA is nearly exclusively High-Explosive Testing, with small areas of Physical and Technical Support and Reserve. Future land use is expected to be similar except the Physical and Technical Support area may not be present (LANL 2003f). TA-36 is within the Water Canyon Development Planning Area. MDA AA is in an area designated as Potential Infill (LANL 2001c).

Technical Area 39. TA-39 is at the bottom of Ancho Canyon in the south-central part of LANL. Covering 2,444 acres (989 hectares), TA-39 was created when explosives work at TA-15 became too crowded. Like TA-36, TA-39 is part of the Dynamic Testing Planning Area at LANL. Nearly the entire TA is classified as High-Explosive Testing, with small areas of Physical and Technical Support and Reserve. Future land use is expected to be similar (LANL 2003f). TA-39 is within the Water Canyon Development Area. MDA Y in the central portion of the TA in an area designated as Potential Infill (LANL 2001c).

Technical Area 49. TA-49 covers 1,280 acres (518 hectares) and is largely undeveloped. The TA is within the south-central portion of LANL and is bordered on the south by Bandelier National Monument. Land use designations include High-Explosive Testing, Physical and Technical Support, and Reserve; these designations are not expected to change in the future (LANL 2003f). MDA AB is within the Physical and Technical Support land use zone. According to the *Comprehensive Site Plan* for 2001, TA-49 is within the Water Canyon Development Area. The general area containing MDA AB is categorized as Potential Infill, indicating that some future development could take place; however, such development would not occur within the MDA (LANL 2001c).

Technical Area 50. TA-50 covers 62 acres (25 hectares). It is 1.3 miles (2.1 kilometers) southeast of TA-3 along Pajarito Road. Land use designations include Waste Management and Reserve. Only the portion of the TA north of MDA C contains buildings. Future land use categories are projected to be similar except that the Waste Management land use area could be enlarged to include the entire northern part of the TA (LANL 2003f). TA-50 is within the Pajarito Corridor West Development Area as set forth in the *Comprehensive Site Plan* for 2001.

Although the area to the south of Pajarito Road is designated as suitable for Secondary Development, the portion of the TA containing MDA C is designated as No Development Zone (Hazard) (LANL 2001c).

Technical Area 54. TA-54 covers 858 acres (347 hectares). MDAs G and L encompass 68 acres (28 hectares), or 7.2 percent of the TA. The 3-mile (4.8-kilometer) northern border of the site forms the boundary between LANL and San Ildefonso Pueblo lands. The residential area of White Rock borders the site at its eastern boundary. Land use within TA-54 is categorized as Experimental Science, Waste Management, and Reserve. Future land use is likely to be similar except that the area devoted to waste management is predicted to expand such that it forms a continuous band along the TA's southern boundary (LANL 2003f). According to the *Comprehensive Site Plan* for 2001, TA-54 is within the Pajarito Corridor East Development Area. The area containing MDAs G and L is categorized as Potential Infill, indicating that some future development could take place; however, such development would not occur within the MDAs (LANL 2001c).

Technical Area 61. Also known as the East Jemez Site, TA-61 is northeast of TA-3 and covers 297 acres (120 hectares). TA-61 is used for physical support and contains infrastructure facilities, including the Los Alamos County Landfill covering 48 acres (19 hectares). The generalized land use categories for the TA include Physical and Technical Support and Reserve. The 43-acre (17-hectare) area containing the borrow pit is next to East Jemez Road in the eastern portion of the TA in an area designated as Physical and Technical Support. The borrow pit is east of the Royal Crest Manufactured Home Community. Future land use will probably be similar (LANL 2003f). According to the *Comprehensive Site Plan* for 2001, the TA is within the Sigma Mesa Development Area that could undergo considerable future development (LANL 2001c).

Technical Area 73. This TA covers 272 acres (110 hectares) along the northern boundary of LANL next to NM 502 (East Road). The TA comprises the Los Alamos County Airport, which is owned by DOE and managed by the Los Alamos County. Land use consists of Airfield and Reserve; it is not expected to change in the future (LANL 2003f). The asphalt is north of the airport terminal building. Land use along East Road near TA-73 includes offices and other light commercial and retail land uses, as well as several churches, a swimming facility, and a park. TA-73 is part of the Omega West Planning Area. The Los Alamos County Airport is part of the DOE land exchange package (see Chapter 4, Table 4-2) (LANL 2001c).

I.4.1.2 Visual Environment

LANL visual resources are addressed in Chapter 4, Section 4.1.2, of the SWEIS. This section discusses the visual setting of the TAs addressed in Section I.4.1.1.

Technical Area 6. TA-6 is on a mesa between Twomile and Pajarito Canyons. The area is largely undeveloped; however, it contains a gas cylinder staging facility, vacant buildings pending decommissioning, and a meteorological tower. The heavily wooded area is visible from Pajarito Road and from higher elevations to the west along the upper reaches of the Pajarito Plateau rim (NNSA 2003). MDA F is a grassy area of which a portion is fenced. These areas are

not readily visible by the public because Twomile Mesa Road, passing to the south of the MDA, is not a public road.

Technical Area 8. TA-8 is between the upper reaches of Pajarito Canyon to the north and TA-16 to the south. Although portions of the TA are forested, the part of the TA containing MDA Q has been cleared and contains a few structures within a grassy area. The site would generally not be visible to the public because trees separate it from West Jemez Road. From higher elevations to the west, TA-8 appears as part of a larger developed area.

Technical Area 15. Situated on Threemile Mesa, TA-15 is bounded on the north by Pajarito Canyon and on the south by Water Canyon. Additionally, the northern part of the TA is dissected by Threemile Canyon and the central portion by Potrillo Canyon. The TA contains scattered facilities within a largely forested area. The dispersed arrangement of facilities reflects the use of the TA for high-explosive research, development, and testing. Due to the isolated nature of TA-15, buildings and structures are generally not visible to the public. If viewed from higher elevations to the west, the TA appears largely as wooded with only a scattering of facilities located throughout. MDAs N and Z and Firing Sites E-F and R-44 present a disturbed appearance that would be indistinguishable from other facilities within TA-15 when viewed from higher elevations to the west.

Technical Area 16. TA-16 is in the southwestern corner of LANL and is bounded on the north by Cañon de Valle and on the south by Water Canyon. Most buildings and structures are in the western part of the TA, with some facilities visible from West Jemez Road. From the mountains to the west, the TA appears as highly developed in the west, with development being replaced by forests in the east. Although portions of MDA R within and immediately adjacent to the High-Explosives Development Area are cleared of forest cover, some of the 11.5-acre (4.7-hectare) site is wooded. The 260 Outfall is generally tree covered.

Technical Area 21. Facilities at TA-21 are on a mesa between Los Alamos Canyon to the south and DP Canyon to the north. Developed portions of the TA present an industrial appearance. Undeveloped portions of the mesa remain vegetated with native grasses, shrubs, and small trees. The canyons are wooded. While portions of the site, particularly the water tower, can be seen from locations along NM 502, the MDAs are not visible. From higher elevations, developed portions of TA-21 have an industrial appearance and would be visible, although the MDAs would appear as cleared or grassy areas (DOE 1999e).

Technical Area 33. TA-33, in the southeast corner of LANL, is bordered by the Rio Grande on the east, TA-39 and TA-70 on the north, and Bandelier National Monument and Santa Fe National Forest on the west. Most of the TA is forested, although three small areas of development are present. As viewed from NM 4, the area would have a natural appearance. MDAs D, E, and K are within these developed areas, each containing buildings, roads, and parking lots; however, these areas are not visible to the public.

Technical Area 35. This TA is part of a highly developed portion of LANL extending along the upper 2.7 miles (4.3 kilometers) of Pajarito Road. This area therefore presents the appearance of a mosaic of industrial buildings and structures interspersed with forests along the mesa. Views

of TA-35 are generally blocked by trees and other development along Pajarito Road. Mortandad Canyon is wooded and has a natural appearance when viewed from a distance and from nearby.

Technical Area 36. The largest LANL TA, TA-36 is traversed or bordered by several forested canyons, including Pajarito, Threemile, Potrillo, and Fence Canyons. Although TA-36 is largely undeveloped and forested, that portion of the TA containing MDA AA includes several buildings. MDA AA is an open area, although it is not accessible to the public.

Technical Area 39. Similar to other large TAs within this portion of LANL, TA-39 is largely forested with pockets of development. MDA Y is to the east of Ancho Road within a developed area. As with most other MDAs, the MDA is a cleared area that cannot be viewed by members of the public.

Technical Area 49. Only a small portion of TA-49 is developed, although several roads cut through portions of the site. Most of the TA is made up of scattered trees and shrubs with a grassy understory. Overall, the site has a natural appearance. The MDAs are within the Frijoles Mesa Site, which contains scattered buildings and roads. The MDAs appear little different than surrounding areas in that they are grass covered and contain scattered shrubs and trees.

Technical Area 50. TA-50 is along Pajarito Road. While much of the mesa along which the road passes is forested, TA-50 is one of a series of TAs along the upper 2 miles (3.2 kilometers) of the road within which development has taken place. Thus, this area presents the appearance of a mosaic of industrial buildings interspersed along a forested mesa. Views of the area from a distance are described in Chapter 4, Section 4.1.2, of this SWEIS. TA-50 includes both portions of the mesa and Mortandad Canyon. Development has occurred on that portion of the site north of Pajarito Road, with the remaining portions of the mesa and the canyon south of the road remaining forested. Although near views of TA-50 are industrial in nature, they are available only to site personnel because Pajarito Road is closed to the public. MDA C is along Pajarito Road and appears as a fenced grassy field. Future plans call for a landscape improvement buffer to be planted along Pajarito Road (LANL 2001c).

Technical Area 54. TA-54 is at the eastern end of Pajarito Road and borders both the San Ildefonso Pueblo and White Rock. While buildings and structures of the TA are visible from higher elevations to the west, near views of many TA elements are limited, as Pajarito Road is closed to the public. However, the dominant feature of the site is the white domes of MDA G in the eastern end of the TA. These domes contrast with the natural landscape and can be seen for many miles from locations in the Nambe-Española area and from locations in western and southern Santa Fe (LANL 2004f). They are visible from the lands of the San Ildefonso Pueblo. The remaining portions of MDAs G and L are less visible from a distance, as they do not contain similar structures.

Technical Area 61. TA-61 is in the northern portion of LANL along East Jemez Road. The TA is bordered by Los Alamos Canyon to the north and Sandia Canyon to the south. Although the Los Alamos County Landfill is the largest facility in TA-61, the borrow pit is also a significant feature. The borrow pit is 2 miles (3.2 kilometers) east of the landfill. Although much of TA-61 presents a forested appearance from higher elevations to the west, the borrow pit (and landfill) would be visible as an area devoid of vegetation. Yet the borrow pit is not visible from East

Jemez Road because of its location relative to the road, trees bordering the road, and a small hill on the north side of the pit.

Technical Area 73. This TA is along the northern boundary of LANL next to NM 502 (East Road). The Los Alamos County Airport is north of the road and DP Canyon is south of it. Views of the TA include those from the north across Pueblo Canyon and from East Road. Views from East Road include the airport to the north and undeveloped wooded areas to the south. The airport is visible from the subdivision to the west. A visual assessment of this tract, made in conjunction with the conveyance of land to Los Alamos County, determined that views of the airport have moderate value, while those of DP Canyon have high value (DOE 1999e).

I.4.2 Geology and Soils

Geology, soils, and mineral resources at LANL are addressed in Chapter 4, Section 4.2, of the SWEIS.

Geology. LANL site geology consists primarily of a complex series of interlayered volcanic deposits. As discussed in Section 4.2, the degree of welding, induration, and fracturing of the rocks at LANL plays an important role in slope stability and subsurface fluid flow. These characteristics are important because the MDAs have generally been cut to varying depths into the upper units of the Tshirege Member of the Bandelier Tuff to varying depths. This may provide a groundwater flow conduit between disposed materials and subsurface permeable rocks. Depending on their location and existing constructed surfaces, certain MDAs may be susceptible to erosion and surface failure (LANL 1999b).

Subunits of the Tshirege Member dip gently southeastward on the Pajarito Plateau. The paleotopography of the pre-Tshirege surface may strongly influence the direction of possible groundwater flow and contaminant migration in subsurface units beneath the MDAs. The paleotopography of the pre-Otowi surface may influence the flow direction of potential perched groundwater (DOE 1999a).

Soils. A description of LANL soils was included in the 1999 SWEIS and is updated in Chapter 4, Section 4.2.3, of this SWEIS. This update includes a description of the soils, the effects of the May 2000 Cerro Grande Fire, and the soil monitoring program. In most cases, environmental restoration activities would not affect native soils because MDAs and PRSs are in areas that have already been disturbed by LANL activities.

Mineral Resources. The only mineral resource being mined at LANL is crushed tuff from the East Jemez Road borrow pit in TA-61. The source material is the Tshirege member of the Bandelier Tuff. Other materials needed to support the corrective action or closure program for LANL MDAs include soil to support vegetation and rock for erosion control. Local offsite sources and excess materials from LANL building construction are available.

I.4.3 Water Resources

Water resources are addressed in Chapter 4, Section 4.3, and Appendix E, Groundwater in the Vicinity of LANL, of the SWEIS. Appendix F, Environmental Sample Data, presents sample information pertaining to water resources.

Water resources in the LANL region include surface waters, sediments, floodplains, and groundwater located onsite, on adjacent properties, and extending to northern New Mexico and southern Colorado. The LANL area includes 15 regional watersheds (see Chapter 4, Figure 4–12), with 12 watersheds crossing LANL boundaries. Water resources were affected by the 2000 Cerro Grande Fire in that it increased the potential for surface runoff and soil erosion in burned areas (see Chapter 4, Section 4.3.1.7). Water resources were the focus of many of the investigations that have been performed at LANL. Several historical investigations pertaining to the LANL MDAs are summarized in the MDA Core Document (LANL 1999b). LANL water resources are a major focus of the Consent Order. Investigations being performed in accordance with the Consent Order are meant to fully characterize the nature, extent, fate, and transport of contaminants that may have entered groundwater and surface water resources at LANL.

Surface Water. Most canyons that drain the LANL site are dry for most of the year. Surface water in the area occurs primarily as short-lived or intermittent reaches of streams. Perennial surface water of varying lengths exists in Sandia, Pajarito, and Water Canyons, and Cañon de Valle. Many streams flow in response to only local precipitation or snowmelt. While there is minimal direct use of the surface water within LANL except by wildlife, streamflow may extend beyond the LANL boundaries where there may be more direct use of the water. LANL programs manage several sources that may impact local water resources, such as liquid effluents discharged through NPDES permitted outfalls, stormwater runoff, sediment transport, and dredge and fill activities or other work within perennial, intermittent, or ephemeral watercourses. LANL personnel routinely monitor surface water, stormwater, and sediments as part of LANL’s ongoing environmental monitoring and surveillance program, and the results are published annually.

Sediments occur in and along LANL’s canyons and watersheds, primarily as narrow bands of canyon bottom deposits that can be transported by surface water flows, effluent discharges, stormwater runoff, or flooding within canyons. Past LANL activities have caused contamination of sediments both onsite and downstream, occurring primarily because of effluent discharge from LANL outfalls and the transport of contaminated sediments from runoff and effluent flow. Sediments in some watersheds and canyons were transported and redistributed downstream from LANL after the Cerro Grande Fire. An overview of sediment quality and contamination levels is provided in Chapter 4, Section 4.3.1.5, of this SWEIS. Investigation and, if necessary, remediation of contaminated sediment at LANL is being conducted in conformance with the Consent Order and other regulatory criteria.

Floodplains are normally dry land areas that can become inundated with surface waters during a period of runoff due to precipitation or snowmelt. The Cerro Grande Fire impacted the extent and elevation of the floodplains in LANL canyons. Several flood and sediment structures were constructed as part of the emergency response to the fire. Following the fire, floodplain boundaries were remapped for all the major watersheds within LANL, as illustrated in Chapter 4, Figure 4–15, of this SWEIS.

Groundwater. Groundwater beneath the Pajarito Plateau is separated into alluvial groundwater in the canyons, intermediate perched groundwater beneath some of the canyons and the western portion of the plateau at depths of 100 to 750 feet (30.5 to 229 meters), and a regional aquifer at depths of 600 to 1,200 feet below the surface of the plateau. About 350 to 620 feet (107 to 189 meters) of unsaturated tuff, basalt, and low-moisture-content sediments separate the alluvial and

perched groundwater zones and the regional aquifer. **Table I–81** summarizes the approximate depths of the regional groundwater table underneath the MDAs considered in this project-specific analysis, as well as the canyon watersheds associated with each MDA (LANL 1999b).

Table I–81 Watersheds and Depth to Regional Water by Material Disposal Area

| <i>Technical Area</i> | <i>Material Disposal Area</i> | <i>Watershed/Canyon</i> | <i>Depth to Regional Water (feet)</i> |
|-----------------------|-------------------------------|---------------------------|---------------------------------------|
| 6 | F | Twomile | 1,275 |
| 8 | Q | Pajarito | 1,200 |
| 15 | N | Cañon de Valle | 1,170 |
| 15 | Z | Cañon de Valle | 1,200 |
| 16 | R | Cañon de Valle | 1,240 |
| 21 | A | DP | 1,230 |
| 21 | B | Los Alamos | 1,300 |
| 21 | T | DP | 1,240 |
| 21 | U | DP | 1,220 |
| 33 | D | Rio Grande | 910 |
| 33 | E | Chaquehui | 760 |
| 33 | K | Chaquehui | 820 |
| 35 | X | Ten Site | 1,160 |
| 36 | AA | Potrillo | 770 |
| 39 | Y | North Ancho | 590 |
| 49 | AB | Ancho | 1,120 |
| 50 | C | Ten Site | 1,175 |
| 54 | G | Pajarito, Cañada del Buey | 900 |
| 54 | L | Cañada del Buey | 940 |

Note: To convert feet to meters, multiply by 0.3048.

Source: LANL 1999b.

Effluent discharge, natural spring discharge, and stormwater runoff create surface waters that infiltrate into the alluvium of some canyons to create shallow, unconfined groundwater. Intermediate perched groundwater is often found beneath canyons having alluvial groundwater and usually does not extend laterally beneath the mesas. Intermediate perched zones may be confined or unconfined, and may not be contiguous along the length of a canyon.

Discharge of effluents has resulted in detection of radionuclide contamination in alluvial groundwater samples from DP, Los Alamos, and Mortandad Canyons. Tritium has been found in intermediate-depth wells in Pueblo, Los Alamos, Mortandad, Pajarito, and Water Canyons, and technetium-99 in one well in Mortandad Canyon. Nonradioactive contaminants found in alluvial and intermediate-depth groundwater samples in Pueblo, Los Alamos, Mortandad, Pajarito, Water, Cañon de Valle, and Sandia Canyons include chromium, nickel, molybdenum, perchlorate, nitrate, barium, 1,4-dioxane, and hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX) (see Chapter 4, Section 4.3.2, of the SWEIS).

Regional groundwater flows toward the east and southeast to the Rio Grande. Little natural recharge occurs along the mesa tops where most LANL facilities and MDAs are located. For the past 5 years, LANL has been drilling and testing wells, monitoring wells, and modeling the subsurface groundwater hydrology as part of its *Hydrogeologic Work Plan* (see Chapter 4, Section 4.3.2, of the SWEIS). Some contamination of the regional aquifer has occurred, as

summarized in Section 4.3.2. LANL personnel conduct subsurface modeling addressing contaminant transport pathways near water supply wells.

I.4.4 Air Quality and Noise

Chapter 4, Section 4.4, of the SWEIS presents a detailed discussion of the climate, current air quality, and noise environments at LANL.

I.4.4.1 Climatology and Meteorology

The Los Alamos region has a semiarid, temperate mountain climate (DOE 1999a). Climatological information presented in the *1999 SWEIS*, and as updated for this SWEIS, has been derived from measurements at the official Los Alamos meteorological weather station and tower which is in TA-6. Additional towers are located in TA-41, TA-49, TA-53, and TA-54, and on Pajarito Mountain. The locations of all six towers are shown in Chapter 4, Figure 4-19, of this SWEIS.

Meteorological conditions are influenced by the Pajarito Plateau elevation. For example, temperatures in the Los Alamos area vary with altitude, averaging 5 °F (3 °C) higher in and near the Rio Grande Valley and 5 to 10 °F (3 to 5.5 °C) in the Jemez Mountains. The Los Alamos region is characterized by seasonable, variable rainfall, with precipitation ranging historically from 10 to 20 inches (25 to 51 centimeters) per year. The normal annual precipitation for Los Alamos from 1961 to 1990 was 19 inches (48 centimeters). Annual precipitation rates within the county decline toward the Rio Grande Valley. For example, the Jemez Mountains receive over 25 inches (64 centimeters) of precipitation annually, while normal precipitation for White Rock has been 14 inches (34 centimeters). About 36 percent of the annual precipitation for Los Alamos County and LANL has resulted from thundershowers that occur in July and August. Los Alamos County wind speeds vary seasonally, but average 7 miles per hour (3 meters per second). (Wind rose information from the LANL meteorological stations is presented in Chapter 4, Section 4.4.1.1, of this SWEIS.) Thunder- and hailstorms are common in Los Alamos County, and lightning can be frequent and intense. Flash flooding is possible in arroyos, canyons, and low-lying areas (DOE 1999a).

Since publication of the *1999 SWEIS*, the LANL region has experienced a notable drought. As discussed in Chapter 4, Section 4.4.1, of this SWEIS, between 1995 and 2004, only 1 year (1997) had above-average precipitation. The drought facilitated the Cerro Grande Fire in May 2000.

A summary of the local climate data for MDAs as measured at the nearest LANL meteorological station from each MDA are presented in **Table I-82**. Mesas are typically sunnier and windier than the canyons or slopes (LANL 1999b).

Table I–82 Comparative Summaries for Los Alamos National Laboratory Meteorological Stations with Nearby Material Disposal Areas

| Meteorological Station | Nearby MDAs | Average Temperature (°C) | | Average Temperature (°F) | | Precipitation (inches per year) | Winds (meters per second) | Winds (miles per hour) ^a |
|------------------------|---------------------|--------------------------|-----|--------------------------|-----|---------------------------------|---------------------------|-------------------------------------|
| | | Min | Max | Min | Max | | | |
| TA-6 | F, Q, N, Z, R, X, C | 1.8 | 15 | 35 | 59 | 19.69 | 2.49 | 5.6 |
| TA-49 | Y, AB | 3.4 | 16 | 38 | 61 | 18.68 | 2.41 | 5.4 |
| TA-53 | A, B, T, U | 4.4 | 17 | 40 | 62 | 15.97 | 2.9 | 6.5 |
| TA-54 | D, E, K, AA, G, L | 0.99 | 18 | 34 | 64 | 14.57 | 2.74 | 6.1 |

^oC = degrees Celsius, ^oF = degrees Fahrenheit, MDA = material disposal area, Min = minimum, Max = maximum, TA = technical area.
Source: LANL 1999b.

I.4.4.2 Air Quality and Visibility

Air quality considerations include nonradiological air quality in terms of criteria pollutants such as nitrogen dioxide, sulfur dioxide, and particulates; radiological air quality; and visibility. Los Alamos County, including LANL, is in attainment with all state ambient air quality standards and with the National Ambient Air Quality Standards (see Chapter 4, Section 4.4.2.3, of this SWEIS). As addressed in Chapter 4, Section 4.4.3, a long-standing and extensive program has existed at LANL to ensure that possible radiological exposures of members of the public from air emissions are maintained to levels as low as reasonably achievable below all applicable standards. Periodic environmental surveillance and compliance reports document compliance with state, EPA, and DOE standards.

Visibility is measured according to a standard visual range. Visibility has been monitored by the National Park Service at Bandelier National Monument since 1988. Average visibility from 1993 through 2002 ranged from 79 to 113 miles (127 to 182 kilometers) (LANL 2004f).

I.4.4.3 Noise, Air Blasts, and Vibration

The LANL noise, air blast, and vibration environment is discussed in Chapter 4, Section 4.4.5, of this SWEIS. Background sounds, vehicular traffic, routine operations, and high-explosives testing contribute to noise levels. Air blasts (air pressure waves or overpressures) are intermittent, accompanying an explosive detonation, and may be heard by workers and the public. Most ground vibrations are from aboveground explosives research.

Sound intensity is expressed in decibels (dB) above the standard threshold of hearing. Noise levels at frequencies corresponding to maximum human sensitivity are used to set human limits for auditory protection. These frequencies are called A-weighted (after middle A and its harmonics), and the sound intensity scale used for this purpose is given in dBA units.

Occupational exposures to noise are compared against a Threshold Limit Value established by the Occupational Safety and Health Administration. The Threshold Limit Value is the sound level to which a worker may be exposed for a specified work period without probable adverse effects on hearing. The Threshold Limit Value for continuous noise is 85 dBA over 8 hours.

The Threshold Limit Value for impulse (impact) noise over 8 hours is not fixed because the daily allowed number of impulses depends on the level of each impulse. No individual impulse should exceed 140 dBA. An action level of 82 dBA for both continuous and impulse noise over an 8-hour workday has been established at LANL. Use of protective equipment is recommended above the action level (DOE 2004b).

I.4.5 Ecological Resources

This section addresses the ecological setting (that is, terrestrial resources, wetlands, and protected and sensitive species) of each of the technical areas listed in **Table I-83**. Also addressed are the potential transport and uptake of wastes by plants and animals. Although there are reaches of perennial streams on LANL, no fish species have been found within the LANL boundaries.

Table I-83 Summary of Material Disposal Area and Potential Release Sites Vegetation Zones

| <i>Technical Area</i> | <i>Site</i> | <i>Vegetation Zone</i> |
|-------------------------------|----------------------------|-------------------------|
| Material Disposal Area | | |
| 6 | F | Ponderosa pine |
| 8 | Q | Grassland |
| 15 | N | Ponderosa pine |
| 15 | Z | Grassland |
| 16 | R | Ponderosa pine |
| 21 | A | Ponderosa pine |
| 21 | B | Ponderosa pine |
| 21 | T | Ponderosa pine |
| 21 | U | Ponderosa pine |
| 33 | D | Juniper savannah |
| 33 | E | Pinyon-Juniper woodland |
| 33 | K | Pinyon-Juniper woodland |
| 35 | X | Ponderosa pine |
| 36 | AA | Pinyon-Juniper woodland |
| 39 | Y | Pinyon-Juniper |
| 49 | AB | Ponderosa pine |
| 50 | C | Ponderosa pine |
| 54 | G | Pinyon-Juniper woodland |
| 54 | L | Pinyon-Juniper woodland |
| Potential Release Site | | |
| 15 | Firing Site E-F | Grassland |
| 15 | Firing Site R-44 | Ponderosa pine |
| 16 | 260 Outfall (16-021(c)-99) | Ponderosa pine |
| 61 | Borrow pit | Ponderosa pine |
| 73 | Ashpile | Ponderosa pine |

Discussions of threatened and endangered species concentrate on those species for which Areas of Environmental Interest have been established. These include the Mexican spotted owl, bald eagle, and southwestern willow flycatcher. Areas of Environmental Interest have been

established in accordance with a habitat management plan. An Area of Environmental Interest essentially consists of a core zone containing important breeding or wintering habitat and a buffer zone around the core area. The buffer protects the area from disturbances that would degrade the value of the core zone (LANL 1998b). Ecological resources of LANL as a whole are described in Chapter 4, Section 4.5, and vegetation zones are shown in Chapter 4, Figure 4–25, of this SWEIS.

Ecological Resources of Technical Areas

Technical Area 6. TA-6 is located primarily within the Ponderosa Pine Forest vegetation zone, although areas along the north-facing slope of Sandia Canyon are included in the Mixed Conifer Forest zone. Vegetation typical of the Ponderosa Pine Forest zone includes ponderosa pine (*Pinus ponderosa* P&C Lawson), gambel oak (*Quercus gambelii* Nutt.), New Mexico locust (*Robinia neomexicana* Gray), and pine dropseek (*Blepharoneuron tricholepis* [Torr.] Nash). Located within the Ponderosa Pine Forest zone, MDA F is a grassy area of which portions are fenced; thus, its use by wildlife would be limited largely to birds, small mammals, and reptiles. Large mammals are excluded from much of the MDA because of fencing. The Cerro Grande Fire impacted TA-6 at severity levels varying from high to low-unburned. The portion of the TA containing MDA F burned at a low-unburned severity level (DOE 2000b). There are no wetlands within TA-6, although a narrow band of riparian vegetation exists along portions of the stream channel of Twomile Canyon.

The southeastern portion of TA-6 is within the core and buffer zones of the Pajarito Canyon Mexican spotted owl Areas of Environmental Interest. TA-6 does not fall within the Area of Environmental Interest for the bald eagle or southwestern willow flycatcher (LANL 2000c). MDA F is not in either the core or buffer zone of the Mexican spotted owl.

Technical Area 8. TA-8 falls primarily within the Ponderosa Pine Forest vegetation zone; however, the portion of the TA within which MDA Q is located is categorized as Grassland. Although the Cerro Grande Fire did not affect much of TA-8, its northeastern portion burned at a low-unburned severity level and a small area in the extreme northeast corner at a high severity level. That portion of the TA containing MDA Q burned at a low-unburned severity level (DOE 2000b). There are no wetlands or aquatic resources within the immediate vicinity of MDA Q, and no portion of TA-8 falls within any of the LANL Areas of Environmental Interest.

Technical Area 15. As is the case for TA-8, TA-15 is primarily located within the Ponderosa Pine Forest vegetation zone; however, areas within the central and southern part of the TA are classified as Grasslands. The Cerro Grande Fire affected about half of TA-15, burned at a low-unburned severity level. At this level, seed sources are expected to remain viable (DOE 2000b). MDA N and Firing Site E-F are located within the Grassland vegetation zone; however, all sites are grassy areas located near buildings and roads. One linear wetland is located in TA-15 within Threemile Canyon; however, it is not close to any MDA or firing site. This wetland is 0.3 acre (0.1 hectare) in size and contains Baltic rush (*Juncus balticus* Willd.) and a number of grasses (ACE 2005).

Portions of TA-15 are within the Pajarito Canyon, Threemile Canyon, and Water Canyon-Cañon de Valle Mexican spotted owl Areas of Environmental Interest. Core areas generally include the

canyons, while buffer zones include some of the mesas. The areas containing the two firing sites do not include either the core or the buffer zones for any of the spotted owl Areas of Environmental Interest. However, MDAs N and Z are within the buffer zone of the Water Canyon-Cañon de Valle Area of Environmental Interest, with a small portion of MDA Z within the core zone. Areas of Environmental Interest for the bald eagle and southwestern willow flycatcher do not include any portion of TA-15 (LANL 2000c).

Technical Area 16. Vegetative cover within TA-16 is largely ponderosa pine; however, an area of grassland occurs within the west-central part of the TA, and a mixed conifer forest occurs along north-facing slopes of Cañon de Valle and Water Canyon. Most development within TA-16 has occurred within the Ponderosa Pine Forest vegetation zone. Although the western part of the TA was not burned during the Cerro Grande Fire, most of the remaining area burned at a low-unburned severity level. However, the central part of the TA burned at a medium severity level (DOE 2000b). At this level, seed stocks can be adversely affected and erosion can increase because of the removal of vegetation and ground cover (DOE 2000b). Within the Ponderosa Pine Forest vegetation zone, MDA R and the 260 Outfall burned at a low-unburned severity level. Excepting those portions of MDA R and the outfall that are within and immediately adjacent to the High-Explosives Processing Area, both PRSs are in forested areas that provide habitat for species common to mixed conifer forests, including large mammals.

Two wetlands have been identified within TA-16; however, they are located a considerable distance to the east of MDA R and the 260 Outfall. These wetlands total 0.04 acre (0.02 hectare) in size and contain Baltic rush and various grasses (ACE 2005).

Only the eastern portion of TA-16 is within the Water Canyon-Cañon de Valle Mexican spotted owl Area of Environmental Interest. Additionally, a very small area on the northern border of the TA is within the buffer zone of the Pajarito Canyon Areas of Environmental Interest. MDA R and the 260 Outfall are not included in either Area of Environmental Interest. No part of the TA is included within Areas of Environmental Interest for the southwestern willow flycatcher or bald eagle (LANL 2000c).

Technical Area 21. About 20 percent of the TA is developed. Although most of TA-21 is within the Ponderosa Pine Forest vegetation zone, the more easterly portion of Los Alamos Canyon is within the Pinyon-Juniper Woodland zone. Wildlife within undisturbed portions of the TA would be typical of those two zones (DOE 1999a). The Cerro Grande Fire did not directly affect TA-21 (DOE 2000b). The MDAs are fenced grassy fields (except those portions of MDAs A and B that are covered with asphalt); thus, wildlife would be limited to birds, small mammals, and reptiles. Large mammals are excluded from the MDAs because of fencing. No wetlands have been identified within TA-21 (ACE 2005).

TA-21 is entirely within the Los Alamos Canyon Area of Environmental Interest, with the southern and eastern portions included within the core zone. The MDAs are located within developed areas of TA-21 that are within both the core and buffer zones of the Los Alamos Canyon Areas of Environmental Interest (LANL 2000c). TA-21 does not include any portion of the Areas of Environmental Interest for the bald eagle or southwestern willow flycatcher.

Technical Area 33. Although TA-33 is mostly within the Pinyon-Juniper Woodland vegetation zone, the eastern part of the TA is within the Juniper Savannah zone at lower elevations near the Rio Grande River. The TA is largely undeveloped. None of TA-33 was affected by the Cerro Grande Fire (DOE 2000b). Although only one small (0.01-acre [0.004-hectare]) wetland dominated by cattails (*Typha* spp.) is within the TA, the TA borders the region's most important aquatic resource, the Rio Grande (ACE 2005). MDAs D and K are within the Pinyon-Juniper Woodland vegetation zone, while MDA E is within the Juniper Savannah vegetation zone. All three MDAs are located away from the wetland and river.

Being located near the Rio Grande River, the eastern portion of TA-33 is within portions of the White Rock Canyon bald eagle Area of Environmental Interest. Yet of the three MDAs within the TA, only MDA D is within this Area of Environmental Interest; however, the MDA is within the core zone. Because bald eagles winter along White Rock Canyon adjacent to the Rio Grande, the Area of Environmental Interest is considered occupied from November through March.

Technical Area 35. TA-35 is entirely within the Ponderosa Pine Forest vegetation zone, but is a highly developed area. Yet the portions of the TA falling within Mortandad Canyon are in a natural state and thus contain wildlife typical of ponderosa pine forests. TA-35 burned at a low-unburned severity level during the Cerro Grande Fire (DOE 2000b). The only wetland present within TA-35 is located in the northwest corner of the TA and is an extension of a wetland primarily located in TA-55. This wetland is 1.2 acres (0.5 hectare) in size; coyote willow (*Salix exigua* Nutt.), cattail, Baltic rush, and various sedges (*Carex* spp.) are some of the species present (ACE 2005).

TA-35 is within the Pajarito Canyon and Sandia-Mortandad Canyon Mexican spotted owl Areas of Environmental Interest. While the southern portion of the TA is within the buffer zone of the former Area of Environmental Interest, the entire TA is within either the buffer or core zone of the latter Area of Environmental Interest.

Technical Area 36. TA-36 is the largest TA at LANL and encompasses both Pinyon-Juniper Woodland and Ponderosa Pine Forest vegetation zones. The TA is largely undeveloped and provides habitat suitable for species typical of both zones. Only the very northern portion of TA-36 was burned during the Cerro Grande Fire, at a low-unburned severity level (DOE 2000b). Although MDA AA is generally within the Pinyon-Juniper Woodland vegetation zone, it is within a developed portion of the TA. It therefore provides minimal wildlife habitat. Although not situated in the immediate area of MDA AA, a series of nine wetlands are within TA-36 along Pajarito Canyon. These wetlands total 15.2 acres (6.2 hectares). Plants found within these wetlands include coyote willow, Baltic rush, sedges, common spike rush (*Eleocharis palustris* (L.) Roemer & Schultes), American speedwell (*Veronica americana* Schwein. ex Benth), and cattail. There are no aquatic resources near MDA AA.

TA-36 includes portions of the buffer and core zones of the Pajarito Canyon, Threemile Canyon, and Water Canyon-Cañon de Valle Mexican spotted owl Areas of Environmental Interest. However, MDA AA is not within any of these three Areas of Environmental Interest (LANL 2000c).

Technical Area 39. Although most of TA-39 is in a Pinyon-Juniper Woodland vegetation zone, the northwestern part of the TA includes an area of grassland and ponderosa pine forest on the north-facing slopes of Water and Ancho Canyons. Because the area is largely undeveloped, wildlife typical of each vegetation zone is expected. TA-39 was not impacted by the Cerro Grande Fire (DOE 2000b). MDA Y is within the Pinyon-Juniper Woodland portion of the TA; however, it is a cleared area along Ancho Road that provides little wildlife habitat. There are no wetlands or aquatic resources in TA-39.

The northern portion of TA-39 includes both buffer and core zones of the Water Canyon-Cañon de Valle Mexican spotted owl Area of Environmental Interest. MDA Y is located in the central portion of the TA and does not fall within this Area of Environmental Interest (LANL 2000c).

Technical Area 49. TA-49 contains three separate vegetation zones—Ponderosa Pine Forest, Pinyon-Juniper Woodland, and Grassland. In general, Ponderosa Pine Forest is found on north-facing canyon slopes, while Pinyon-Juniper Woodland is present in the eastern quarter of the TA and Grassland occupies the remainder of the area.

The TA is largely in a natural state with a few scattered buildings at the Frijoles Mesa Site. Wildlife using the TA would include species typical of each vegetation zone. TA-49 was largely unaffected by the Cerro Grande Fire because only the northern edge of the TA burned at a low-unburned severity level (DOE 2000b). MDA AB is in the Frijoles Mesa Site in the central portion of the TA and is presently within the Grassland vegetation zone. The separate MDA AB areas are grass covered with scattered shrubs and trees. There are no wetlands within TA-49.

The northern part of TA-49 is within both the buffer and core zones of the Water Canyon-Cañon de Valle Mexican spotted owl Area of Environmental Interest. It does not include portions of the Areas of Environmental Interest for the bald eagle or southwestern willow flycatcher. The northern elements of MDA AB are within the buffer zone of the Mexican spotted owl Area of Environmental Interest (LANL 2000c).

Technical Area 50. TA-50 is within the Ponderosa Pine Forest vegetation zone. Although most of the area north of Pajarito Road has been developed, the area south of the road is in a more natural state. During the Cerro Grande Fire, the entire TA burned at a low-unburned severity level (DOE 2000b). Wildlife within undeveloped portions of the TA would be typical of ponderosa pine forests (DOE 1999a). MDA C is a relatively large grassy area that is fenced. Wildlife would be limited to small mammals, birds, and reptiles. There are no wetlands within TA-50.

TA-50 is within both the core and buffer zones of the Pajarito Canyon Mexican spotted owl Area of Environmental Interest and the buffer zone of the Sandia-Mortandad Canyon Area of Environmental Interest. MDA C falls within the buffer zone of both Mexican spotted owl Areas of Environmental Interest. TA-50 does not include portions of the Areas of Environmental Interest for the bald eagle or southwestern willow flycatcher (LANL 2000c).

Technical Area 54. TA-54 is primarily within the Pinyon-Juniper Woodland vegetation zone; however, a ponderosa pine forest occurs on the north-facing slope of Cañada del Buey. Wildlife using the TA would include species typical of both vegetation zones. Although most of the area

was untouched by the Cerro Grande Fire, the northwestern portion of the TA burned at a low-unburned to medium severity level. At a medium severity level, seed stocks can be adversely affected and erosion can increase because of the removal of vegetation and ground cover (DOE 2000b). MDAs G and L are disturbed areas having minimal ground cover, and each is enclosed by a fence. Thus, wildlife would be limited to small mammals, birds, and reptiles. Large mammals are excluded from the MDAs because of fencing. Although a series of wetlands occur along Pajarito Canyon (see the description of TA-36), none are found within any of the MDAs (Marsh 2001).

A portion of TA-54 is within the core and buffer zones of the southwestern willow flycatcher Areas of Environmental Interest; however, the Area of Environmental Interest is restricted to the canyon and does not include any part of the MDAs. Areas of Environmental Interest for the Mexican spotted owl and bald eagle do not encompass any part of TA-54 (LANL 2000c).

Technical Area 61. TA-61, including the borrow pit, falls within the Ponderosa Pine Forest vegetation zone. Although wildlife within undeveloped portions of the TA would be typical of ponderosa pine forests, the borrow pit lacks cover and therefore suitable habitat for wildlife. Most of TA-61 was unaffected by the Cerro Grande Fire. However, the very eastern portion of the TA, including the borrow pit area, burned at a low-unburned severity level (DOE 2000b). There are no wetlands or aquatic resources within the borrow pit site. However, the largest contiguous wetland on LANL, the Sandia wetland, is south of the Los Alamos County Landfill. This wetland is dominated by cattails. In 2000, it encompassed 3.5 acres (1.4 hectares), a 48 percent reduction in size from 1996; presently, it covers 3 acres (1.2 hectares) (Bennett, Keller, and Robinson 2001; ACE 2005).

TA-61 is within the buffer and core zones of both the Los Alamos Canyon and Sandia-Mortandad Canyon Mexican spotted owl Area of Environmental Interest. The borrow pit is within the buffer zone of the former and the core zone of the latter (LANL 2000c). TA-61 does not fall within the Area of Environmental Interest for the bald eagle or southwestern willow flycatcher (LANL 2000c).

Technical Area 73. TA-73 is covered by ponderosa pine forest and pinyon-juniper woodland in the east. Wildlife using the TA would include species typical of both vegetation zones such as mule deer and elk (DOE 1999a). The TA was not burned by the Cerro Grande Fire (DOE 2000b). There are no perennial surface watercourses within the TA. There are no wetlands in TA-73 (ACE 2005).

TA-73 is within the Los Alamos Canyon Mexican spotted owl Area of Environmental Interest. A small section of the southeastern part of the TA is within the core zone, while the remaining portions of TA-73 are within the buffer zone. TA-73 does not encompass any part of the Areas of Environmental Interest for the southwestern willow flycatcher or bald eagle (LANL 2000c).

Potential Transport and Uptake of Wastes

The ecological setting of the MDAs affects the potential for transport and uptake of radioactive and chemical constituents. Animals may burrow into disposal units, excavating contaminated materials and providing conduits for moisture to the waste. Plants can grow roots into disposal

units, incorporating contaminants that may be dispersed to surface soil when the plants defoliate. Plants can also reduce erosion of disposal unit covers and remove moisture from the soil that could otherwise percolate into disposal units. Typical plant species common to the Pajarito Plateau have average measured root depths ranging from less than 0.3 feet (0.1 meters) to greater than 5 feet (1.6 meters). Typical indigenous burrowing animals have average measured burrow depths ranging from about 0.3 feet (0.1 meters) to nearly 10 feet (3.0 meters) (LANL 1999b).

I.4.6 Human Health

Chapter 4, Section 4.6, of this SWEIS discusses measures taken at LANL to maintain the quality of human health for both workers and the public. Chapter 4, Figures 4–26 and 4–27 illustrate radiation doses to populations and maximally exposed individuals from 1993 through 2005.

I.4.7 Cultural Resources

Cultural resources are human imprints on the landscape and are defined and protected by Federal laws, regulations, and guidelines. Cultural resources within LANL and its region are classified as archaeological resources, historic buildings and structures, and traditional cultural properties. Cultural resources at LANL are addressed in Chapter 4, Section 4.7, of this SWEIS. This section summarizes the cultural resources of each of the technical areas addressed in Section I.4.1.1. Cultural resources are not expected within the MDAs themselves because all MDAs are highly disturbed areas.

I.4.7.1 Archaeological Resources and Historic Buildings and Structures

Technical Area 6. Twelve archaeological resource sites have been identified within TA-6. These sites include rock features, an artifact scatter, a one- to three-room structure, structures, wagon road segments, water control features, and a fence. Four of the 12 archaeological sites are eligible for listing in the National Register of Historic Places, 5 are of undetermined status, and 3 are not eligible. There is one historic structure eligible for listing in the National Register of Historic Places, the “concrete bowl” in TA-6. There are seven cultural resource sites in the vicinity of MDA F.

Technical Area 8. TA-8 contains 11 archaeological sites, including lithic scatters, a wagon road segment artifact scatters, a lithic and ceramic scatter, and a historic structure. Of these sites, four are eligible for listing in the National Register of Historic Places, 1 is of undetermined eligibility, 1 is not eligible, and 5 have not been evaluated for their eligibility. Six historic buildings in TA-8 are eligible for listing in the National Register of Historic Places. Three are located near MDA Q. Only one cultural resource site is in the vicinity of MDA Q.

Technical Area 15. TA-15 contains numerous cultural resource sites; thus, this section identifies only those sites within about a 1,000-foot (305-meter) radius of each MDA and firing site. There are 9 archaeological sites in the vicinity of MDA N, 7 sites in the vicinity of MDA Z, 11 sites in the vicinity of Firing Site E-F, and 3 sites in the vicinity of Firing Site R-44. These sites include Pueblo roomblocks, a plaza Pueblo, a water control structure, one- to three-room structures, cavates, a lithic scatter, and a rock shelter. Of these features, thirteen are eligible for listing in the National Register of Historic Places, 4 are not eligible, and 14 have yet to be formally assessed

for their eligibility. Two historic buildings in TA-15 are eligible for listing in the National Register of Historic Places. One of these buildings is within the R-44 SWMU. However, there are 26 additional significant buildings that have yet to be assessed for National Register of Historic Places eligibility.

Technical Area 16. Although TA-16 contains a fairly large and diverse number of cultural resource sites, only two are in the vicinity of MDA R and the 260 Outfall. One site is a lithic scatter of undetermined prehistoric affiliation. One site is an archaeological site that has not been formally evaluated for National Register of Historic Places eligibility, but is considered not eligible for listing. However, there is a historic process building that is eligible and is situated about 1,300 feet (400 meters) south of MDA R and the 260 Outfall. There are also other archaeological sites and National Register of Historic Places-eligible buildings within the TA, but none are in the vicinity of MDA R or the 260 Outfall.

Technical Area 21. Five archaeological sites have been identified within TA-21. These sites include a cavate, a rock shelter, trails or stairs, and an enclosure. These sites are eligible for listing on the National Register of Historic Places. One of the historic trails passes close to MDA B. Sixteen buildings and structures eligible for listing in the National Register of Historic Places are located within TA-21, a number of which are near the MDAs.

Technical Area 33. Similar to TA-15, TA-33 contains numerous cultural resource sites. Thus, the following discussion addresses only those resources in the vicinity of each MDA. There is one archaeological site near MDA D, six near MDA E, and three near MDA K. Archaeological sites in the vicinities of the MDAs include Pueblo roomblocks, one- to three-room structures, a lithic scatter, a cavate, rock shelters, and rock features. Four of these sites are eligible for listing in the National Register of Historic Places, one is not eligible, and two are of undetermined eligibility. Seven National Register of Historic Places-eligible buildings and structures are in TA-33. Additionally, there are other potentially significant historic buildings that have not yet received eligibility assessments.

Technical Area 35. TA-35 does not contain any known archaeological sites, but does include one building eligible for listing in the National Register of Historic Places. There are other potentially significant historic buildings that have not been assessed for National Register of Historic Places eligibility.

Technical Area 36. Because TA-36 contains numerous archaeological sites, only those resources within the vicinity of MDA AA are addressed. The three cultural resource sites identified near MDA AA include a one- to three-room structure, a rock shelter, and lithic and ceramic scatters. None of the sites have been formally assessed for eligibility for listing in the National Register of Historic Places; however, without further evaluation, one is deemed to be eligible and the other two are deemed to be of undetermined eligibility. One structure, north of MDA AA, is eligible for listing on the National Register of Historic Places. There are other potentially significant historic buildings that have not been assessed for National Register of Historic Places eligibility.

Technical Area 39. TA-39 is the second largest TA at LANL and contains numerous archaeological sites; thus, only those in the vicinity of MDA Y are addressed. Seven archaeological sites are in or near MDA Y. These resources include lithic and ceramic scatters,

rock features, cavates, and a rock shelter. None of the sites have been formally determined to be eligible for listing in the National Register of Historic Places; however, they are all deemed eligible or potentially eligible for listing. To date, no building or structure in TA-39 has been formally determined eligible for listing in the National Register of Historic Places. However, there are other potentially significant historic buildings that have not yet been reviewed for eligibility.

Technical Area 49. As with other large TAs on LANL, TA-49 contains numerous archaeological sites; thus, only those resources in the vicinity of MDA AB are summarized in this section. Forty-four archaeological sites are near MDA AB and include rock art, rock features, rock shelters, lithic scatters, one- to three-room structures, Pueblo roomblocks, and plaza Pueblos. Twelve of the 44 cultural resource sites have been formally declared eligible or potentially eligible for listing on the National Register of Historic Places, 1 is not eligible, and 31 are of undetermined status. Two buildings eligible for listing in the National Register of Historic Places are in TA-49; both are in the general vicinity of MDA AB. There is one additional potentially significant historic building that has not yet been assessed for eligibility.

Technical Area 50. TA-50 contained a single archaeological site and historic structure south of MDA C that was eligible for listing on the National Register of Historic Places. This site has been excavated. Currently, there are no buildings or structures in TA-50 eligible for listing. However, there are several potentially significant historic buildings that have yet to be reviewed for National Register of Historic Places eligibility.

Technical Area 54. Because TA-54 has many cultural resource sites, only those resources within the vicinity of MDAs G and L are addressed. There are 22 cultural resource sites near MDA G and 10 near MDA L. Of the cultural resource sites near MDA G, 7 have been excavated within the MDA area and 1 partially excavated within Zone 4. Fifteen of the sites are eligible for listing on the National Register of Historic Places. The 10 sites near MDA L are also eligible for listing on the National Register of Historic Places. Sites include lithic scatters, rock art, rock shelters, cavates, Pueblo roomblocks, plaza Pueblos, one- to three-room structures, and pit structures. Twenty-eight sites are eligible for listing in the National Register of Historic Places. A number of prehistoric sites were within MDA G; however, these were examined by archaeologists before its development. No buildings or structures in TA-54 have been evaluated for National Register of Historic Places eligibility. There are, however, four potentially significant historic buildings within TA-54.

Technical Area 61. TA-61 contains six archaeological sites. These sites include a trail and stairs, a number of cavates, and a historic structure. Four of the archaeological sites are eligible for listing in the National Register of Historic Places. Two sites are of undetermined eligibility. There are no cultural resources in the immediate vicinity of the borrow pit. No buildings or structures within TA-61 are eligible for listing in the National Register of Historic Places.

Technical Area 73. Nine archaeological sites have been identified within TA-73, including lithic and ceramic scatters, a cavate, a one- to three-room structure, a Pueblo roomblock, garden plots, and trails or stairs. Four of the archaeological sites are eligible for listing in the National Register of Historic Places. Two are not eligible, and three are of undetermined status. None of the cultural resource sites within TA-73 are near the ashpile. Two historic buildings within

TA-73 are eligible for listing on the National Register of Historic Places. One of these, a storage building, is in the vicinity of the ashpile. There are several other potentially significant historic buildings within TA-33 that have yet to be assessed for National Register of Historic Places eligibility.

I.4.7.2 Traditional Cultural Properties

A traditional cultural property is a significant place or object associated with historical and cultural practices or beliefs of a living community rooted in the community's history and is important in maintaining the community's continuing cultural identity. Within LANL's boundaries, there are ancestral villages, shrines, petroglyphs, sacred springs, trails, and traditional use areas that could be identified by Pueblo and Athabascan communities as traditional cultural properties. See Chapter 4, Section 4.7.3, for a discussion of traditional cultural properties. Some of the cultural resources addressed above may also be considered important in maintaining the continuing cultural identity of the local pueblo communities and so are considered traditional cultural properties.

I.4.8 Socioeconomics and Infrastructure

Socioeconomics and infrastructure are addressed in Chapter 4, Section 4.8, of this SWEIS and summarized below.

I.4.8.1 Socioeconomics

Socioeconomic impacts are defined in terms of changes to the demographic and economic characteristics of a region. The number of jobs created could affect regional employment, income, and expenditures. Job creation is characterized by (1) construction-related jobs that tend to be short in duration and transient, and thus less likely to impact public services; and (2) operation-related jobs that would last longer and could thus create additional service requirements. Chapter 4, Section 4.8.1, of this SWEIS summarizes, in the LANL region, economic characteristics, demographic characteristics, regional income, housing, local transportation, and the growth in recent years of the LANL-affiliated workforce. LANL currently has about 13,500 employees. These employees have had a positive economic impact on northern New Mexico.

I.4.8.2 Infrastructure

Site infrastructure includes the physical resources required to support the construction and operation of LANL facilities (see Chapter 4, Section 4.8.2). Utility infrastructure encompasses the electrical power, natural gas, steam, and water supply systems at LANL. Electrical service to LANL is supplied through a cooperative arrangement with Los Alamos County, the Los Alamos Power Pool. DOE operates a natural-gas-fired steam and electrical power generating plant within TA-3, capable of producing up to 20 megawatts of power. The natural gas system includes a high-pressure main and distribution system to Los Alamos County and pressure-reducing stations at LANL buildings. Over 90 percent of the gas used at LANL is used for heating. The Los Alamos water production system consists of 14 deep wells, 153 miles (246 kilometers) of main

distribution lines, pump stations, and storage tanks. The system supplies potable water to all of the county, LANL, and Bandelier National Monument.

I.4.9 Waste Management

LANL has a well-developed infrastructure and extensive facilities for managing radioactive, toxic, and hazardous materials. Many facilities are in TA-50 and TA-54 and include treatment of liquid radioactive and hazardous wastes; solid radioactive waste through measures such as dewatering or compaction; hazardous wastes (particularly characteristic wastes) through methods such as neutralization or reaction to eliminate reactivity concerns; and high explosive-contaminated material, often by burning. LANL has facilities to characterize the radioactive and hazardous content of the waste. Some wastes are stored onsite, including some low-level radioactive, TSCA, and hazardous wastes, as well as transuranic wastes. Stored transuranic wastes are being retrieved for repackaging and shipment to WIPP. Additional information is in Chapter 4, Section 4.9, of this SWEIS.

Solid waste disposal capacity will exist at LANL on a temporary basis. LANL and Los Alamos County have both used a solid waste landfill located within TA-61. Established in 1974, the landfill must close to comply with solid waste management regulations administered by NMED (LANL 2005d). The landfill is expected to operate through fall 2008 (Finrock 2008). A solid waste transfer station located at the existing county landfill is to open at that time. Access to the landfill is via East Jemez Road (LANL 2005d). LANL nonhazardous waste will be processed through this new transfer station, and municipal and LANL waste will be transported to a location outside of Los Alamos County. Waste will be collected, processed, and transferred into larger trucks before being shipped offsite. Management and operation of the transfer station will be by Los Alamos County (LANL 2005a).

The only operating low-level radioactive waste disposal facility at LANL is at Area G in TA-54. Disposal of mixed low-level radioactive waste is not authorized, although disposal of waste containing PCBs occurs. Low-level radioactive waste disposal operations will be expanded initially into Zone 4 of TA-54, an expansion of about 30 acres (12 hectares), and then as necessary into Zone 6 of TA-54 (72 acres total). This expansion was addressed in Volume II (*Project-Specific Siting and Construction Analyses*) of the 1999 SWEIS (DOE 1999a) (see Appendix H, Section H.3). The disposal units at Zone 4 would contain shafts for wastes requiring special controls (such as remote-handled-waste or wastes containing biological hazards or PCBs), as well as several pits or trenches for routine wastes. Assuming a delivery rate of 2,600 to 3,900 cubic yards (2,000 to 3,000 cubic meters) of waste per year, Zone 4 should be able to provide disposal capacity for 40 to 60 years (LANL 2005h).

I.4.10 Transportation

Motor vehicles are the primary means of transportation at LANL (see Chapter 4, Section 4.10). Principal access routes to each of the MDAs and PRSs listed in Table I-80 are listed in **Table I-84**. The principal access road to the TA-61 borrow pit is East Jemez Road.

Table I–84 Principal Access Routes to Material Disposal Areas and Selected Solid Waste Management Units

| <i>TA</i> | <i>MDA or SWMU</i> | <i>Principal Access</i> | <i>Comments</i> |
|-----------|------------------------------|-------------------------|---|
| 6 | MDA F | Twomile Mesa Road | Terminates in TA-40 to the west; intersects with Anchor Ranch Road and West Jemez Road (NM 501) to the east. |
| 8 | MDA Q | Anchor Ranch Road | Intersects with West Jemez Road to the southwest. |
| 15 | MDA N | R-Site Road | Intersects with Anchor Ranch Road to the west. Anchor Ranch Road intersects with West Jemez Road to the southwest. |
| 15 | MDA Z SWMUs E-F, R-44 | | Intersects with R-Site Road to the north. |
| 16 | MDA R | K-Site Road | Intersects with Anchor Branch Road. |
| 16 | SWMU 260 Outfall | K-Site Road | Intersects with Anchor Ranch Road. |
| 21 | MDAs A, B, T, U | DP Road | Intersects just to the west of TA-21 with NM 502 in the Los Alamos Townsite. |
| 33 | MDAs D, E, K | NM 4 | |
| 35 | MDA X and other nearby SWMUs | Pecos Drive | Intersects with Pajarito Road in TA-50. |
| 36 | MDA AA | Potrillo Drive | Intersects with Pajarito Road in TA-18. |
| 39 | MDA Y | NM 4 | |
| 49 | MDA AB | Frijoles Mesa Drive | Intersects with NM 4 to the west. |
| 50 | MDA C | Pajarito Road | Passes through TA-50 and intersects with NM 501 (East and West Jemez Roads) to the east and NM 4 to the west. |
| 54 | MDAs G and L | Mesita del Buey Road | Intersects with Pajarito Road in the northern area of TA-54. Pajarito Road intersects with NM 501 (East and West Jemez Roads) to the east and NM 4 to the west. |
| 73 | Ashpile | East Road | |

TA = technical area, MDA = material disposal area, SWMU = solid waste management unit, NM = New Mexico.

Figure I–25 shows many of the principal transportation routes within LANL. Materials such as concrete or fill dirt could be delivered using NM 4 to the west or NM 502 to the east. Waste and materials moved within LANL would be transported mainly over NM 501 (East and West Jemez Roads), NM 502, NM 4, and Pajarito Road. Much of the waste sent offsite from LANL for treatment or disposal may be transported over NM 502 to the east (**Figure I–26**). NM 502 intersects with NM 30 in San Ildefonso. NM 30 passes north to Española. NM 502 continues east, intersecting with US 285/84. US 285/84 is routed north to Española and south to Santa Fe, where it intersects with I-25. A new Santa Fe bypass connects with US 285/84 north of Santa Fe and passes to the northwest of Santa Fe, connecting with I-25 west of Santa Fe. I-25 connects with I-40 in Albuquerque to the south.

The primary route designated by the State of New Mexico for radioactive and other hazardous material shipments to and from LANL is the 40-mile (64-kilometer) corridor between LANL and I-25 at Santa Fe. This route passes through the Pueblos of San Ildefonso, Pojoaque, Nambe, and Tesuque and along the northern segment of Bandelier National Monument (DOE 1999a).

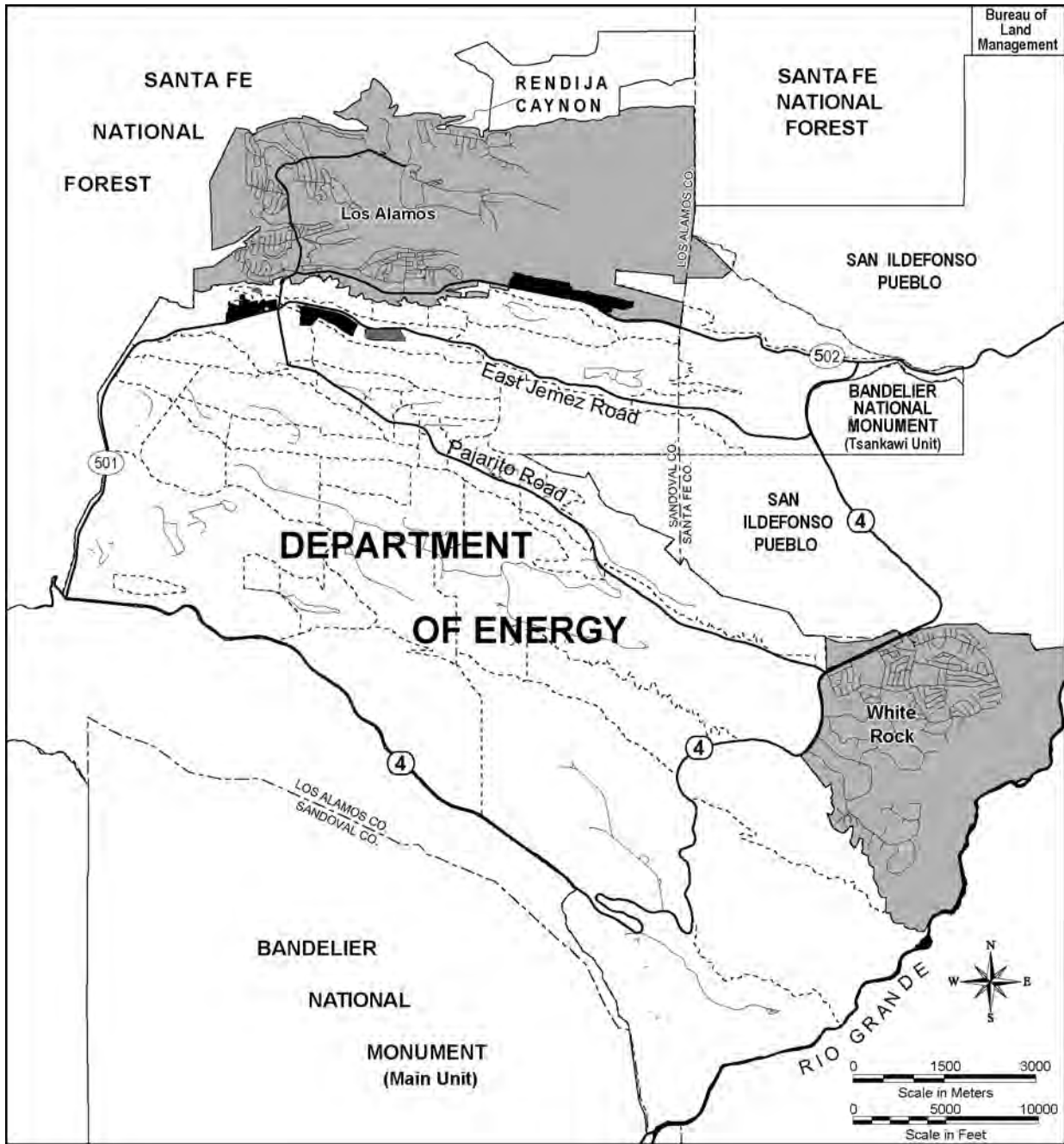


Figure I-25 Major Transportation Routes within Los Alamos National Laboratory

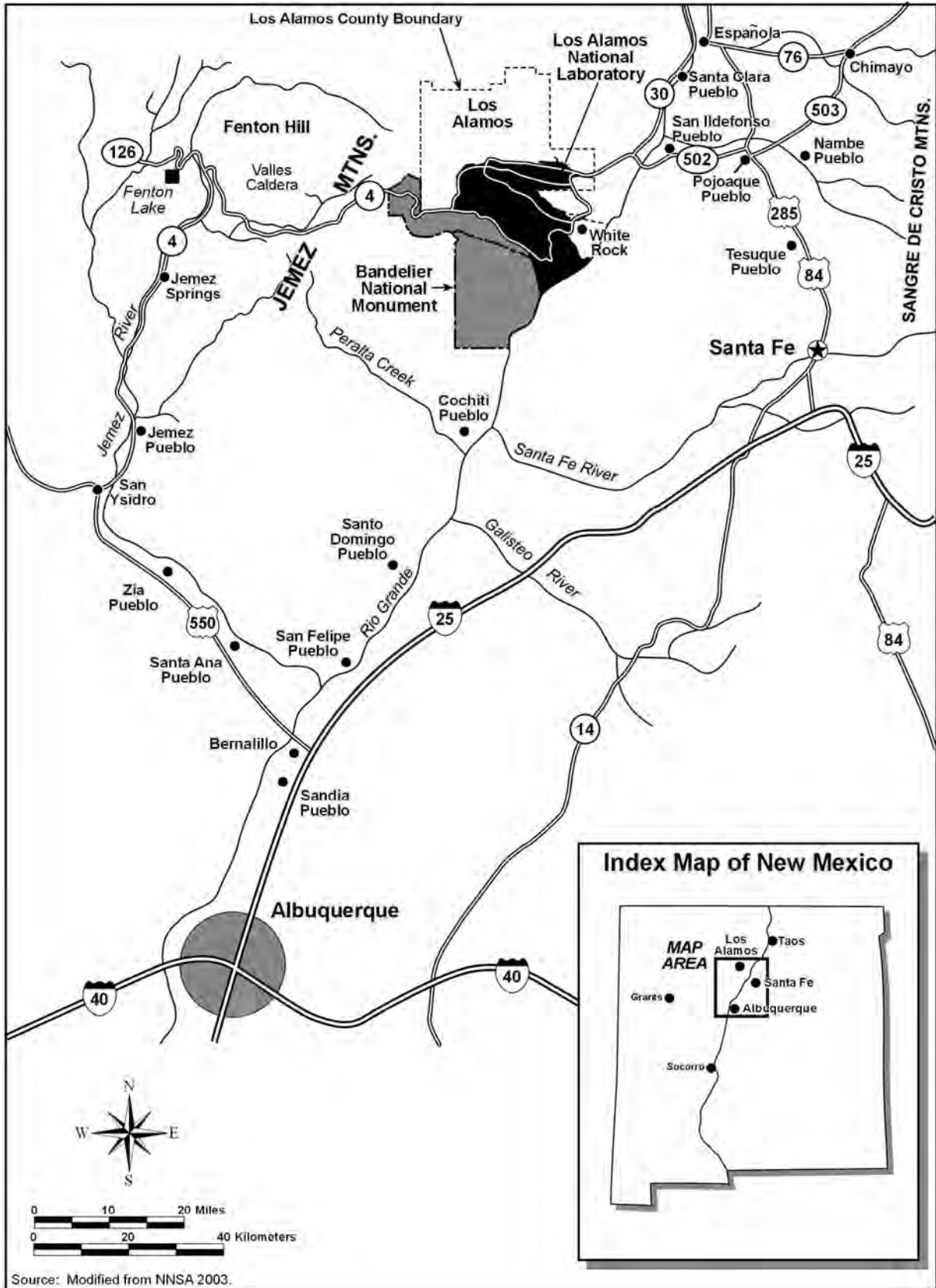


Figure I-26 Major Transportation Routes Outside of Los Alamos National Laboratory

I.4.11 Environmental Justice

As summarized in Chapter 4, Section 4.11, of this SWEIS, a majority of residents (54 percent) in the eight potentially affected counties surrounding LANL designated themselves as minorities in the 2000 Census. Hispanics and American Indians composed approximately 91 percent of the minority population. The percent of low-income population residing in these counties was reported to be approximately 13 percent in the 2000 census, compared to nearly 18 percent of the total population of New Mexico.

Estimates of transportation impacts are based on an assumed route from LANL heading east on NM 502 and south toward I-25 passes through San Ildefonso, Pojoaque, Nambe, and Tesuque Pueblo lands.

The Pueblo of San Ildefonso is a minority-dominated community and had a median household income of \$30,457 in the 2000 census. About 12.4 percent of the families lived below the poverty level. The median household income in Pojoaque was \$34,256, with 11.3 percent of families living below the poverty level (DOE 2004b).

I.5 Environmental Consequences

The major options considered in this appendix are No Action, Capping, and Removal. As the LANL environmental restoration project continues, so do operational and decommissioning activities at LANL. These activities may have environmental benefits and detriments, and will generate wastes requiring treatment and disposal. DD&D of structures in TA-18 and TA-21 is addressed in Appendix H, Sections H.1 and H.2. Wastes projected from recovery of transuranic waste from storage are addressed in Section H.3. Total wastes from all sources are addressed in Chapter 5, Section 5.9, of this SWEIS.

I.5.1 Land Resources

Resources include land use and the visual environment (physical characteristics, air quality, light pollution).

I.5.1.1 No Action Option

Under the No Action Option, LANL would continue its environmental restoration project at levels as described for the Expanded Operations Alternative in the *1999 SWEIS* (DOE 1999a).

I.5.1.1.1 Land Use

Continuing LANL's environmental restoration project would reduce the amount of land and property at LANL that is contaminated with radioactive or hazardous constituents. There would be a wider range of options for future use of this land and property. However, many, if not most, of the PRSs being addressed under LANL's environmental restoration project are near other operating facilities. Operation of these facilities, and the missions conducted within the TAs containing these facilities, are largely independent of remediation actions for individual PRSs. Therefore, continuing the environmental restoration project would probably not change many basic restrictions such as control of access to LANL and particular TAs. Restrictions would

probably continue consistent with security or safety needs. Nonetheless, within the context of the overall LANL mission and that for particular TAs, continuing the environmental restoration project could result in expanded options for some lands and property.

I.5.1.1.2 Visual Environment

Continuing LANL's environmental restoration project should generally improve visual resources as older structures and signage warning of possible hazards are removed for lack of need, and areas are revegetated. But there could be some temporary, short-term reductions in the visual environment. For example, vegetative covers over small portions of land being remediated may be removed. But this visual effect would be temporary until vegetation is restored. Small quantities of dust could be generated, which could slightly reduce visual quality. But dust generation would be localized and temporary and could be mitigated.

But the large domes at Area G in TA-54 would remain until operations associated with the domes (such as transuranic waste storage) are completed. The domes contrast with the natural landscape and can be seen from the Nambe-Española area, from areas in western and southern Santa Fe, and from lands of the San Ildefonso Pueblo. Recovery of aboveground stored waste is planned for completion by the end of FY 2012. DD&D of structures in Area G will be performed in three phases during FY 2010, FY 2012, and FY 2014, to be completed early in FY 2015 (see Appendix H, Section H.3, of this SWEIS).

I.5.1.2 Capping Option

I.5.1.2.1 Land Use

Site Investigations. Consent Order investigation programs such as well installation and monitoring will not change the designated land use in the TAs where the investigations take place. Wells or other monitoring equipment should not require significant dedication of land once installed. However, there may be temporary commitments of land to construct the investigation systems. For example, installation of a well may require temporary clearing of several hundred square feet of vegetation. But this resource commitment would be short lived. Following well installation, the affected land would be allowed to return to its original condition.

Remediation of MDAs. Because the Capping Option would stabilize rather than remove existing contamination, future use of the MDAs would remain restricted. At present, most MDAs are open areas that are fenced and excluded from any use other than safely maintaining inventories of waste. In the future, the MDAs would continue to be surveyed and maintained to protect public health and safety and the environment.

Although 37 acres (15 hectares) of TA-21 either have been or will be conveyed to Los Alamos County, conveyance of most of TA-21 has been deferred. Many of the structures in TA-21 will be removed (see Appendix H, Section H.2). Yet because capping would stabilize rather than remove existing contamination, development within the TA would be restricted. The MDAs are within areas designated as No Development Zone (Hazard). This designation is expected to continue under the Capping Option.

Capping the MDAs within TA-54 would result in no significant change to current restrictions on accessing the land comprising the MDAs. Overall, those portions of TA-54 currently used as waste management areas would still be used for that purpose. If some of the transuranic waste currently stored in the Area G shafts is left in place (see Section I.3.3.2.1.2.2), then long-term institutional controls (which include land use restrictions, signage, and other controls) may be needed, as called for in 40 CFR Part 191.

The Capping Option would maintain the commitment of roughly 110 acres (45 hectares) of land as waste disposal areas. In addition, the Capping Option would involve the temporary commitment of land to support capping activities; following capping, the land would be remediated as needed and made available for other uses. As addressed in Section I.3.6.5, temporary support areas may include project management areas, areas for parking personal vehicles, areas for temporarily storing any wastes that may be generated, and areas for stockpiling bulk materials. Project management areas are expected to be small, involving total commitment of only a few acres for all MDAs. For most MDAs, personal vehicles could probably be parked at existing facilities; little additional parking capacity should be needed. Because capping MDAs is expected to generate only small quantities of waste, only a few acres would be temporarily affected as waste storage areas.

The largest temporary commitment of land would be for temporary storage of bulk capping materials. Assuming that capping requires the temporary storage of a 6-month supply of materials at each MDA, then 37 to 81 acres (15 to 33 hectares) of land could be temporarily affected.⁷⁵

Remediation decisions at the MDAs may involve a combination of measures (some portions capped; some portions removed). Activities at TA-21 will include DD&D as well as MDA remediation, which may in combination temporarily affect up to 130 acres (53 hectares).

Remediation of Other PRSs. Removal of contamination at PRSs such as Firing Sites E-F and R-44 at TA-15 would probably not result in significant changes in land use. Remediating the firing sites would not independently change the operational mission assigned to TA-15, and the land use classification would remain High-Explosive Testing. Remediating the 260 Outfall would result in no change in land use; TA-16 is expected to remain as LANL's high explosive processing area, with attendant security restrictions. Similarly, action to remediate groundwater and surface water contamination within canyons (or elsewhere) would not by itself change current land use within the TAs containing these canyons.

Remediation of PRSs may directly affect several acres of land on an annual basis, assuming that remediation involves removal of contamination from the affected area. Additional acreage may be temporarily committed to support remediation. For example, removal operations at surface contamination sites such as firing sites may require the temporary establishment of management areas (including management trailers) or waste storage and processing areas. Remediation of subsurface volatile organic compound plumes will require temporary commitment of small quantities of land for extraction or offgas treatment systems. Installation of subsurface barriers such as slurry walls or permeable reactive barriers will require temporary areas for project

⁷⁵ Includes capping contaminated areas in TA-49.

management, equipment parking, and bulk materials storage. Possible installation of groundwater pump-and-treat systems may require a temporary commitment of land for equipment installation. Operation of the systems would require temporary dedication of land for pumping equipment, treatment systems, plumbing, and temporary water storage.

Borrow Pit. Use of the borrow pit on East Jemez Road in TA-61 as a source for capping materials would result in no changes to the current land use category for the TA (Physical and Technical Support and Reserve).

I.5.1.2.2 Visual Environment

Site Investigations. Consent Order investigation programs will have some visual impacts. There would be temporary clearing or vegetation disruption to construct the investigation systems. Installing a well may require temporary clearing of several hundred square feet of land. But visual impacts would be short lived. Cleared or disrupted areas would be allowed to return to their original condition. Site monitoring and sample collection systems would be unobtrusive.

Remediation of MDAs. Capping the MDAs would have short-term visual impacts. It would require stripping or disrupting the existing vegetative cover over the MDAs, placing cover materials in compacted lifts, and providing for revegetation. But not all land would be affected at the same time, and many of the MDAs are not readily visible by the public.

The Capping Option would involve placement of final covers on up to 110 acres (45 hectares) of LANL property containing MDAs and landfills. However, because capping would take place over a period of 10 years of different times within different TAs, a much smaller area would be affected during any single year. In addition to presenting a disturbed appearance, there could be temporary visual impacts of suspended dust. These impacts could be mitigated using water sprays or other techniques.

In addition, there would be areas temporarily affected by support operations needed to construct the caps. In addition to small project management areas for MDAs requiring remediation, there would be areas used by site workers for parking personal vehicles, as well as areas used for temporary management of waste or demolition debris, or temporary storage of bulk materials such as crushed tuff. These areas would have an industrial appearance. However, it is probable that most of the areas so affected would be in previously disturbed areas, and because most MDAs are near existing LANL facilities, parking areas may already largely exist, meaning no change in existing appearance.

The average affected will depend on regulatory decisions, operational needs, and related LANL activities. Remediation decisions for the MDAs may involve a combination of measures. Activities at TA-21 will include DD&D as well as MDA remediation, which may temporarily impact up to 130 acres (53 hectares).

After capping is completed for most MDAs, there would be only minor changes in visual resources. Once the MDAs are capped, those visible from higher elevations to the west would have the same grassy appearance as they had before capping began. Support areas would be remediated as needed. But similar to the No Action Option, there would be a noticeable

improvement at Area G within TA-54, where a grassy field would eventually replace the visually intrusive white domes. This replacement would improve views from the Jemez Mountains, the Pueblo of San Ildefonso, and as far away as the towns of Española and Santa Fe.

If some of the transuranic waste currently stored in the Area G shafts is left in place (see Section I.3.3.2.1.2.2), then long-term institutional controls may be needed as called for in 40 CFR Part 191. Passive institutional controls would include markers or other devices intended to warn against unauthorized intrusion into the disposal area, and these markers or devices, which would be designed to be long lasting, may be visible at a distance.

Remediation of Other PRSs. Visual impacts associated with remediating other PRSs would depend on their location and the nature and extent of the contamination. For example, the firing sites in TA-15 are in a restricted, wooded area. Because removal of contamination would involve surface recovery rather than excavation, minimal damage to existing vegetation would probably occur. Remediating the 260 Outfall would require partial clearing and excavating some areas. Any visual impacts of dust or particulate matter that may be suspended from remediation operations could be mitigated. Remediation of subsurface volatile organic compound plumes would require installation of vapor removal and treatment systems that would be small and visually unobtrusive. Installation of subsurface barriers such as slurry walls or permeable reactive barriers would require temporary disruption of land, but affected land could be revegetated as needed. Possible use of groundwater pump-and-treat systems may result in a temporary industrial appearance at the remediation sites, given the possible need for pumping equipment, treatment systems, plumbing, and temporary water storage. These systems should be relatively compact, however.

In any event, several acres of land may be annually visually affected through continued remediation of dozens of LANL PRSs. Individual affected areas would be generally small, and many would be in locations not routinely accessed by the public. Once remediation is complete, the affected areas would quickly return to a similar appearance, when viewed from afar, to that before remediation was initiated.

Borrow Pit. Visual impacts may be associated with operation of the borrow pit in TA-61 to provide fill for MDA capping. Quantities of fill and other materials needed to cap the MDAs would be large. To obtain the required fill, the small hill that currently screens the pit from observation from East Jemez Road may require removal. Thus the pit, which is a cleared area several acres in size, may become visible from East Jemez Road. There could also be visual impacts of suspended dust from borrow pit operation. These impacts could be mitigated using water sprays or other techniques. (See Section I.5.4.2.1 for an estimate of the quantities of dust raised from borrow pit operation.)

I.5.1.3 Removal Option

I.5.1.3.1 Land Use

Site Investigations. Impacts on land use under the Removal Option would be the same for site investigations as under the Capping Option.

Removal of MDAs. Under the Removal Option, there would be fewer restrictions on land use than under the Capping Option. Capping the MDAs is expected to cover about 110 acres (45 hectares) of land, which would be retained as exclusion areas for radioactive waste. Removing the MDAs could free the land occupied by the MDAs for other purposes. Any buffer area surrounding the MDAs could also be used for other purposes.

But implementation of the Removal Option may not cause major changes in the designated uses of the TAs containing MDAs. Operating or inactive contaminated facilities would remain near MDAs C, G, and L. Assuming complete removal at MDAs A, T, and U, there may be residual stabilized contamination after other, nearby, structures are removed (see Appendix H, Section H.2). After removal of MDA AB, other nearby PRSs in TA-49 may remain. A similar situation exists at the other, smaller, MDAs. While future use of the remediated sites is not yet known, it is likely that the land would be reused to support existing and future LANL missions.

The Removal Option would involve the temporary commitment of land to support removal operations; following removal, the land would be remediated as needed and be made available for other uses. Temporary support areas may include project management areas; areas for parking personal vehicles; areas for temporary storage of waste; capacity for storing bulk materials such as excavation spoil; and capacity for waste hazard identification, waste processing, or characterization. Project management area requirements will be probably small for most MDAs. Larger area commitments may be needed for removal of large MDAs such as MDA C or G. For most MDAs, personal vehicles could probably be parked at existing facilities. However, removal of MDA G could require a large work force, which may require development of additional capacity for vehicle parking.

It is expected that removing the MDAs could require up to 63 acres (25 hectares) for temporary storage or management of mostly low-activity bulk waste. Assuming that removing the MDAs requires the temporary storage of a 6-month supply of spoil, then the Removal Option would temporarily affect up to 99 acres (40 hectares) of land for bulk material storage. An additional 10 to 22 acres (4 to 9 hectares) would be temporarily affected for capping remaining disposal units in Area G and small areas in TA-49. Also, 84 acres (34 hectares) may be needed to site several hazard identification, waste processing, or characterization facilities around LANL. However, because removal would take place over a period of 10 years at different times within different TAs, smaller areas than those estimated above would be affected annually.

Remediation decisions for the MDAs may involve a combination of measures. Remediation will be coordinated with other LANL activities such as DD&D. Combined DD&D and MDA remediation at TA-21 may temporarily affect up to 130 acres (53 hectares).

Remediation of Other PRSs. The Removal Option is expected to have the same effect on land use for other LANL PRSs as the Capping Option.

Borrow Pit. The Removal Option is expected to have the same effect on land use for the TA-61 borrow pit as the Capping Option.

I.5.1.3.2 Visual Environment

Site Investigations. Visual impacts of the Removal Option would be the same for site investigations as under the Capping Option.

Remediation of MDAs. Under the Removal Option, many of the larger MDAs may be exhumed under enclosures similar to those used for transuranic waste recovery at TA-54. (The investigation and remediation program at MDA B will be conducted under enclosures.) These enclosures would be visible from greater distances than would the MDAs under the Capping Option, but their presence would be temporary. After waste removal is completed, the enclosures would be removed and the backfilled excavations revegetated. MDAs not exhumed under enclosures would present a disturbed appearance while removal takes place. However, after removal is complete, the excavations would be backfilled and revegetated.

As under the Capping Option, implementation of the Removal Option would temporarily visually affect land used to support removals. Support activities could include management and staging areas; waste inspection, treatment, packaging, and storage areas; equipment decontamination areas; parking areas for worker vehicles; and areas for bulk storage of materials such as exhumed soil. The amount of acreage so affected would depend on regulatory decisions, operational needs, and other LANL infrastructure and activities. Remediation decisions for the MDAs may involve a combination of measures, as contemplated for MDA B within TA-21. DD&D and MDA remediation within TA-21 may temporarily impact up to 130 acres (53 hectares).

The Removal Option would probably cause smaller visual impacts of suspended dust than the Capping Option. Waste removal at the larger MDAs may occur within enclosures, and air exhausted from these structures would be filtered.

Remediation of Other PRSs. The Removal Option is expected to have the same visual impacts for other LANL PRSs as the Capping Option.

Borrow Pit. Visual impacts may be associated with operation of the borrow pit in TA-61 to provide backfill for the excavated MDAs. Quantities of fill would be large and comparable to those required under the Capping Option (see Section I.5.1.2.2). To obtain the required fill, the small hill that currently screens the pit from observation from East Jemez Road may require removal. Thus the pit, a cleared area several acres in size, may become visible from East Jemez Road. The potential for visual impacts of suspended dust would be comparable to those under the Capping Option.

I.5.2 Geology and Soils

Resource areas of interest are: (1) the possibility of geological effects on MDAs and other PRSs; (2) soil contamination; and (3) the need for soil, rock, and similar materials for MDA remediation. Site investigations conducted under the Consent Order, as well as LANL surveillance and maintenance programs for nuclear environmental sites, should have little or no effect on these resource areas.

I.5.2.1 No Action Option

Under the No Action Option, concerns identified at the MDAs and all other PRSs at LANL from erosion or other mass-wasting processes would be addressed. But action to address the long-term protection of the MDAs from erosion and other possible mass-wasting damage would not occur consistent with the schedules in the Consent Order.

The environmental restoration project would continue to address contamination in soil or other media at the LANL PRSs. But the activities of LANL environmental restoration project activation would not necessarily be consistent with the schedules or priorities of the Consent Order.

The TA-61 borrow pit would continue to operate at existing levels.

I.5.2.2 Capping Option

Geological Effects. Covers for the MDAs would be contoured and provided with runoff and runoff control measures consistent with their design. In addition, soils adjacent to or beneath the waste may be affected by construction of vertical or subwaste horizontal containment walls. The final designs of the covers would follow completion of the corrective measure studies being performed for the Consent Order. The corrective measure studies would include conceptual models of each MDA that would consider long-term geologic processes such as cliff retreat.

Soil Contamination. Other than that existing as a gas or vapor, contamination within the subsurface of the MDAs and in the immediate vicinities would be fixed in place. Capping would not by itself address any contamination existing as vapor within soil, such as volatile organic compounds or tritium as a gas or vapor. However, soil vapor volatile organic compounds can be removed and treated using unobtrusive equipment that would be compatible with the installed evapotranspiration covers (see Section I.3.3.2.2.4). Remediation of the firing sites, the outfalls, and other PRSs would address existing soil contamination at these PRSs.

Borrow Pit. Under the Capping Option, the MDAs would be capped in place using evapotranspiration covers. To construct these covers, from 750,000 to 2,000,000 cubic yards (570,000 to 1,500,000 cubic meters) of crushed tuff may be needed through 2016, assuming that all such material is obtained from the TA-61 borrow pit. (From 370,000 to 930,000 cubic yards (280,000 to 710,000 cubic meters) of crushed tuff would be needed through 2011.) The site containing the borrow pit covers 43 acres (17 hectares). Assuming an excavation depth of 50 feet (15 meters), excavating 750,000 cubic yards (570,000 cubic meters) of tuff would create a hole 9.3 acres (3.8 hectares) in size, while excavating 2,000,000 cubic yards (1,500,000 cubic meters) of tuff would create a 50-foot (15-meter) hole roughly 25 acres (10 hectares) in size.

Alternatively, the required fill for the MDA covers may be partially obtained from offsite sources, at additional cost and transportation impacts. In addition to fill, construction of the MDA covers through 2016 would require 440,000 to 460,000 cubic yards (340,000 to 350,000 cubic meters) of additional rock, gravel, topsoil, and other bulk materials from local sources. The total quantity of crushed tuff, rock, and other bulk materials needed through 2016 would range from 1.2 to 2.5 million cubic yards (0.92 to 1.9 million cubic meters).

I.5.2.3 Removal Option

Geological Effects. Complete removal of the MDAs would eliminate concern about the susceptibility of the MDAs to erosion or other geological processes. For partial removal of MDAs, there would be residual, but reduced, concerns because high-concentration pockets of contamination would be removed.

Soil Contamination. This option would greatly reduce existing soil contamination in the vicinity of the MDAs. Contamination existing as a soil or gas would also be largely eliminated. Remediation of the firing sites, outfalls, sediments in canyons, and other PRSs would address existing soil contamination at these PRSs.

Borrow Pit. Under the Removal Option, the waste in all MDAs considered in this appendix would be removed. Roughly 1,300,000 cubic yards (990,000 cubic meters) of backfill would be needed to replace the excavated waste and contamination, as well as 61,000 cubic yards (47,000 cubic meters) of rock, gravel, topsoil, and other bulk materials obtained from local sources. In addition, from 190,000 to 510,000 cubic yards (150,000 to 390,000 cubic meters) of crushed tuff would be needed for capping the remaining disposal units at the existing Area G footprint in TA-54, plus 160,000 cubic yards (120,000 cubic meters) of additional bulk materials from local sources. Roughly 31,000 to 84,000 cubic yards (24,000 to 64,000 cubic meters) of crushed tuff, and 2,600 to 7,000 cubic yards (2,000 to 5,400 cubic meters) of additional materials may be needed to cap other landfills, and contaminated areas such as those in Areas 6 and 12 of TA-49. A total of 1.6 to 1.9 million cubic yards (1.2 to 1.5 million cubic meters) and about 220,000 cubic yards (170,000 cubic meters) of rock, gravel, and other bulk materials would be needed, or about 1.8 to 2.2 million cubic yards (1.4 to 1.7 million cubic meters) of combined tuff, rock, and other bulk materials.

Assuming that the crushed tuff would be obtained from the TA-61 borrow pit, then removal of up to 1,900,000 cubic yards (1,500,000 cubic meters) of material from the pit would create a 50-foot (15-meter) hole, 24 acres (9.7 hectares) in size. The demands on the borrow pit would be comparable to those under the Capping Option and could, again, be reduced by obtaining some backfill from other local sources.

I.5.3 Water Resources

Possible impacts on surface water and groundwater resources would be addressed as part of any required corrective measure evaluation to be performed for MDAs and other PRSs in accordance with the Consent Order. A corrective measure evaluation for an MDA would consider alternatives, including capping and removal, two bounding options for MDA remediation that are considered in this appendix.

I.5.3.1 No Action Option

I.5.3.1.1 Surface Water

Under the No Action Option, surface water quality would be gradually improved as continuing corrective measures are performed on LANL PRSs. There would be fewer risks to surface water because sources of contamination in soil and sediments would be stabilized in place or removed.

I.5.3.1.2 Groundwater

Gradual improvements to groundwater quality would occur.

Investigative and monitoring programs have long existed at LANL to assess the presence of contaminants, and to obtain information needed to predict impacts on water resources. Investigations have addressed radionuclide transport beneath pits at MDA G, tritium transport around disposal shafts at MDA G, volatile organic compound transport at MDA L and MDA G, and plutonium transport at MDA T. Investigations intended to characterize vadose zone hydrologic conditions have included injection well tests, natural tracer analyses, chloride measures, stable isotope measurements, and in situ moisture monitoring (LANL 1999b).

In compliance with an earlier version of DOE’s Radioactive Waste Management Order, DOE 435.1 (DOE 2001), a performance assessment and a composite analysis were issued in 1997 for the Area G low-level radioactive waste disposal facility in TA-54 (LANL 1997). The performance assessment addresses all waste projected to be disposed of at Area G following September 25, 1988, while the composite analysis addresses all sources of radioactive material within the disposal area that may cause impacts on a hypothetical future member of the public. The performance assessment and composite analysis are of interest because of the large inventory of radionuclides within Area G. The results of the analyses are summarized in **Table I-85** and represent projected exposures to members of the public over the next 1,000 years (LANL 1997).

Table I-85 Material Disposal Area G Performance Assessment and Composite Analysis Summary Results

| <i>Inventory</i> | <i>Analysis</i> | <i>Location</i> | <i>Calculated Peak Dose (millirem per year)</i> | <i>Performance Objective (millirem per year)</i> |
|------------------------|------------------------|----------------------------|---|--|
| Performance assessment | Air pathway | Cañada del Buey | 6.6×10^{-2} | 10 |
| Composite analysis | All pathways | Cañada del Buey | 5.5 ^a | 30 to 100 |
| Performance assessment | Groundwater protection | White Rock Pajarito Canyon | 4.5×10^{-5} ^b | 4 |
| Performance assessment | All pathways | White Rock Pajarito Canyon | 1.0×10^{-4} | 25 |
| Composite analysis | All pathways | White Rock Pajarito Canyon | 7.2×10^{-3} ^c | 30 to 100 |

^a This dose was determined at an assumed receptor location in Cañada del Buey assuming airborne suspension and transport of surface contamination from biotic intrusion into buried waste.

^b From Section 4.1.2 of LANL 1997, the peak annual dose within 1,000 years was 4.5×10^{-5} millirem, occurring at 700 years at the Pajarito Canyon location of maximum projected groundwater concentration. Beyond 1,000 years, the peak annual dose was 1.4×10^{-5} millirem, occurring at 4,000 years at a location 330 feet (100 meters) downgradient of MDA G.

^c From Section 4.2.1 of LANL 1997, the dose of 7.2×10^{-3} millirem was determined at an assumed receptor location in Pajarito Canyon, and includes a 1.9×10^{-7} millirem dose from hypothetical ingestion of groundwater. A dose of 1.2×10^{-5} millirem was determined at a location 330 feet (100 meters) downgradient of MDA G, and includes a 4.6×10^{-6} millirem dose from hypothetical ingestion of groundwater.

Source: LANL 1997.

With respect to the groundwater pathway, the model used for the analyses considered transport of contaminants from leachate vertically downward through the vadose zone to the regional aquifer or laterally to the perched alluvial groundwater in Pajarito Canyon, where the contaminants may be transported downward to the regional aquifer. For the performance assessment, doses for the groundwater pathway were determined at hypothetical receptor locations at the LANL boundary

near White Rock, at a point 330 feet (100 meters) east-southeast of MDA G, and in Pajarito Canyon. For the composite analysis, doses for the groundwater pathway were determined at the locations of maximum projected concentration downgradient of MDA G and in Pajarito Canyon (LANL 1997). The doses were calculated assuming the continuation of the existing temporary disposal covers at Area G.

The performance assessment and composite analysis for Area G are being revised. Work being done at LANL to develop conceptual models of the hydrogeology and numerical models of groundwater flow under the Pajarito Plateau will be incorporated into the revised performance assessment and composite analysis and will be applicable to future modeling efforts such as those used to develop remediation alternatives for the MDAs in corrective measure evaluations. Many of the more recent efforts to develop these conceptual models were published in an August 16, 2005, online publication of *Vadose Zone Journal*. Journal articles are summarized in Appendix E of this SWEIS.

Researchers developing improved conceptual models have postulated low rates of downward migration based on low rates of infiltration (for example, 0.04-0.08 inches [1-2 millimeters] per year) at LANL mesa tops, particularly in the eastern part of LANL (Birdsell et al. 1999, 2000, 2005; Kwicklis et al. 2005). A newly generated infiltration map for the Los Alamos area has been constructed using estimates of infiltration at points in upland areas, as well as estimates of streamflow losses and gains along canyon bottoms (Kwicklis et al. 2005). Although infiltration rates of less than 0.08 inches (2 millimeters) per year were estimated for mesa tops, larger infiltration rates were estimated at higher elevations in the Sierra de los Valles (for example, greater than 25 millimeters per year in mixed conifer areas to greater than 7.9 inches (200 millimeters) per year for areas having aspen). Canyon bottom infiltration rates depend on the size and elevation of the canyon's watershed and on the history of effluent discharge. Canyon infiltration rates can range from those that are not significantly different from surroundings mesa tops to several hundred millimeters per year (Kwicklis et al. 2005).

Either by increased matrix flow or fracture flow, flow focusing can cause flow and contaminant migration to increase above that otherwise predicted. For example, LANL staff point out that although mesa tops exhibit low infiltration, rates can become high in mesa top areas that contain faults or have become "disturbed" in some manner (for example, areas covered with asphalt or located in drainage diversions). Such anomalous (non-"background") infiltration rates should be considered in risk assessments of disturbed areas (Kwicklis et al. 2005). In the more extreme cases, the net infiltration rate has been estimated to be as high as 12 inches (300 millimeters) per year (Birdsell et al. 2005).

(Birdsell et al. 2005) describes conditions, and the results from disturbances, at two dry mesas, Mesita del Buey and Frijoles Mesa. At Mesita del Buey, downward fluxes vary with depth and across the mesa and are estimated to range from 0.001 to 0.2 inches (0.03 to 6 millimeters) per year. The estimates were made using volumetric moisture content and chloride data (Newman 1996) from four boreholes and from numerical modeling (Birdsell et al. 2000). Further, the four boreholes have depth intervals where fluxes are smaller than 1 millimeter per year. Chloride-based residence times range from 1,300 to 17,000 years (Newman 1996). These estimates of flux and residence time indicate very little water movement.

But there is evidence that dry mesa conditions can change when the water balance is perturbed; for example, when water is added to the soil from wastewater lagoons or stormwater diversion ditches. Focused runoff from an asphalt pad near a borehole on Mesita del Buey caused ponding in a localized area. Moisture content measurements in the borehole showed increasing water content as deep as 24 meters (roughly 80 feet) in less than 10 years after the ponding was initiated (Birdsell et al. 2005).

Dry conditions at Frijoles Mesa are similar to those at Mesita del Buey (that is, estimated infiltration rates are 0.3 to 2 millimeters per year, based on chloride data from a 210-meter borehole). At MDA AB on Frijoles Mesa, hydrodynamic testing was performed in 1960 and 1961 at the bottoms of numerous deep shafts that had been backfilled with sand and crushed tuff. One area at MDA AB was paved with asphalt in 1961 in an attempt to minimize surface contamination. But the asphalt inhibited evapotranspiration and dammed surface water along its edge. In 1975, the asphalt pad over a backfilled shaft collapsed, leaving a $6 \times 7 \times 4$ foot ($1.8 \times 0.9 \times 1.2$ meter) hole in the asphalt and underlying fill, and probably causing the standing water seen in Core Hole 2. After the standing water was bailed dry, the asphalt developed cracks; estimates of leakage through the cracked pad ranged from 2.4 to 15 inches (60 to 388 millimeters) per year. Standing water was again observed in Core Hole 2. Data from two other boreholes in 1994 indicated elevated water contents to a depth of 18 meters (roughly 60 feet). In contrast, background water-content profiles measured in five boreholes around the site showed tuff water content below about 10 feet (3 meters) to be less than ten percent. Numerical simulations for MDA AB based on an infiltration rate of 2.4 inches (60 millimeters) per year during the period 1961 through 1994 showed a reasonable fit to a water content profile obtained in 1994 (LANL 1992b, Birdsell et al. 1999, 2005). In 1998 and 1999, Core Hole 2 was grouted and abandoned, the asphalt was removed, and the site regraded and capped with an evapotranspiration cover (see Section I.2.5.3). Since then, the upper 20 feet (6 meters) of soil beneath the cover appear to be slowly drying (Levitt et al. 2005, Birdsell et al. 2005).

The field and laboratory study by Nyhan et al. (LANL 1984) at Area T illustrated that water can move rather efficiently through the tuff at mesa tops, and that mobile contaminants can move quickly in response to the water flux. Roughly 1.2 million gallons (4,600 cubic meters) of water were disposed of in Absorption Pit 1 at Area T over a 2-month period (LANL 1984).

Subsurface contaminant data collected beneath the absorption beds show evidence of contaminant transport associated with fractures, while subsurface data collected in boreholes adjacent to the beds showed none. The general assumption is that fracture transport occurred while the beds actively received liquid waste, and that the contaminants associated with the fractures are remnants of previous fracture flow episodes. The data support the idea that some fractures in the nonwelded to moderately welded tuff will flow when the matrix is saturated (Birdsell et al. 2005).

Flow focusing of some form may have caused the apparent observed movement of radionuclides from disposal units at Area G in TA-54. As cited in the MDA G investigative work plan, five radionuclides (americium-241, plutonium-238, plutonium-239, uranium, and cobalt-60) were found at depths exceeding 80 feet (24 meters) in four RFI boreholes at MDA G. Tritium was found in one borehole to a depth of 130 feet (40 meters) (LANL 2004c).

To conclude, MDAs are disturbed areas, and this, or flow focusing, may have caused or contributed to the observed elevated water content in subsurface soils and movement of contaminants at some MDAs. Uncertainty about the long-term infiltration rates at MDAs leads to uncertainty about the long-term performance of the MDAs. The result is uncertainty about possible future human risk from groundwater contamination, assuming nothing is done to reduce long-term infiltration into the MDAs. Deep contamination may be evidence of accelerated contaminant migration, due to possible fast paths (vertical fractures) or areas of increased infiltration and matrix flow, or both. The No Action Option would leave the MDAs vulnerable to these uncertainties.

I.5.3.2 Capping Option

I.5.3.2.1 Surface Water

Site Investigations. Investigations conducted under the Consent Order will provide additional information about the identity and extent of contaminants in groundwater and surface waters and information needed to predict impacts on water resources. The investigations may cause small risks to surface water quality because of generation of purge water as part of well sampling. However, this purge water would be retained and managed as required in the Consent Order, indicating that impacts on surface water of the investigation programs would be minimal.

Remediation of MDAs. Installing final covers at the MDAs would cause short-term risks to surface waters. Industrial equipment would disturb land, disrupting existing covers and presenting opportunities for runoff and erosion to transport soil and small levels of contamination to canyons. In addition, capping the MDAs would require the import of large quantities of tuff and surface amendment, some of which could be eroded into canyons. These risks would be reduced and mitigated using best management practices consistent with documented stormwater pollution prevention plans.

Despite possible short-term detriments, the Capping Option is expected to improve surface water quality compared to the No Action Option. A final cover is being designed consistent with the update of the performance assessment and composite analysis for the Area G low-level radioactive waste disposal facility. The final cover will extend over MDA G. Features of the final cover to resist biological intrusion would reduce the potential for contact by burrowing animals. Because of this, and because the final covers would overlie existing levels of surface contamination at MDA G, surface water pathways should be correspondingly protected from runoff and erosion of surface contamination. The design and installation of the final covers for the other MDAs would similarly minimize surface water runoff and erosion and would similarly protect surface water resources.

Remediation of Other PRSs. Continued progress would be made in remediating PRSs at various locations within LANL. There would be less contamination in soils and sediments that could present a risk to surface water quality.

Borrow Pit. Expanded use of the borrow pit in TA-61 has the potential for affecting surface water quality in Sandia Canyon. To preclude significant impacts, the expanded use would be consistent with a stormwater pollution prevention plan that would be prepared for the expanded

use. Runoff control structures or features would be installed as needed, and operational or administrative controls would be implemented consistent with the plan.

I.5.3.2.2 Groundwater

Site Investigations. Site investigations under the Consent Order are expected to have little or no impact on groundwater quality.

Remediation of MDAs. Placement of final covers over the MDAs, which would be among the alternatives considered in corrective measure evaluations for MDAs performed under the Consent Order,⁷⁶ would reduce risks to groundwater quality. Work on developing final covers has progressed over many years. Some of the considerations and tradeoffs to be weighed are addressed in Appendix C of the *MDA Core Document* (LANL 1999b). Technical and regulatory guidance on design, installation, and monitoring of alternative final landfill covers, including evapotranspiration covers, has been issued by the Interstate Technology and Regulatory Council (ITRC 2003b).

The long-term effectiveness of a final cover in reducing infiltration into the disposed waste at Area G or any of the other MDAs will depend on its design and construction, considering the natural processes that will affect its performance. Conventional covers, often called RCRA covers, include a resistive barrier layer as the primary barrier to percolation into underlying wastes. Alternative covers, often called evapotranspiration covers, depend on water storage and evapotranspiration. They have received increasing regulatory acceptance, particularly for arid locales. A few examples of research into use of alternative covers include the EPA Alternative Cover Assessment Project that has been ongoing since 1998 (DRI 2002a, 2002b; Roesler, Benson, and Albright 2002); test plots at LANL (Breshears, Nyhan, and Davenport 2005; Nyhan 2005); and a recently constructed cover over a uranium mill tailings site at Monticello, Utah (Waugh et al. 2001). Case studies addressing the use of evapotranspiration covers at landfills covering a range of climatic conditions are presented at a website hosted by EPA's Technology Innovation Program.

One of the studies cited in the EPA *Alternative Cover Assessment Project Report* is the Alternative Landfill Cover Demonstration at Sandia National Laboratories in Albuquerque, New Mexico. This Sandia project is performing side-by-side tests of six test plots, each 330 feet (100 meters) long and 43 feet (13 meters) wide, and each comprising a different cover design, including an evapotranspiration cover design (Dwyer 2001).

The LANL field demonstration was initiated in 1981 with the goals of developing barriers against biological intrusion and systems for groundwater and surface water management. In 1984, test sections of two cover designs were constructed. The cover sections have been monitored with respect to water balance, vegetation cover, rooting patterns, geotextile liner deterioration, preferential flow paths, and soil properties. It was determined, among other things, that the structure, bulk density, and effective permeability of cover layers can be altered over

⁷⁶ A corrective measure evaluation performed for MDA G in TA-54 would be coordinated with the update to the performance assessment and composite analysis that is currently under preparation. This update would consider the application of a final evapotranspiration cover over the disposal units, and would also update information about the site and the contents of the disposal units.

time by pedogenic processes, root intrusion, animal burrowing, and other disturbances (Breshears, Nyhan, and Davenport 2005). Another set of test plots at LANL investigated the total water balance within four unvegetated evapotranspiration covers having varying slopes. Evaporation usually increased with increasing slope, while interflow and seepage usually decreased with increasing slope (Nyhan 2005).

Evapotranspiration landfill covers can limit infiltration if properly designed, constructed, and maintained. Technical and regulatory guidance for design, installation, and monitoring of evapotranspiration landfill covers has been issued by the Interstate Technology and Regulatory Council (ITRC 2003b). If there are fast paths under waste facilities through which water and contaminants move episodically, covers may significantly inhibit that kind of transport by limiting the rapid water infiltration that drives it. However, the design of a successful cover will depend on systematic planning against processes that can degrade its performance over time. Accurate predictions of percolation rates through landfill covers will depend on knowledge of soil water storage and evapotranspiration. These elements will be influenced by the hydraulic properties of the soil used in the covers and by the properties of covering vegetation. Changes in vegetation can affect cover performance, and mineralogical and textural changes to the soil due to pedogenic processes can change the water retention properties of the soil layer. The potential for extreme weather events should be considered. Cover designs should also incorporate features to limit adverse changes caused by animal and root intrusion. Another consideration is the potential for long-term subsidence caused by slow decomposition and consolidation of the waste within the disposal units.

Remote-Handled Transuranic Waste Option. The option of leaving some remote handled transuranic waste in place would need to be protective of water resources, and such protection would be addressed as part of analyses performed for this option. In addition to future assessments performed as part of corrective measure evaluations under the Consent Order, inventories of transuranic and associated radioactive material would be included in composite analyses for Area G performed in compliance with DOE Order 435.1 (DOE 2001). These composite analyses address all radiological pathways involving potential release of radioactive material to an uncontrolled area, including pathways involving possible transport of contaminants by surface water and groundwater. And as noted in Section I.3.3.2.1.2.2, if required, an assessment pursuant to 40 CFR Part 191 may be performed. Such an assessment would address possible movement of contaminants from the disposal area by both surface water and groundwater.

Remediation of Other PRSs. Remedial actions conducted under the Consent Order will either improve groundwater quality or reduce risks to it from LANL PRSs. The scope of any remediation program for any watershed cannot be fully defined at this time, although potential remediation alternatives could range from no action to more significant activities such as in situ bioremediation, permeable reactive barriers, or groundwater pump-and-treat systems.

Borrow Pit. Operation of the TA-61 borrow pit should have no impact on groundwater quality.

I.5.3.3 Removal Option

I.5.3.3.1 Surface Water

Surface water quality would be improved compared to the No Action Option.

Site Investigations. Investigations conducted under the Consent Order may cause small risks to surface water quality because of generation of purge water from well sampling. But this purge water would be retained and managed as required in the Consent Order. Hence, impacts on surface water of the investigation program would be minimal.

Remediation of MDAs. Under the Removal Option, contamination in most LANL MDAs would be removed. Assuming that the contamination is removed to screening levels, surface water could remain at slight risk. Complete removal would eliminate the great bulk of the contamination at the MDAs. The contamination at the MDAs would be subsequently treated and disposed of either on or offsite. (By either method, disposal would be consistent with groundwater and surface water protection criteria and goals at the disposal facilities.) Partial removal of waste from MDAs would result in smaller risks to surface water resources than either the No Action or the Capping Option. After waste is partially removed from the MDAs, residual contamination would be stabilized and capped.

Removal of the waste and contamination at the MDAs would entail small, short-term risks to surface waters. Excavated waste may spill or release liquids. Industrial equipment would disturb land, disrupting existing covers and causing opportunities for runoff and erosion to transport soil and small levels of contamination into canyons. Removal of the MDAs would require the import of very large quantities of tuff and surface amendment, some of which could be eroded into canyons. These risks would be reduced and mitigated using techniques, including safe waste management procedures, contamination control, monitoring, and best management practices.

Remediation of Other PRSs. As part of the Removal Option, continued progress would be made in remediating PRSs within LANL. There would be less contamination in soils and sediments that could present a risk to groundwater or surface water quality.

Borrow Pit. Because the amount of material to be removed under the Removal Option is comparable to that under the Capping Option, impacts on surface water quality would be comparable.

I.5.3.3.2 Groundwater

Site Investigations. Similar to that under the Capping Option, there should be few, if any, impacts on or risks to groundwater from conducting site investigations under the Consent Order.

Remediation of MDAs. Because the bulk of the contamination in most MDAs would be removed, groundwater risks would be greatly reduced, although some slight risk may remain from any remaining contamination meeting screening levels. In addition, the filled, compacted excavation may still experience larger infiltration rates (for a time) than undisturbed areas, which might further drive migration of deeper contaminants that are beyond the reach of the excavation.

Partial removal of waste from MDAs, such as that contemplated for MDA B, would result in smaller risks to groundwater resources than either the No Action or Capping Options. Residual contamination in the MDAs would be stabilized and capped.

Remediation of Other PRSs. Improvements in groundwater quality from implementation of the Consent Order would be the same as those addressed for the Capping Option.

Borrow Pit. Similar to the Capping Option, operation of the TA-61 borrow pit should have little to no effect on groundwater quality.

I.5.4 Air Quality and Noise

I.5.4.1 No Action Option

I.5.4.1.1 Air Quality

Continuing LANL's environmental restoration project may have small impacts on air quality. Pollutants would be emitted from operation of waste management facilities supporting environmental restoration, as well as from vehicles and construction equipment. Combustion products would be emitted from thermal treatment of any high explosives recovered as part of the environmental restoration project. These releases, however, would probably be small compared with those that would occur as part of ongoing LANL operations and DD&D activities involving safe destruction of high explosives.

Pollutant releases from heavy equipment operation for contaminated material recovery during environmental restoration were estimated for the No Action Option using the procedures outlined in Section I.3.6.4, for which emissions were related to the volumes of wastes projected to be generated. Calculated total release of nitrogen oxides (NO_x), carbon monoxide (CO), sulfur oxides (SO_x), particulate matter with an aerodynamic diameter less than or equal to 10 micrometers (PM₁₀), carbon dioxide (CO₂), aldehydes, and total organic compounds are presented in **Table I-86** in units of tons.

Table I-86 No Action Option Projected Pollutant Releases to Air from Heavy Machinery Operation

| Pollutant (tons) | Fiscal Year | | | | | | | | | |
|---------------------|-------------|------|------|---------|--------|--------|--------|--------|--------|--------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 |
| NO _x | 4.6 | 7.7 | 6.3 | 0.045 | 0.51 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| CO | 12 | 19 | 16 | 0.11 | 1.3 | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 |
| SO _x | 0.30 | 0.50 | 0.41 | 0.0029 | 0.033 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| PM ₁₀ | 0.32 | 0.54 | 0.44 | 0.0032 | 0.036 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 |
| CO ₂ | 190 | 310 | 260 | 1.8 | 21 | 7.3 | 7.3 | 7.3 | 7.3 | 7.3 |
| Aldehydes | 0.080 | 0.13 | 0.11 | 0.00079 | 0.0089 | 0.0032 | 0.0032 | 0.0032 | 0.0032 | 0.0032 |
| TOCs | 0.86 | 1.5 | 1.2 | 0.0086 | 0.10 | 0.034 | 0.034 | 0.034 | 0.034 | 0.034 |

NO_x = nitrogen oxides, CO = carbon monoxide, SO_x = sulfur oxides, PM₁₀ = particulate matter with an aerodynamic diameter less than or equal to 10 micrometers, CO₂ = carbon dioxide, TOCs = total organic compounds.

Note: To convert tons to metric tons, multiply by 0.90718. Numbers have been rounded.

Small levels of dust (and particulate matter) would be released to the air, as well as small quantities of radionuclides. These releases are not expected to result in emissions that would exceed applicable standards. The major sources of criteria pollutants at LANL have not been historically from the environmental restoration project (see Chapter 4, Section 4.4.2.2, of this SWEIS). Continuing environmental restoration should not, therefore, result in major changes to existing compliant conditions. Nonetheless, there would be continued release of small quantities of volatile organic compounds to the air from some MDAs.

Trends have shown reductions in annual doses to the public from release of radionuclides to the air. Continuing these programs should therefore neither reverse these trends nor cause noncompliance with NESHAP.

I.5.4.1.2 Noise

Continuing the LANL environmental restoration project should result in some levels of sound perceived as noise. This would result from operation of construction equipment and vehicles. Vehicle noise would result from operation of personal vehicles and from transport of wastes and other materials. Under the No Action Option, the total number of one-way waste shipments from the environmental restoration project is estimated at about 1,000 through FY 2016. The largest number of one-way shipments (400 or about 1.6 per working day) is projected to occur in FY 2008. Therefore, the noise from continuing the current program should be similar to that resulting from the past several years in which environmental restoration has taken place at LANL.

I.5.4.2 Capping Option

I.5.4.2.1 Air Quality

Site Investigations. Site investigations under the Consent Order should have few, if any, impacts on LANL air quality.

Remediation of MDAs and Other PRSs. The Capping Option may have temporary impacts on air quality. Compared to the No Action Option, the Capping Option would require the use of additional heavy equipment that would result in additional air emissions. Pollutants including nitrogen oxides, carbon monoxide, sulfur oxide, PM₁₀, carbon dioxide, aldehydes, and total organic compounds are summarized in **Tables I-87** and **I-88** in units of tons released to the air. Table I-87 lists pollutants released for the entire Capping Option. Table I-88 lists pollutants for capping the existing Area G footprint and for capping MDAs A, B, T, and U in TA-21. Quantities released were calculated using the procedures outlined in Section I.3.6.4.

In addition, dust (and particulate matter) would be dispersed into the air from grading, earthmoving, and compaction. This could occur at the MDAs being remediated and at locations where sources of capping materials would be excavated. Dust and particulate emissions would be mitigated, however, by standard dust control measures such as water sprays.

Small levels of radionuclides may be discharged into the air from capping the MDAs because of small quantities of radionuclides and other contaminants in soil. Construction activities that abrade and loosen the soil would help to promote release. But these levels would be small and

temporary. Capping would be accompanied, as needed, by installation of soil vapor extraction systems to address phases of volatile organic compounds at some MDAs (see Section I.3.3.2.2.4). As needed, vapor withdrawn from soil using the extraction systems would be treated using carbon absorption, catalytic oxidation, or other technologies.

Table I-87 Capping Option Projected Pollutant Releases to Air from Heavy Machinery Operation

| Pollutant (tons) | Fiscal Year | | | | | | | | | |
|------------------------------|-------------|-------|-------|-------|--------|------|-------|-------|-------|-------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 |
| Minimum-Thickness Cap | | | | | | | | | | |
| NO _x | 20 | 23 | 52 | 77 | 190 | 15 | 160 | 18 | 160 | 64 |
| CO | 49 | 57 | 130 | 200 | 470 | 39 | 400 | 45 | 410 | 160 |
| SO _x | 1.3 | 1.5 | 3.4 | 5.0 | 12 | 1.0 | 10 | 1.2 | 11 | 4.1 |
| PM ₁₀ | 1.4 | 1.6 | 3.6 | 5.4 | 13 | 1.1 | 11 | 1.2 | 11 | 4.4 |
| CO ₂ | 790 | 920 | 2,100 | 3,100 | 7,600 | 620 | 6,500 | 730 | 6,600 | 2,600 |
| Aldehydes | 0.34 | 0.40 | 0.91 | 1.4 | 3.3 | 0.27 | 2.8 | 0.31 | 2.9 | 1.1 |
| TOCs | 3.7 | 4.3 | 9.8 | 15 | 35 | 2.9 | 30 | 3.4 | 31 | 12 |
| Maximum-Thickness Cap | | | | | | | | | | |
| NO _x | 24 | 27 | 69 | 120 | 270 | 20 | 220 | 25 | 230 | 87 |
| CO | 61 | 68 | 170 | 310 | 690 | 50 | 560 | 63 | 570 | 220 |
| SO _x | 1.6 | 1.8 | 4.5 | 8.0 | 18 | 1.3 | 14 | 1.6 | 15 | 5.7 |
| PM ₁₀ | 1.7 | 1.9 | 4.8 | 8.5 | 19 | 1.4 | 16 | 1.8 | 16 | 6.1 |
| CO ₂ | 980 | 1,100 | 2,800 | 5,000 | 11,000 | 810 | 9,000 | 1,000 | 9,300 | 3,500 |
| Aldehydes | 0.42 | 0.48 | 1.2 | 2.1 | 4.8 | 0.35 | 3.9 | 0.44 | 4.0 | 1.5 |
| TOCs | 4.5 | 5.1 | 13 | 23 | 51 | 3.8 | 42 | 4.8 | 43 | 16 |

NO_x = nitrogen oxides, CO = carbon monoxide, SO_x = sulfur oxides, PM₁₀ = particulate matter with an aerodynamic diameter less than or equal to 10 micrometers, CO₂ = carbon dioxide, TOCs = total organic compounds.

Note: To convert tons to metric tons, multiply by 0.90718. Numbers have been rounded.

Grouting the General's Tanks in MDA A may result in release of small quantities of pollutants into the air, principally from operation of equipment and vehicles. Activities preliminary to grouting may result in a one-time release of small quantities of hydrogen or other gases as noted in Section I.3.3.2.2.5. Similarly, if some transuranic wastes are left in TA-54 under the option discussed in Section I.3.3.2.1.2.2, there may be some small release of pollutants into the air as part of stabilization activities (for example, grout encapsulation or in situ vitrification). Stabilization activities may result in small releases of pollutants from operation of heavy equipment. If vitrification is considered, the process would generate water vapor and organic combustion products that would be drawn into an offgas treatment system.

Otherwise, under the Capping Option, continued remediation of PRSs may release small quantities of radionuclides into the air and cause public exposures to radiation. Public doses from such releases are estimated in Section I.5.6.2.2.

Table I-88 Projected Pollutant Releases to Air from Heavy Machinery Operation from Capping Area G and Combined Material Disposal Areas A, B, T, and U

| Pollutant (tons) | Fiscal Year | | | | | | | | | |
|---|-------------|------|-------|-------|-------|----------------------|-------|------|-------|-------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 |
| Area G ^a | | | | | | | | | | |
| <i>Minimum-Thickness Cap</i> | | | | | | | | | | |
| NO _x | – | – | – | – | 150 | – | 150 | – | 150 | 48 |
| CO | – | – | – | – | 370 | – | 370 | – | 370 | 120 |
| SO _x | – | – | – | – | 9.4 | – | 9.4 | – | 9.4 | 3.1 |
| PM ₁₀ | – | – | – | – | 10 | – | 10 | – | 10 | 3.4 |
| CO ₂ | – | – | – | – | 5,900 | – | 5,900 | – | 5,900 | 2,000 |
| Aldehydes | – | – | – | – | 2.5 | – | 2.5 | – | 2.5 | 0.85 |
| TOCs | – | – | – | – | 27 | – | 27 | – | 27 | 9.2 |
| <i>Maximum-Thickness Cap</i> | | | | | | | | | | |
| NO _x | – | – | – | – | 200 | – | 200 | – | 200 | 68 |
| CO | – | – | – | – | 510 | – | 510 | – | 510 | 170 |
| SO _x | – | – | – | – | 13 | – | 13 | – | 13 | 4.4 |
| PM ₁₀ | – | – | – | – | 14 | – | 14 | – | 14 | 4.7 |
| CO ₂ | – | – | – | – | 8,200 | – | 8,200 | – | 8,200 | 2,700 |
| Aldehydes | – | – | – | – | 3.5 | – | 3.5 | – | 3.5 | 1.2 |
| TOCs | – | – | – | – | 38 | – | 38 | – | 38 | 13 |
| Material Disposal Areas A, B, T, and U | | | | | | | | | | |
| <i>Minimum-Thickness Cap</i> | | | | | | | | | | |
| NO _x | – | – | 4.1 | 33 | 22 | 0.16 | – | – | – | – |
| CO | – | – | 10 | 82 | 55 | 0.41 | – | – | – | – |
| SO _x | – | – | 0.27 | 2.1 | 1.4 | 0.010 | – | – | – | – |
| PM ₁₀ | – | – | 0.29 | 2.3 | 1.5 | 0.011 | – | – | – | – |
| CO ₂ | – | – | 170 | 1,300 | 890 | 6.5 | – | – | – | – |
| Aldehydes | – | – | 0.072 | 0.57 | 0.38 | 2.8x10 ⁻³ | – | – | – | – |
| TOC | – | – | 0.77 | 6.1 | 4.1 | 0.030 | – | – | – | – |
| <i>Maximum-Thickness Cap</i> | | | | | | | | | | |
| NO _x | – | – | 7.9 | 59 | 37 | 0.32 | – | – | – | – |
| CO | – | – | 24 | 180 | 110 | 0.95 | – | – | – | – |
| SO _x | – | – | 11 | 79 | 50 | 0.41 | – | – | – | – |
| PM ₁₀ | – | – | 0.81 | 6.0 | 3.8 | 0.032 | – | – | – | – |
| CO ₂ | – | – | 320 | 2,400 | 1,500 | 13 | – | – | – | – |
| Aldehydes | – | – | 170 | 1,200 | 770 | 6.3 | – | – | – | – |
| TOCs | – | – | 1.6 | 12 | 7.4 | 0.062 | – | – | – | – |

NO_x = nitrogen oxides, CO = carbon monoxide, SO_x = sulfur oxides, PM₁₀ = particulate matter with an aerodynamic diameter less than or equal to 10 micrometers, CO₂ = carbon dioxide, TOCs = total organic compounds.

^a Refers to capping the existing Area G footprint in TA-54, which includes MDA G.

Note: To convert tons to metric tons, multiply by 0.90718. Numbers have been rounded.

Borrow Pit. Projected annual releases of pollutants from operation of heavy equipment at the TA-61 borrow pit, using procedures outlined in Section I.3.6.4, are listed in **Table I-89**.

Table I-89 Capping Option Projected Pollutant Releases to Air from Technical Area 61 Borrow Pit Heavy-Machinery Operation

| Pollutant (tons) | Fiscal Year | | | | | | | | | |
|------------------------------|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 |
| <i>Minimum Thickness Cap</i> | | | | | | | | | | |
| NO _x | 2.7 | 2.7 | 22 | 39 | 71 | 2.7 | 57 | 4.2 | 59 | 21 |
| CO | 6.7 | 6.7 | 54 | 99 | 180 | 6.9 | 140 | 11 | 150 | 53 |
| SO _x | 0.17 | 0.17 | 1.4 | 2.5 | 4.6 | 0.18 | 3.7 | 0.27 | 3.8 | 1.4 |
| PM ₁₀ | 0.19 | 0.19 | 1.5 | 2.7 | 5.0 | 0.19 | 4.0 | 0.29 | 4.1 | 1.5 |
| CO ₂ | 110 | 110 | 880 | 1,600 | 2,900 | 110 | 2,300 | 170 | 2,400 | 850 |
| Aldehydes | 0.046 | 0.046 | 0.38 | 0.69 | 1.2 | 0.048 | 1.0 | 0.073 | 1.0 | 0.37 |
| TOCs | 0.50 | 0.50 | 4.1 | 7.4 | 13 | 0.52 | 11 | 0.79 | 11 | 3.9 |
| <i>Maximum Thickness Cap</i> | | | | | | | | | | |
| NO _x | 7.3 | 7.3 | 45 | 94 | 200 | 7.5 | 160 | 11 | 160 | 57 |
| CO | 18 | 18 | 110 | 240 | 490 | 19 | 400 | 29 | 410 | 140 |
| SO _x | 0.47 | 0.47 | 3.0 | 6.1 | 13 | 0.49 | 10 | 0.74 | 10 | 3.7 |
| PM ₁₀ | 0.51 | 0.51 | 3.2 | 6.6 | 14 | 0.52 | 11 | 0.80 | 11 | 4.0 |
| CO ₂ | 290 | 290 | 1,800 | 3,800 | 8,000 | 300 | 6,400 | 460 | 6,500 | 2,300 |
| Aldehydes | 0.13 | 0.13 | 0.80 | 1.6 | 3.4 | 0.13 | 2.7 | 0.20 | 2.8 | 1.0 |
| TOCs | 1.4 | 1.4 | 8.6 | 18 | 37 | 1.4 | 30 | 2.2 | 30 | 11 |

NO_x = nitrogen oxides, CO = carbon monoxide, SO_x = sulfur oxides, PM₁₀ = particulate matter with an aerodynamic diameter less than or equal to 10 micrometers, CO₂ = carbon dioxide, TOCs = total organic compounds.

Note: To convert tons to metric tons, multiply by 0.90718. Numbers have been rounded.

Potential dust levels at the borrow pit were estimated using Equation 1 from *Compilation of Air Pollutant Emission Factors, Volume 1: Stationary Point and Area Sources*, Section 13.2.4, “Aggregate Handling and Storage Piles (EPA 1995). An average wind speed of 2.9 meters per second and an average moisture content of 3.4 percent was assumed.⁷⁷ Also, assuming that the material would be “dropped” twice (once when piled and once when placed in a truck); assuming no controls or mitigation measures; and assuming an 8.2-foot (2.5-meter) cap at all MDAs, the largest release (1,000 pounds [450 kilograms]) of PM₁₀ would occur during FY 2011. Emissions of dust and particulates would be mitigated, however, using standard dust control measures such as water sprays.

Localized emissions of criteria pollutants, particulates, and dust would be further reduced if some material was obtained from other sources.

I.5.4.2.2 Noise

Site Investigations. Site investigations under the Consent Order would cause very small noise impacts from activities such as well installation.

⁷⁷ A moisture content of 3.4 percent was assumed from Table 13.2.4-1 of AP42 (EPA 1995). It is typical for exposed ground of western surface coal mines.

Remediation of MDAs and Other PRSs. The Capping Option would have increased noise impacts as compared to the No Action Option. Heavy equipment would be used during site preparation and for earthmoving. The noise would depend on the equipment design and its quantity—that is, the scale of operation would depend on the size of the worksite. Issues would include the effect of noise on workers, other LANL personnel, or the public in the vicinities of the worksites. Workers would be equipped with hearing protection if the work produced noise levels above the LANL action level of 82 dBA. These measures, as well as adherence to other safe operating procedures such as training and designated worker exclusion areas, should preclude serious injuries from noise exposures. Regarding persons near the worksite, noise levels would depend on the characteristics of the equipment, separation distance, and presence of physical features that can attenuate noise, such as topography or vegetation. Heavy equipment such as front-end loaders and backhoes would produce intermittent noise levels at 73 to 94 dBA at 50 feet (15 meters) from the worksite under normal working conditions (DOE 2004b). Considering physical features, noise levels from this equipment could return to background levels within about 1,000 feet from the noise source.

Accompanying this noise would be that from trucks shipping waste to on- and offsite destinations and deliveries of cover materials. Assuming all solid waste under the Capping Option is shipped offsite, the total number of one-way shipments from FY 2007 through FY 2016 would increase from about 1,000 under the No Action Option to 7,200. Waste shipments under the Capping Option would average about 3 per day, assuming 250 working days per year. The largest number of one-way waste shipments (970 shipments) would occur during FY 2008. One-way shipments of crushed tuff, rock, gravel, and other capping materials would total from 92,000 to 191,000 over 10 years, or an average of 9,200 to 19,100 per year (37 to 76 trucks per day), depending on the thickness of cover. This increase in one-way truck traffic should be small compared with normal vehicle traffic in the LANL area. For example, a September 2004 study recorded vehicular traffic counts at several locations in the LANL region (KSL 2004). Average weekday traffic counts for selected locations were (KSL 2004):

- 9,502 vehicles per day on East Jemez Road near its intersection with NM 4
- 4,984 vehicles per day on Pajarito Road near its intersection with NM 4
- 12,185 vehicles per day on NM 502 (East Road) west of its intersection with NM 4
- 16,866 vehicles per day on Diamond Drive just south of its intersection with East Jemez Road
- 6,019 vehicles per day on West Jemez Road just south of its intersection with Camp May Road

Traffic on East Jemez Road may be heard in the trailer park on East Jemez Road. Traffic passing by the trailer park could include shipments of solid waste to the transfer station at the county landfill, and shipments of crushed tuff from the TA-61 borrow pit. (However, shipments of solid waste generated by LANL's environmental restoration project have historically been sent directly to an offsite landfill. Hence, use of the transfer station by LANL's environmental restoration project may be minimal.) The number of trucks would depend not only on the quantities of

wastes shipped, or tuff delivered, but on routing decisions (for example, trucks stopping at the borrow pit from East Jemez Road may, once loaded, continue in the same direction or return in the original direction).

If all industrial solid waste under the Capping Option passes through the transfer station at the county landfill, then about 3,600 trucks containing this waste could transit East Jemez Road over 10 years, averaging 360 per year.⁷⁸ If all tuff used for capping the MDAs were to originate from the TA-61 borrow pit, and all shipments passed the trailer park, then approximately 59,000 to 155,000 one-way shipments would transit East Jemez Road over 10 years. This would average 5,900 to 15,500 per year. The largest number of one-way shipments would occur during FY 2011, when from 15,000 to 41,000 trucks containing tuff would transit East Jemez Road. Adding solid waste shipments to these tuff shipments could result in a little more than 41,000 one-way shipments in FY 2011 on East Jemez Road, or 165 trucks every working day. This increased truck traffic may be compared to the average number of vehicles on East Jemez Road (11,181 vehicles per day on workdays), as measured near the trailer park in September 2004 (KSL 2004). Assuming all trucks pass the trailer park twice (coming and going), this would be an increase of 3 percent in the number of vehicles traveling the road on a daily basis.

I.5.4.3 Removal Option

I.5.4.3.1 Air Quality

Site Investigations. Site investigations under the Consent Order are expected to have little to no impacts on air quality.

Remediation of MDAs and Other PRSs. The Removal Option may have short-term effects on air quality. Dust and particulate matter would be generated as part of MDA exhumation, backfilling, and final restoration. Release of dust into the air would be controlled using standard techniques.

This alternative would greatly reduce, if not eliminate, the potential for long-term release of volatile organic compounds from the MDAs.

The Removal Option would require use of additional vehicles and construction equipment compared with the Capping Option. Therefore, air emissions from these sources would be increased compared with the Capping Option. Estimated releases from FY 2007 through FY 2016, and from FY 2007 through FY 2011, are listed in **Tables I-90** and **91** in units of tons. The releases were estimated using the procedures outlined in Section I.3.6.4, and no reductions in release were considered for removal operations that could occur under enclosures (see below). The releases estimated in Table I-90 are for complete removal of all MDAs and other remediation activities conducted under the Removal Option, as well as capping the remaining disposal units in the existing Area G footprint, plus some small areas in TA-49. Releases estimated in Table I-91 are for complete removal of MDA G and for combined MDAs A, B, T, and U. A thick cap was assumed for both tables. Partial removal of waste and contamination from MDAs would result in reduced emissions.

⁷⁸ This is unlikely because solid waste is normally sent directly to an offsite industrial landfill.

Table I-90 Removal Option Projected Pollutant Releases to Air from Heavy-Machinery Operation ^a

| Pollutant (tons) | Fiscal Year | | | | | | | | | |
|---------------------|-------------|-------|--------|---------|---------|--------|---------|---------|---------|--------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 |
| NO _x | 30 | 64 | 2,000 | 2,900 | 2,500 | 2,400 | 2,500 | 2,600 | 2,500 | 470 |
| CO | 74 | 160 | 5,100 | 7,300 | 6,400 | 6,100 | 6,300 | 6,400 | 6,200 | 1,200 |
| SO _x | 1.9 | 4.1 | 130 | 190 | 160 | 160 | 160 | 170 | 160 | 30 |
| PM ₁₀ | 2.0 | 4.4 | 140 | 200 | 180 | 170 | 180 | 180 | 170 | 33 |
| CO ₂ | 1,200 | 2,600 | 82,000 | 120,000 | 100,000 | 99,000 | 100,000 | 100,000 | 100,000 | 19,000 |
| Aldehydes | 0.51 | 1.1 | 35 | 51 | 44 | 43 | 44 | 45 | 43 | 8.2 |
| TOCs | 5.5 | 12 | 380 | 550 | 480 | 460 | 470 | 480 | 470 | 88 |

NO_x = nitrogen oxides, CO = carbon monoxide, SO_x = sulfur oxides, PM₁₀ = particulate matter with an aerodynamic diameter less than or equal to 10 micrometers, CO₂ = carbon dioxide, TOCs = total organic compounds.

^a Includes releases projected from placing a thick evapotranspiration cap over the remaining disposal units, at Area G, and over small areas in TA-49.

Note: To convert tons to metric tons, multiply by 0.90718. Numbers have been rounded.

Table I-91 Projected Pollutant Releases to Air from Heavy-Machinery Operation from Removal of Material Disposal Areas G and Material Disposal Areas A, B, T, and U

| Pollutant (tons) | Fiscal Year | | | | | | | | | |
|---|-------------|-------|--------|--------|--------|------------------------|--------|--------|--------|--------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 |
| MDA G ^a | | | | | | | | | | |
| NO _x | – | – | 1,600 | 2,400 | 2,400 | 2,400 | 2,400 | 2,400 | 2,400 | 440 |
| CO | – | – | 3,900 | 6,100 | 6,100 | 6,100 | 6,100 | 6,100 | 6,100 | 1,100 |
| SO _x | – | – | 100 | 160 | 160 | 160 | 160 | 160 | 160 | 29 |
| PM ₁₀ | – | – | 110 | 170 | 170 | 170 | 170 | 170 | 170 | 31 |
| CO ₂ | – | – | 64,000 | 98,000 | 98,000 | 98,000 | 98,000 | 98,000 | 98,000 | 18,000 |
| Aldehydes | – | – | 27 | 42 | 42 | 42 | 42 | 42 | 42 | 7.7 |
| TOCs | – | – | 300 | 450 | 450 | 450 | 450 | 450 | 450 | 83 |
| MDAs A, B, T, and U ^b | | | | | | | | | | |
| NO _x | – | 28 | 310 | 370 | 85 | 0.10 | – | – | – | – |
| CO | – | 7.1 | 780 | 930 | 210 | 0.24 | – | – | – | – |
| SO _x | – | 1.8 | 20 | 24 | 5.5 | 6.2 × 10 ⁻³ | – | – | – | – |
| PM ₁₀ | – | 2.0 | 22 | 26 | 5.9 | 6.6 × 10 ⁻³ | – | – | – | – |
| CO ₂ | – | 1,200 | 13,000 | 15,000 | 3,400 | 3.9 | – | – | – | – |
| Aldehydes | – | 0.5 | 5.4 | 6.5 | 1.5 | 1.7 × 10 ⁻³ | – | – | – | – |
| TOCs | – | 5.3 | 58 | 70 | 16 | 1.8 × 10 ⁻² | – | – | – | – |

MDA = material disposal area, NO_x = nitrogen oxides, CO = carbon monoxide, SO_x = sulfur oxides, PM₁₀ = particulate matter with an aerodynamic diameter less than or equal to 10 micrometers, CO₂ = carbon dioxide, TOCs = total organic compounds.

^a Includes releases projected from placing a thick evapotranspiration cap over the remaining disposal units in the existing Area G footprint.

^b Includes projected releases from MDA U for completeness. No additional remediation is expected for MDA U.

Note: To convert tons to metric tons, multiply by 0.90718. Numbers have been rounded.

Based on the above projected releases, minor to moderate increases in short-term concentrations of criteria pollutants could occur near MDA remediation activities. For MDA G removal, concentrations at the site boundary near White Rock may exceed the 1-hour and 8-hour ambient standards for carbon monoxide, and the 24-hour and annual standards for nitrogen dioxide. Also, concentrations at the site boundary near the Los Alamos townsite for combined removal of MDAs A, B, T, and U may exceed the 1-hour ambient standard for carbon monoxide and the

24-hour standard for nitrogen dioxide. Tailpipe emissions of PM₁₀ from removal of MDA G would be more than 80 percent of ambient standards, conservatively assuming no reductions in release of particulate matter from use of enclosures. Appropriate management controls and scheduling would be used to minimize impacts on the public and to meet regulatory requirements.

The operation causing the largest release would be complete removal of MDA G.

The Removal Option may cause radiological exposures to the public from dispersion of radioactive material into the air and transport by wind to locations occupied by humans. Excavating, sorting, characterizing, and classifying the waste removed from the larger MDAs may be performed within enclosures (see Sections I.3.3.2.6 and I.5.6.3.2). Enclosures may not be needed for many MDAs, particularly the small ones, or for remediating other PRSs. Enclosures may be used for removal of the larger MDAs because of the types and quantities of the wastes to be exhumed and the proximity of the MDAs to occupied areas.

Exposures to the public were estimated by: (1) establishing a source term for release from each MDA, and (2) assuming that releases into the air would be transported to locations occupied by members of the public using standard sector-averaged Gaussian plume dispersion models and joint distribution frequencies appropriate for the LANL area. Estimated radiological doses are presented in Section I.5.6.3.2.

Borrow Pit. Operation of heavy equipment at the borrow pit is conservatively projected, using the procedures outlined in Section I.3.6.4, to release pollutants listed in **Table I-92**.

Table I-92 Removal Option Projected Pollutant Releases to Air from Technical Area 61 Borrow Pit Heavy Machinery Operation ^a

| Pollutant (tons) | Fiscal Year | | | | | | | | | |
|---------------------|-------------|------|-------|-------|-------|-------|-------|-------|-------|------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 |
| NO _x | 6.6 | 16 | 110 | 130 | 90 | 86 | 88 | 89 | 87 | 21 |
| CO | 17 | 40 | 280 | 340 | 230 | 220 | 220 | 220 | 220 | 53 |
| SO _x | 0.43 | 1.0 | 7.1 | 8.8 | 5.9 | 5.6 | 5.7 | 5.7 | 5.6 | 1.4 |
| PM ₁₀ | 0.46 | 1.1 | 7.7 | 9.4 | 6.3 | 6.0 | 6.1 | 6.2 | 6.1 | 1.5 |
| CO ₂ | 270 | 640 | 4,500 | 5,500 | 3,700 | 3,500 | 3,600 | 3,600 | 3,500 | 860 |
| Aldehydes | 0.12 | 0.28 | 1.9 | 2.4 | 1.6 | 1.5 | 1.5 | 1.6 | 1.5 | 0.37 |
| TOCs | 1.3 | 3.0 | 21 | 25 | 17 | 16 | 17 | 17 | 16 | 4.0 |

NO_x = nitrogen oxides, CO = carbon monoxide, SO_x = sulfur oxides, PM₁₀ = particulate matter with an aerodynamic diameter less than or equal to 10 micrometers, CO₂ = carbon dioxide, TOCs = total organic compounds.

^a Includes releases projected from placing a thick evapotranspiration cap over the remaining disposal units at Area G, and over small areas in TA-49.

Note: To convert tons to metric tons, multiply by 0.90718. Numbers have been rounded.

Dust levels at the borrow pit were estimated using the methods discussed in Section I.5.4.1.1, assuming complete removal of waste and contamination from MDAs, and assuming that all material needed to backfill the excavated MDAs would be obtained from this borrow pit. The TA-61 borrow pit was also assumed to be the source for crushed tuff for capping the remaining disposal units within the existing Area G footprint and the small areas in TA-49. Assuming no controls or mitigation measures, the largest release of PM₁₀ (700 pounds [320 kilograms]) would

occur during FY 2010. Emissions of dust and particulate matter would be mitigated, however, using dust control measures such as water sprays.

Localized emissions of criteria pollutants, particulates, and dust would be further reduced if some material was obtained from other sources.

I.5.4.3.2 Noise

The Removal Option could have larger noise impacts compared with the Capping Option. The Removal Option would require more heavy equipment than the Capping Option, and there would be increased vehicle traffic. Both factors would increase background noise near the work areas.

With respect to vehicular traffic, assuming all waste generated under the Removal Option is shipped offsite, the total number of one-way waste shipments from FY 2007 through FY 2016 would be approximately 109,000, an average of 10,900 per year. The largest number of one-way waste shipments (about 22,000 shipments) would be during FY 2010. Shipments of backfill and topsoil would number up to 160,000 shipments over 10 years, or an average of 16,000 per year.⁷⁹ Thus, the Removal Option could increase traffic noise at LANL compared to the Capping Option.

Trucks on East Jemez Road may be heard in the trailer park. If all solid waste from the Removal Option passes through the transfer station at the county landfill (which is unlikely, given the existing practice of sending solid waste from environmental restoration directly to an offsite landfill), then about 9,700 one-way shipments containing this waste could transit East Jemez Road over 10 years, or about 970 per year. This averages 3.9 trucks per working day. If all crushed tuff for the Removal Option came from the TA-61 borrow pit, up to 142,000 one-way shipments of crushed tuff would transit East Jemez Road through FY 2016, assuming a thick cap for Area G and TA-49. This averages 14,200 per year (57 per working day). The largest number of shipments would occur during FY 2010, when about 26,000 one-way shipments of crushed tuff could transit East Jemez Road. As noted for the Capping Option, this increase in traffic can be compared to the average vehicular traffic on East Jemez Road of 11,181 vehicles per day during weekdays (KSL 2004). Adding solid waste shipments through the transfer station, the total shipments on East Jemez Road during the peak year, FY 2010, would approach 56,000 two-way shipments, or roughly 220 trucks per day. Assuming these trucks passed the trailer park twice each day (going and coming), this would be a 2 percent increase in the number of vehicles traveling the road on a daily basis.

I.5.5 Ecological Resources

I.5.5.1 No Action Option

LANL's environmental restoration project would continue to reduce ecological risks associated with the legacy of past LANL operations. As noted in the *1999 SWEIS*, the remaining contamination is the primary contributor to ecological health risk (DOE 1999a). In the *1999 SWEIS*, ecological risk was estimated to be very small, and no significant adverse impacts on

⁷⁹ Includes material for backfilling and covering removed MDAs, and capping the remaining disposal units in the existing Area G footprint, plus small areas in TA-49. A thick cap is assumed.

ecological and biological resources were projected under the Expanded Operations Alternative. The No Action Option for this appendix represents a continuation of the 1999 SWEIS Expanded Operations Alternative. Completion of site investigations and cleanups translates to a reduction in ecological risk.

As LANL's environmental restoration project activities are undertaken, limited, short-term impacts on ecological resources are likely. The extent, duration, and intrusive nature of the remedial activity would affect the magnitude of the ecological impacts. Disturbed areas would be revegetated to restore ecological conditions. Because negative impacts are expected to be limited to short durations, the overall impact on ecological resources would be positive as contamination is removed from the environment.

I.5.5.2 Capping Option

Site Investigations. Under the Capping Option, installation of exploratory and monitoring wells (or similar investigative features) in compliance with the Consent Order would cause some impacts such as clearing of vegetation. Well drilling equipment would typically be mounted on trucks that must be positioned at the drilling locations. Well installation could require several days or more. Following well installation, vegetation would return. Sampling of wells would require periodic, but brief, occupation of the sampling locations.

Remediation of MDAs and Other PRSs. Under the Capping Option, terrestrial resources would be disturbed as the MDAs were cleared of vegetation and then capped. At most MDAs, this activity would have minimal direct impact because the MDAs are generally grassy areas enclosed by fencing. However, siting and operation of temporary support facilities could disrupt some nearby habitat over the short term, and noise and human presence during remediation could also disturb wildlife in nearby areas. Proper maintenance of equipment and restrictions preventing workers from entering adjacent undisturbed areas would be implemented, as appropriate, to lessen impacts on ecological resources. Once the MDAs are capped and revegetated, they would provide habitat similar to that existing before remedial actions were implemented: they would be fenced, grassy areas. In the case of MDA G, the current industrial environment could be replaced by an open grassy area more attractive to wildlife. This would be the case whether or not any transuranic waste currently in subsurface storage in TA-54 would be left in place.

Regarding other PRSs, because partial clearing would often be needed, such as at the 260 Outfall, there would be a loss of habitat with an accompanying loss or displacement of wildlife. Upon completion of remedial actions, the sites would be revegetated. In the long run the sites containing the PRSs would return to a more natural condition absent further development to support LANL operations. Many PRSs such as firing sites in TA-15 may not require substantial clearing to remove contamination; thus, impacts may be restricted to short-term effects resulting from noise and increased human presence as the sites are remediated. Similar conclusions would be derived for other possible corrective reviews such as operation of volatile organic compound removal or groundwater treatment systems.

The Capping Option would have minimal impact, if any, on wetlands or aquatic resources. None of the MDAs contain such resources, as well as few, if any, of the other PRSs. Best management

practices would be implemented to prevent erosion and any subsequent sedimentation of downstream wetlands or ephemeral streams.

Although some of the MDAs fall within the core and buffer zones of the Mexican spotted owl (see Section I.4.5), direct impacts on this species are not expected from remediation activities, including capping. This sensitive species would not likely be present because of the disturbed nature of the sites. Additionally, remediation activities would not result in habitat loss. Indirect impacts on the Mexican spotted owl from noise are possible where MDAs are in or near Areas of Environmental Interest. Remedial action could in some cases generate noise levels that would be greater than 6 dBA above background levels. A LANL biological assessment determined that provided reasonable and prudent alternatives were implemented, work at MDAs N, Z, A, and AB may affect, but is not likely to adversely affect, the Mexican spotted owl. Reasonable and prudent alternatives include muted back-up indicators on heavy equipment, keeping disturbance and noise to a minimum, avoidance of unnecessary disturbance to vegetation including not removing trees having a diameter at breast height larger than 8 inches (20 centimeters), reseeding and erosion protection, and ensuring that any new lighting meets the requirements of the New Mexico Night Sky Protection Act. Also, activities involving heavy equipment would not be permitted between March 1 and May 15, or until the completion of surveys for spotted owls. If owls were determined to be present, work restrictions would be extended until August 31. Remediation of other areas evaluated in the biological assessment was determined to not affect the Mexican spotted owl (LANL 2006b). The U.S. Fish and Wildlife Service (USFWS) has concurred with this assessment (see Chapter 6, Section 6.5.2).

Although MDA D is within the Area of Environmental Interest for the bald eagle, no undeveloped habitat would be disturbed. A LANL biological assessment determined that remediation activities would likely result in noise levels exceeding 6 dBA above background levels in the core zone. The biological assessment concluded that provided reasonable and prudent alternatives were implemented, remediation activities may affect, but would not likely adversely affect, the bald eagle. Reasonable and prudent alternatives include reducing noise levels, not removing trees having a diameter at breast height greater than 8 inches (20 centimeters) (that is, roost trees), and providing erosion protection and prompt reseeding of disturbed areas. For other MDAs evaluated in the biological assessment, remediation activities were determined to not affect the bald eagle (LANL 2006b). The USFWS has concurred with this assessment (see Chapter 6, Section 6.5.2).

Although TA-54 includes a portion of the southwestern willow flycatcher Area of Environmental Interest, MDAs G and L are no closer than about 450 feet (137 meters) from the core habitat. Thus, there would be no direct loss of foraging or nesting habitat. Also, a LANL biological assessment determined that noise levels should not exceed 6 dBA above background levels in the core zone. Provided reasonable and prudent alternatives were implemented, the biological assessment concluded that the project may affect, but would not likely adversely affect, the southwestern willow flycatcher. Reasonable and prudent alternatives include designing all lighting so that it would be confined to the site, keeping disturbance and noise to a minimum, implementing appropriate erosion and runoff controls, avoiding unnecessary disturbance to vegetation (including wetland vegetation) and re-vegetating when needed with native plant species, and continuing to perform annual surveys adjacent to the project area before and during remediation. The biological assessment determined that the other remediation projects that were

evaluated would not affect the southwestern willow flycatcher (LANL 2006b). The USFWS has concurred with this assessment (see Chapter 6, Section 6.5.2).

Ecological risks from contaminants being reintroduced into the environment by ecological processes would be reduced. Caps over MDAs would be designed to prevent or reduce intrusion by roots or burrowing animals. The capped sites would be maintained in grassy states; shrubs and trees would be prevented from becoming established. Penetration of the waste by burrowing animals would be prevented by the design of barriers within final MDA covers. Ecological risks from contaminants at other PRSs (for example, the 260 Outfall and the firing sites) would be eliminated, if not reduced, because contamination would be stabilized, if not removed.

Borrow Pit. A portion of the 43 acres (17.4 hectares) containing the borrow pit is wooded. Greatly increased withdrawal of material from the pit may require clearing of additional acreage, thus eliminating wildlife habitat in the cleared areas. Expansion of the cleared area could also result in the removal of undeveloped buffer and core habitat for the Mexican spotted owl. Although the area is not within Areas of Environmental Interest for the bald eagle, the loss of potential foraging habitat could affect this species. The southwestern willow flycatcher Area of Environmental Interest is over 2.5 miles (4 kilometers) from the borrow pit; thus, impacts to this species are unlikely. Because expansion of the borrow pit was not evaluated in the DOE biological assessment (LANL 2006b), such an assessment, as well as consultation with the USFWS, would have to be undertaken before the expansion took place.

I.5.5.3 Removal Option

Site Investigations. Under the Removal Option, installation of exploratory and monitoring wells (or similar investigative features) in compliance with the Consent Order would cause some temporary environmental impacts such as clearing of vegetation.

Remediation of MDAs and Other PRSs. Impacts on ecological resources under the Removal Option would be similar to those described for the Capping Option. Although little habitat exists within the MDAs themselves, siting and operation of temporary remediation support facilities could disrupt some nearby habitat over the short term, and noise and human presence could disturb wildlife. This would probably occur whether removals are complete or partial. Yet once remediation actions are complete, the sites would be recontoured and revegetated. Because wastes would have been removed from the MDAs, there would be few restrictions on the types of plants that could be reintroduced. This would permit the establishment of more natural conditions that would, in turn, provide additional habitat for area wildlife.

Although remedial actions would create a disruptive environment for local wildlife in the short term, long-term impacts would be beneficial. With the removal of wastes and contamination from the MDAs and PRSs, deep-root penetration and burrowing animals would not reintroduce contamination to the environment. Thus, this option would result in long-term benefits because of reductions in contaminants.

Borrow Pit. Operation of the borrow pit would cause impacts on ecological resources that would be comparable to those under the Capping Option.

I.5.6 Human Health

This resource area addresses possible health impacts on workers and the public. Workers could be impacted by exposure to radionuclides or hazardous chemicals. Impacts on the public could result from future exposure to radionuclides from either PRS radionuclide releases or from future accidental occupation of DOE property resulting from temporary disruptions in institutional control.

Impacts on workers and the public could also result from transportation of waste or materials or from possible accidents at remediation sites. Possible transportation accidents are addressed in Section I.5.10; while accidents at remediation sites are addressed in Section I.5.12.

I.5.6.1 No Action Option

This option would continue the current program of environmental restoration.

I.5.6.1.1 Worker Impacts

There would be continuing risks to workers from exposure to ionizing radiation and hazardous chemicals. It is unlikely that these risks would be significantly larger, if at all, than current impacts and risks (see Section I.4.6). Worker radiation doses associated with the No Action Option were estimated using the procedures outlined in Sections I.3.5 and I.3.6.4. Personnel radiation exposures were estimated by calculating worker hours required to remove contaminated material and then multiplying these hours by an assumed average radiation dose environment. To these exposures were added those from waste processing and loading onto trucks. From FY 2007 through FY 2016, the total worker dose using this procedure was estimated to be 0.25 person-rem, or an LCF risk of 1.5×10^{-4} . From FY 2007 through FY 2011, the total worker dose was estimated to be 0.24 person-rem, or an LCF risk of 1.4×10^{-4} . In addition, workers could receive radiation doses from proximity of the PRSs being addressed to other LANL radiation sources. The total dose experienced by an environmental restoration worker could range up to several tens of millirem per year.

I.5.6.1.2 Public Impacts

There would be essentially no risk to the public from waste disposed of in the MDAs and contamination in the other PRSs for as long as DOE maintains control of the property and continues its surveillance and monitoring programs. But at some time in the future, there could be lapses in institutional controls and surveillance and monitoring programs. If this occurs, the largest risks to the public would result from accidental improper or unauthorized use of the property. Analyses for operation of low-level radioactive waste disposal facilities have long included assessments of radiological impacts on persons (inadvertent intruders) that have temporarily used property for activities such as housing construction or backyard gardening. In these assessments, intruders are assumed to excavate into the waste, thus contacting it and bringing it to the surface where it could be incorporated into the soil. Exposures could occur while the waste is inadvertently excavated and afterwards as persons use the property contaminated with radionuclides or organic or inorganic chemicals.

Inadvertent intruder scenarios are commonly addressed in performance assessments for low-level radioactive waste disposal facilities, including those performed for Area G in TA-54 (LANL 1997). Impacts on potential future inadvertent intruders have also been addressed as part of a No Action Alternative for the *Waste Isolation Pilot Plant Disposal Phase Final Supplemental Environmental Impact Statement* (DOE 1997a). As addressed in Section I.3.3.2.1.2.2, this No Action Alternative (not proposed or adopted by DOE) considered leaving all buried and stored transuranic waste in place at DOE generator-storage sites, including LANL. Impacts on intruders were assessed and included impacts of nonretrieval of remote-handled waste such as that in shafts 200 through 233 in Area G in TA-54.

I.5.6.2 Capping Option

I.5.6.2.1 Worker Impacts

There would be somewhat increased radiological doses received by site workers compared to the No Action Option. Worker doses from implementing the site investigations program under the Consent Order should be very small. Compared to the No Action Option, additional worker doses could result from capping the MDAs and annually remediating several PRSs. Using the procedures for estimating worker doses outlined in Sections I.3.5 and I.3.6.4, for FY 2007 through FY 2016, the total additional worker dose ranged from 9.7 to 13 person-rem, depending on whether a thin or thick cap was emplaced. This worker dose corresponds to an LCF risk ranging from 5.8×10^{-3} to 7.8×10^{-3} . For FY 2007 through FY 2011, the total additional worker dose ranged from 4.6 to 6.3 person-rem, and the LCF risk ranged from 2.8×10^{-3} to 3.8×10^{-3} .

In addition, small radiation doses to workers may result from actions associated with grouting the General's Tanks in MDA A or optionally stabilizing in place the transuranic waste currently stored in shafts 200-232 in Area G.⁸⁰ Operation of the TA-61 borrow pit to support MDA capping would not cause radiation exposures to borrow pit workers.

Risks to workers from possible exposure to hazardous or toxic chemicals would continue to be minimized through training, administrative controls, monitoring, and proper use of equipment.

I.5.6.2.2 Public Impacts

Site Investigations. Site investigation under the Consent Order should have no effects on public health.

Remediation of MDAs. Although the waste and contamination in the MDAs would remain in place, future risks to the public would be reduced. The improved covers would reduce infiltration of water into the waste, which would reduce the potential for release of radionuclides and hazardous constituents into the environment. The improved covers would also reduce the

⁸⁰ *In neither case are large worker doses expected. For example, the contents of a buried 50,000-gallon tank were mixed and removed at Oak Ridge National Laboratory using a fluidic pulse jet mixing system similar to the system considered for the General's Tank in MDA A. Although the tank contained sludge that had a larger inventory of activation and fission products than that expected to be in the General's Tanks (the sludge was, in fact, considered to be remote-handled material), the total radiation dose received by workers for the entire removal project was 1.23 person-rem, which was smaller than the planned dose of 4 person-rem estimated in the projected ALARA (as low as reasonably achievable) plan (ORNL 1998).*

potential for dispersion of contaminated materials currently existing as hotspots in soil, and as brought to the surface from burrowing animals.

The Capping Option would generally result in increased thicknesses of rock, tuff, and soil over the MDAs. This would reduce the risk to future potential inadvertent intruders. A larger thickness of cover implies less chance of contaminated material being contacted from future inadvertent intrusion into disposal units; if the contaminated material is contacted, less would be brought to the surface for dispersal and possible human exposure.

However, capping the MDAs would require the use of heavy equipment that would result in emissions of air pollutants, including criteria and hazardous contaminants. Particulate matter would be dispersed into the air from grading, earthmoving, and compaction at the MDA sites. These emissions could result in minor-to-moderate increases in short-term concentrations of criteria pollutants near the MDAs.

Remediation of Other PRSs. The Capping Option would result in removal of contaminated materials at numerous PRSs. At other PRSs, existing contamination would be fixed in place. Recovery of contamination at various PRSs at LANL may cause small quantities of radionuclides being released to the air that would cause public exposures to radiation. These exposures were estimated using the procedures described in Section I.5.6.3.2. The results of this assessment are an annual MEI dose of up to 7.5×10^{-3} millirem and an annual population dose of up to 1.8×10^{-2} person-rem. Operation of heavy equipment to remove contamination would release small quantities of nonradioactive pollutants into the air.

Borrow Pit. Operation of the borrow pit will entail the use of heavy equipment that would cause the emission of pollutants such as those addressed in Section I.5.4.2.1. In addition, particulate matter would be dispersed into the air from excavating bulk materials for MDA capping. These emissions may result in increases in short-term concentrations of pollutants near the boundary of the borrow pit.

I.5.6.3 Removal Option

I.5.6.3.1 Worker Impacts

Possible risks to site workers from the site investigations program from possible exposure to radiation or chemically toxic or hazardous materials would again be small.

Regarding remediation of MDAs and PRSs, the Removal Option would result in larger radiation doses to site workers than the Capping Option. Worker doses were estimated using the procedures outlined in Sections I.3.5 and I.3.6.4. Compared to the No Action Option, for FY 2007 through FY 2016, the total additional worker dose was estimated as 1,400 person-rem, assuming a thick cap over the remaining disposal units in the existing Area G footprint, and over small areas in TA-49. This results in an LCF risk of 0.84. For FY 2007 through FY 2011, the total additional worker dose was estimated as 580 person-rem, resulting in an LCF risk of 0.35. These estimates reflect the assumption of complete removal of waste from MDAs. Partial removal of waste from MDAs would result in smaller doses and risks to workers. Doses and risks could be reduced in practice using standard radiation protection techniques. The bulk of the

doses and LCF risks would be from complete removal of MDA G. Operation of the borrow pit to support MDA removal would not result in radiation doses to borrow pit workers.

Compared with the Capping Option, the Removal Option could result in increased risks to site workers from exposure to hazardous or toxic chemicals. These risks would be minimized through training, administrative controls, monitoring, and proper use of equipment.

I.5.6.3.2 Public Impacts

The Removal Option would reduce long-term risks to members of the public from either contaminants released slowly over time or inappropriate uses of the sites assuming temporary future accidental breakdowns in institutional control. The bulk of the contamination within and near the MDAs would be removed, and remaining contamination would be stabilized in place. Contamination at other PRSs would also be removed or stabilized in place.

Site Investigations. The site investigations programs under the Consent Order should not affect public health.

Radiological Emissions from Remediation of MDAs and Other PRSs. MDA removal would cause short-term radiological doses to the public from release of radionuclides into the air. To estimate these radiological doses:

- Transport through the air pathway to the public was modeled using the Clean Air Act Assessment Package – 1988 (CAP88-PC), Version 3.0. (See Appendix C of the SWEIS for further information on the CAP88-PC model.)
- Radiological doses and risks to the public were modeled using exposure and environmental transfer assumptions embedded in CAP88-PC. Exposures included external exposures from immersion in a radiological plume, inhalation and ingestion exposures, and exposures following deposition of contamination on the ground and surfaces, including resuspension and food transfer pathways. The public was assumed to take no measures to avoid radiation doses.
- Air emissions from removal of large MDAs were modeled as individual release sites. These MDAs included MDA A, B, T, U, AB, C, and G. Schedules for removal of these MDAs were conservatively assumed to comply with the remedy completion schedules in the Consent Order. Complete removal of waste and contamination was assumed.
- Remediation needs and schedules for other LANL PRSs are uncertain. Airborne releases were modeled by assuming that contamination is removed from an assumed area of property at LANL annually. The mechanical stresses imposed on the contaminated property were assumed to disperse contamination into the air.

It was assumed that during removal, a fraction of the radioactive inventory within the MDAs would be released into the air. The total source term for release was given as:

$$\text{Source Term (picocuries per year)} = \text{Total MDA Inventory (curies)} \times \text{Fraction Released}$$

The inventories for the MDAs were developed using several information sources. For some MDAs, although historical information indicated that particular isotopes may have been disposed of, disposed quantities were lacking. In these cases, the inventories were estimated by scaling to known inventories in MDA G. In addition, a documented safety analysis was issued in 2004 for nuclear environmental sites (LANL 2004). The analysis performed for this documented safety analysis reconsidered earlier information, and better accounted for the initial presence of plutonium-241 and the ingrowth of its progeny, americium-241. Where different inventories from different references could be assumed for some MDAs, doses (MEI and population within 50 miles) were calculated for each inventory, and the more conservative inventory (the one resulting in the larger dose) was used. In addition, because many MDAs have several radionuclides in their inventories, a screening process eliminated those radionuclides that contributed minimally (less than 1 percent) to the total dose. This screening resulted in those radionuclides having the largest health impacts being modeled. The postscreening inventories for each of the MDAs (and the combined PRS area) are listed in **Table I-93**.

The fraction of the inventory that would be released was generally assumed to be represented by PM_{10} . A conservative release fraction of 10^{-4} was assumed. Volatile radionuclides such as C-14, radon isotopes, and iodine were conservatively assumed to be all released (release fraction = 1). The release fraction for tritium was assumed to be 0.01 for MDA G and unity for other MDAs.

It is believed that very little of the tritium disposed of in the MDAs was disposed of in a gaseous form (as in vials of tritium gas). Rather, most tritium was disposed of as an absorbed liquid (generally tritiated water) or otherwise solid objects such as pumps. The great bulk of the tritium disposed of at LANL was disposed of within shafts within Area G at TA-54. Early disposals of large quantities of tritium were within asphalt-lined drums that were emplaced, rather than dropped, within the shafts (Rogers 1977). The largest quantities of tritium were double-packaged (one asphalt-lined and sealed drum within another). Shafts containing large quantities of tritium were asphalt-lined (Rogers 1977). Starting in the 1990s, disposal was within stainless steel containers.

Although many of the drums containing the tritium may have corroded to the point that there are leak paths from the drum interior to the environment, it is expected that the drums would still be sufficiently intact that widespread gross wall failures would be uncommon. Hence, the drums would largely retain their overall integrity during removal. In addition, it is expected that removal of waste from those shafts containing large quantities of tritium would be controlled in a manner sufficient to safeguard worker and public safety and the environment.

A release fraction of unity was assumed for tritium disposed of in other MDAs because of uncertainties about the form of the waste and the packaging used (if any).

All MDAs were modeled assuming that removal occurred with and without enclosures. For those MDAs assumed to be exhumed without enclosures, an area source was modeled. For such MDAs, it was assumed that, at any given time in the exhumation of an MDA, an area no larger than 100 square meters would be disturbed. The area source was modeled with zero velocity and zero height to the air emissions.

Table I-93 Screened Inventories of Radionuclides Within Large Material Disposal Areas and the Combined Potential Release Site Area ^a

| <i>Radionuclide (curies)</i> | <i>MDA A (TA-21)</i> | <i>MDA B (TA-21)</i> | <i>MDA T (TA-21)</i> | <i>MDA U (TA-21)</i> | <i>MDA AB (TA-49)</i> | <i>MDA C (TA-50)</i> | <i>MDA G (TA-54)</i> | <i>Combined PRS</i> |
|------------------------------|----------------------|----------------------|----------------------|----------------------|-----------------------|----------------------|----------------------|----------------------|
| Americium-241 | 6.14 | 6.55 | 3,740 | | 6,570 | 140 | 2,140 | 0.130 |
| Cobalt-60 | – | – | – | – | – | 8.42 | 480 | |
| Cesium-137 | – | – | – | – | – | – | 726 | 4.7×10^{-4} |
| Plutonium-238 | 0.266 | 9 | 31.3 | 0.414 | 2,990 | 6.7×10^{-9} | 3,590 | 0.14 |
| Plutonium ^b | 55.5 | 7.65 | 161 | 6.59 | 2,830 | – | 2,370 | 0.335 |
| Plutonium-241 | 78.9 | – | 37,400 | – | 3,370 | 82.9 | – | – |
| Strontium-90 | – | – | – | – | – | 12 | 1,040 | 0.013 |
| Tritium | – | 252 | – | 4.34 | 0.917 | 16,800 | 472,000 | 0.047 |
| Uranium ^c | 3.95 | 0.22 | 6.9 | – | 0.258 | 29.5 | 68 | 0.442 |

MDA = material disposal area, TA = technical area, PRS = potential release site.

^a The screening process eliminated those radionuclides contributing less than one percent of the total dose.

^b Plutonium may include plutonium-239 and plutonium-240.

^c Uranium may include uranium-233, uranium-234, uranium-235, uranium-236, or uranium-238.

Inventory sources:

MDA A – LANL 2004l for General's Tanks. For Eastern and Central Pits, available information (for example LANL 1991) identifies disposed radionuclides but not quantities. Hence, for these pits, the radionuclide inventories were scaled from known inventories in MDA G (LANL 1997).

MDA B – For plutonium-239, assumed 6.22 curies from LANL 1999b, DOE 1999g, and LANL 2004l, and added an estimated 1.45 curies of plutonium-240. For plutonium-240 and other radionuclides, because available information (Rogers 1977; LANL 1991, 1999b, 2004d) did not provide quantities, inventories were scaled from known inventories in MDA G (LANL 1997). A 2007 document estimates a plutonium-239 inventory ranging from 1.5 to about 15 curies, with an estimated 7.08 curies at the 50th percentile and 10.6 curies at the 90th percentile. The inventory in interstitial soil and backfill is estimated to be 4.53 curies at the 50th percentile and 5.87 curies at the 90th percentile. The remaining inventory is distributed among gloves, personal protective equipment, glassware, lab debris, and liquid containers (LANL 2007g), and would be expected to be less subject to airborne dispersal during normal removal operations than the inventory in the interstitial soil and backfill.

MDA T – LANL 2004l.

MDA U – The original inventory was estimated from available information (LANL 1991, 2004k). Some radionuclides were scaled from known inventories in MDA G (LANL 1997). Two-thirds of the original inventory was assumed removed in 1985. The Removal Option for MDA U is unlikely, because NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b).

MDA AB – Most radionuclides estimated from *RFI Work Plan for Operable Unit 1044* (LANL 1992b). Americium-241 was decayed from the cited inventory of plutonium-241. Inventories of plutonium-238 and plutonium-242 were scaled from known inventories in MDA G (LANL 1997).

MDA C – Radionuclide inventories were developed from data from LANL 1992c, LANL 2003k, Rogers 1977, and DOE 1999g.

MDA G – LANL 1997.

Combined PRS – Scaled from known inventories of contaminated soil disposed of into MDA G (LANL 1997).

Release of radionuclides from enclosures was modeled as a point source assuming a representative enclosure for all MDAs.⁸¹ (Enclosures would be relocated as needed.) The assumed enclosure has dimensions of 150 by 300 feet (46 by 91 meters), with a minimum height of 20 feet (6.1 meters) at the structure eaves. Assuming an elliptically domed roof having flat sides and a maximum height under the dome of about 40 feet (12 meters), the interior volume of the structure would be 1.25×10^6 cubic feet (35,400 cubic meters).

⁸¹ Additional engineering work would be needed to arrive at optimum numbers, sizes, configurations, and relocation schedules for the removal enclosures.

The ventilation system for the enclosure would be designed to provide sufficient air exchange to ensure that airborne concentrations would not exceed derived air concentration limits over a given period of time, based on a conservative estimate of entrainment of contaminants from the digface. It was assumed that the ventilation system would exhaust through a roughing filter and at least one HEPA filter before discharge through a 20-foot-high (6.1-meter-high), 36-inch-diameter (0.91-meter-diameter) stack. A 99.95 percent removal efficiency was assumed.⁸² The flow rate out the stack was assumed to be 20,000 cubic feet per minute, corresponding to an average air exchange rate within the enclosure of once per hour. This flow rate was converted to 14.4 meters per second by dividing by the cross-sectional area of the stack.

When determining the distance and direction from each MDA to the MEI, the land parcels that are designated as “To Be Conveyed” were considered. For additional CAP88-PC input, the same meteorological, population, and agriculture values and data were used here as in Appendix C of this SWEIS. (The location [latitude and longitude] that was used for each MDA is available in the administrative record.)

In addition to the MDAs addressed above, it was assumed that each year from FY 2007 through FY 2016, several small PRSs would be remediated at different locations within LANL. There may be several options for remediation, including removing, treating, or stabilizing contamination at a site. It was assumed that some of these remediation activities would annually cause release of radionuclides to the air from mechanical disturbance of soil, sediment, or other property. To estimate this release, a single PRS combined area was assumed to represent the annual remediation of several PRSs. The radioactive inventory subject to disturbance was estimated by extrapolating the radionuclide inventory in “contaminated soil,” as reported disposed of in Area G from 1971 through September 25, 1988 (LANL 1997). The average radionuclide concentrations from this inventory, which was contained within 47,000 cubic yards (36,000 cubic meters) of disposed contaminated soil, was extrapolated to an assumed annual radiologically contaminated volume of 5,200 cubic yards (4,000 cubic meters).⁸³ Because of the large number of PRSs within TA-35 (see Section I.2.7.7), the location of the combined PRS area was assumed to be within TA-35.

The results of the analysis are presented in **Table I-94** for complete removal of waste from the large MDAs. The annual dose was calculated by dividing the total dose from MDA removal by the number of years needed to exhume the entire MDA. Smaller doses are expected from partial removal of waste from the MDAs. The annual MEI dose associated with the combined PRS area would be 7.5×10^{-3} millirem, and the annual population dose would be 1.8×10^{-2} person-rem.

⁸²A single HEPA filter has a nominal rating of 99.97 percent efficiency for particulate removal, as designed and tested for 0.3-micrometer (1.2×10^{-6}) aerodynamic-equivalent diameter. This is equivalent to a leak rate of 3×10^{-4} . In practice, however, a lower level of efficiency is often assumed. Assuming an efficiency of 99.8 percent for one HEPA filter, and an efficiency of 99.7 percent for a second HEPA filter, the particulate release rate for two filters would be 6×10^{-6} . For purposes of this analysis, a more conservative release rate of 5×10^{-4} (99.95 percent efficiency) was used.

⁸³Pit inventories from 1971 through September 1988 are provided in Table 3-8 of Appendix 2e of the 1997 Area G performance assessment and composite analysis (LANL 1997). Contaminated soil inventories were obtained from this table, and disposed volumes were obtained from Table 3-7 of this reference. The estimate of 5,200 cubic yards (4,000 cubic meters) was estimated assuming annual waste generation rates from remediating several PRSs. The inventory used for the analysis conservatively reflect the possibility that all waste removed from PRSs in any single year may be radioactively contaminated.

Table I-94 Annual Dose Estimates from Complete Removal of Large Material Disposal Areas

| MDA | Removal Period (years) | Individual MDA MEI Dose (millirem per year)^a | Dose to LANL MEI^{b, c} (millirem per year) | Population Dose (person-rem per year)^c |
|--------------------|-------------------------------|--|--|--|
| MDA A | 1.8 | 0.0013 to 7.1 | 0.000097 | 0.00066 |
| MDA B ^d | 2.4 | 0.062 to 50 | 0.0081 | 0.024 |
| MDA T | 2.0 | 0.064 to 310 | 0.0043 | 0.036 |
| MDA U ^e | 0.8 | 0.0025 to 1.9 | 0.047 | 0.31 |
| MDA AB | 2.1 | 0.030 to 85 | 0.0017 | 0.056 |
| MDA C | 1.8 | 0.45 to 1.2 | 0.34 | 5.5 |
| MDA G | 6.8 | 0.18 to 97 | 0.012 | 0.25 |
| Total | Not applicable | Not applicable | 0.42 | 6.2 |

MDA = material disposal area, MEI = maximally exposed individual.

^a A different MEI was assumed for removal of each MDA. The smaller dose for each MDA is for removal assuming use of an enclosure; the larger dose is for removal assuming no use of an enclosure.

^b Total dose of the LANL MEI was conservatively estimated by assuming that all listed MDAs would be removed during an overlapping period of time, which would probably not actually occur.

^c Doses are based on using enclosures except at MDAs C and U.

^d Due to the high potential dose to the MEI, an enclosure would be used at MDA B. Consequently, even if the plutonium inventory were higher (see Table I-93), the offsite doses would be low.

^e The Removal Option for MDA U is unlikely, because NMED has issued a Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b).

Note: Numbers have been rounded.

The MEI location for each MDA was calculated separately. Those MEI locations for the four MDAs at TA-21 are very close. The other MDAs are relatively distant from one another. In this table, the "Individual MDA MEI Dose" is to the MEI associated with each MDA removal. The smaller dose would be received if the MDA is removed under an enclosure. If the MDA is exhumed without an enclosure, the MEI would receive the larger dose.

Because the MEI locations for the TA-21 MDAs are so close, the total dose to that MEI (MDAs A, B, T, and U) was assessed assuming that all removals occurred at the same time under enclosures (0.13 millirem per year). If removal of MDA U occurred, which is unlikely (see footnote c to Table I-94), and without use of an enclosure, the dose to the TA-21 MEI would increase to 2 millirem (1.9 millirem for MDA U plus the lower doses for MDAs A, B and T) in a year assuming the release assumptions and the inventory presented in Table I-93. If MDA A was also exhumed without the use of an enclosure, the dose to the TA-21 MEI could potentially exceed the 10-millirem public dose limit (7.1 millirem for MDA A plus 1.9 millirem for MDA U plus 1.5 millirem dose to TA-21 from operations at LANSCE). Notwithstanding this assessment, LANL would be operated, and remediations conducted, to ensure compliance with the 10-millirem public dose limit.

In addition to addressing doses to each MEI associated with large-MDA removal, the impacts of MDA removal on the LANL site-wide MEI were analyzed. Each MDA could add to the LANL site-wide MEI dose. In Table I-94, the doses to the LANL site-wide MEI were calculated separately. Doses from removal of MDA U and MDA C were calculated without use of enclosures because their contribution to the LANL site-wide MEI dose would be small. (Total doses to the LANL MEI from all sources are summarized in Chapter 5 of the SWEIS.)

When calculating the dose to the population within 50 miles (80 kilometers) of each MDA, it was assumed that MDA U and MDA C would be exhumed using no enclosures. All other large MDAs would be removed under enclosures. As much as an additional 6.2 person-rem per year would be attributed to the LANL population dose if all large MDAs were exhumed at the same time.

Nonradiological Emissions from Remediating MDAs and Other PRSs. The Removal Option would require the use of heavy equipment, resulting in emission of pollutants to the air, including criteria and hazardous pollutants. At some MDAs, these activities would be of longer duration than typical LANL construction activities and could involve extensive movement of materials. The overall emissions from heavy equipment under the Removal Option would be more than 20 times those under the Capping Option. As noted in Section I.5.4.3.1, emissions of some pollutants could be above 1-hour and 8-hour ambient standards. These emissions could be reduced by management controls such as scheduling so that public impacts would be minimized.

Borrow Pit. Operation of the borrow pit under the Removal Option could result in emissions of pollutants and particulate matter that would be comparable to those estimated for the Capping Option. Particulate emissions would be controlled using standard dust control techniques such as water sprays. Emissions could be controlled by management controls such as scheduling.

I.5.7 Cultural Resources

A variety of cultural resources are present within or near LANL boundaries, including archaeological resources, historic buildings and structures, and traditional cultural properties.

I.5.7.1 No Action Option

Under the No Action Option, there would be small risks to cultural resources at any of the TAs within which MDAs and PRSs are located, as the LANL environmental restoration project continues. These small risks would be managed using existing procedures.

I.5.7.2 Capping Option

Site Investigations. Installation of monitoring wells or other site investigation equipment under the Consent Order would be coordinated with LANL personnel responsible for preservation of cultural resources, with the objective of avoiding impacts on cultural resources. Usually there is sufficient flexibility in the selection of sites for investigation equipment so that impacts on cultural resources can be avoided.

Remediation of MDAs and Other PRSs. Under this option, the MDAs would be cleared of vegetation before being capped. Because no archaeological resources are within any of the MDAs, the Capping Option would not directly impact such sites. This would also be the case for actions involving grouting the General's Tanks in MDA A (see Section I.3.3.2.2.5) or actions performed to provide additional stabilization to any transuranic waste left in place in TA-54, if this option is implemented (see Section I.3.3.2.1.2.2).

Risks to cultural resources for other PRSs would depend on the PRS. In most cases, there would be few or no risks to cultural resources. At sites where there may be questions about risks,

remediation operational plans and procedures would be coordinated with LANL personnel responsible for preservation of cultural resources. For example, one building eligible for listing in the National Register of Historic Places is within the R-44 firing site (SWMU 15-006(c)); however, this building would not be disturbed by remediation activities involving surface recovery of contamination.

Indirect impacts on cultural resources of remedial actions are possible because of increased erosion resulting from capping operations or PRS remediation and from workers or equipment occupying the work area. In those cases where archaeological resource sites and historic buildings and structures are located near work areas, LANL personnel responsible for preservation of cultural resources would be notified so that site boundaries could be marked and fenced, as needed (LANL 2006l). Fencing would prevent accidental intrusion and disturbance to the site. Best management practices would control erosion.

Borrow Pit. There are no archaeological resources in the immediate vicinity of the borrow pit in TA-61.

I.5.7.3 Removal Option

Site Investigations. Possible impacts on cultural resources of site investigations under the Consent Order would be the same as those under the Capping Option.

Remediation of MDAs and Other PRSs. Potential impacts under this option would be similar to those addressed for the Capping Option. Direct impacts on cultural resources would be unlikely. The potential for indirect impacts also would be similar to that under the Capping Option. As with that option, LANL personnel responsible for preservation of cultural resources would be notified so that any resource sites located near the affected areas would be protected. These conclusions would apply whether complete or partial removal occurred at the MDAs.

Borrow Pit. There are no archaeological resources in the immediate vicinity of the borrow pit in TA-61.

I.5.8 Socioeconomics and Infrastructure

I.5.8.1 No Action Option

Under the No Action Option, existing employment practices for LANL's environmental restoration project would continue, with contractor labor providing much of the support for site investigation and remediation. LANL's environmental restoration project currently employs 45 to 50 University of California and captive contractors,⁸⁴ along with 250 subcontractors who support various tasks at various levels (LANL 2006a). This may be compared with the total employment at LANL, which is currently about 13,500 employees (see Section I.4.8.1). Using the procedures outlined in Sections I.3.5 and I.3.6.4, total personnel hours were estimated through FY 2016 for removal of contaminated material from PRSs as part of the No Action Option. This estimate is 50,000 person-hours through FY 2016 (48,000 person-hours through FY 2011). Utility usage (electricity, natural gas, water) would not be significantly affected by

⁸⁴ A DOE captive contractor is one that engages in little or no commercial business outside its work for DOE.

continuing environmental restoration project operations. Roughly 75,000 gallons (280,000 liters) of liquid fuel (diesel and gasoline) would be required to operate heavy equipment for continuing site remediation through FY 2016.

I.5.8.2 Capping Option

Under the Capping Option, a higher density of remedial activities would occur through FY 2016 compared to the No Action Option. Including operations at the TA-61 borrow pit, carrying out the Capping Option is projected to require 1,400,000 to 2,200,000 person-hours through FY 2016 (680,000 to 1,100,000 person-hours through FY 2011). Assuming 2,000 hours per year per worker, the Capping Option would require the full-time efforts of an average of 70 to 110 workers per year.

Use of electricity or natural gas would likely be only marginally increased compared to the No Action Option. Roughly 3.9 to 6.7 million gallons (15 to 25 million liters) of liquid fuel (diesel and gasoline) may be needed through FY 2016 to operate heavy equipment under the Capping Option.

Compared to the No Action Option, additional water would be required, mainly for soil compaction at the MDAs and dust suppression at the MDAs and borrow pit. Implementing the Capping Option could require from 20 to 53 million gallons (76 to 200 million liters) of water from FY 2007 through FY 2016, with the largest annual quantity of water (roughly 5 to 14 million gallons [19 to 53 million liters]) needed during FY 2011.

I.5.8.3 Removal Option

Under the Removal Option, a very high density of remedial activities would conservatively occur through FY 2016 compared to the No Action Option. Under the Removal Option, complex and cost-intensive excavation processes would provide local economic benefits.

Including operations at the TA-61 borrow pit, and capping areas in TA-54 and TA-49, carrying out the Removal Option is projected to require up to 36 million person-hours through FY 2016 (16 million person-hours through FY 2011), assuming complete removal of waste from MDAs and covering the remaining disposal units in the existing Area G footprint with a thick cap. Assuming 2,000 hours per year per worker, the Removal Option would require the full-time efforts of an average of 1,800 workers per year.

Utility use may be affected. Significant additional volumes of waste would be generated, and it may be necessary to develop additional capacity to sort, characterize, treat, and package all the waste to be removed (see Section I.3.3.2.8 and Section I.5.9.3). Use of this additional capacity would increase utility infrastructure demands at LANL. Operation of heavy equipment for exhuming MDAs and performing other actions under the Removal Option is projected to require use of up to 70 million gallons (260 million liters) of liquid fuel (diesel and gasoline) through FY 2016. Water use through FY 2016 would be comparable to that under the Capping Option, or up to 58 million gallons (220 million liters).

I.5.9 Waste Management

I.5.9.1 No Action Option

The quantities of solid, chemical, and radioactive wastes to be generated would generally be consistent with, if not smaller than, previous projections of waste for continued operation of LANL. There should be no difficulty in accommodating the waste in existing on- and offsite low-level radioactive waste treatment and disposal facilities. Solid waste disposal capacity exists in nearby locations in New Mexico. Chemical waste treatment and disposal capacity exists at several locations within 600 miles of LANL. Low-level radioactive waste disposal capacity exists at LANL, and offsite capacity exists for the relatively small quantities of mixed low-level radioactive waste projected from LANL's environmental restoration project.

The expansion of low-level radioactive waste disposal operations into Zone 4 would accommodate the low-level radioactive wastes to be generated by LANL's environmental restoration project for the foreseeable future. Using the onsite disposal capacity in conjunction with possible use of offsite disposal capacity would allow flexibility to address short-term increases in waste generation from planned environmental restoration activities.

Only very small quantities of transuranic waste would be generated by LANL's environmental restoration project. Quantities of environmental restoration project wastes contaminated with high explosives are expected to be small compared to other sources at LANL.

Otherwise, LANL's environmental restoration project is not expected to generate liquid wastes (industrial, hazardous, radioactive) in volumes that would impact existing LANL treatment capacity. Because the No Action Option is not expected to significantly increase personnel needs at LANL, there would be no impact on LANL's capacity to treat sanitary wastes.

I.5.9.2 Capping Option

Although the Capping Option may cause generation of somewhat larger quantities of solid, liquid, and sanitary wastes compared with the No Action Option, impacts on LANL's waste management infrastructure should be small. Solid waste disposal capacity exists in nearby locations in New Mexico. Chemical wastes would be transported offsite for treatment and disposal. Quantities of environmental restoration wastes contaminated with high explosives should be small compared to several other sources at LANL.

Low-level radioactive waste disposal capacity exists at LANL and offsite, and would not be significantly impacted by the expected waste volume under this option. Offsite capacity exists for the relatively small quantities of mixed low-level radioactive waste projected from LANL's environmental restoration project. Only small quantities of transuranic waste would be generated by LANL's environmental restoration project and would not significantly increase current transuranic waste generation rates. Impacts on WIPP would hence be small.

Otherwise, compared to the No Action Option, LANL's environmental restoration project would generate somewhat larger quantities of liquid wastes (industrial, hazardous, radioactive), but not in quantities that by themselves would tax existing LANL treatment capacity. Because the

Capping Option is not expected to significantly increase personnel requirements, compared to the No Action Option, LANL's capacity to treat sanitary wastes should not be impacted.

I.5.9.3 Removal Option

The Removal Option would result in large quantities of wastes being excavated, requiring sorting, characterization, classification, treatment, packaging, shipment, and disposal. The material would include physically or chemically hazardous materials, and some would present external exposure or inhalation hazards. This may require development of additional waste management capacity as discussed in Section I.3.3.2.8. Development and use of this capacity would require increased use of utilities such as gas, water, or electricity, increased use of natural resources, and larger personnel requirements. These impacts would occur for the time required to remove and process the waste from the MDAs. Any structures constructed and used for this purpose would have to be safely decommissioned, which could generate additional quantities of waste to be treated, packaged, shipped, and disposed of.

Compared with the Capping Option, the Removal Option would generate much larger quantities of low-level radioactive waste—about 1 million cubic yards of bulk, alpha-contaminated, and remote handled wastes. About 180,000 cubic yards of mixed low-level radioactive wastes would also be generated. Low-level radioactive wastes would be generated from the environmental restoration program at annual rates that would exceed current plans for annual waste acceptance at Zone 4 of TA-54. The Zone 4 disposal capacity could be used within a shorter period of time than planned, requiring sooner expansion into Zone 6. Use of offsite disposal capacity would alleviate these impacts.

The amount of transuranic waste that would be exhumed from the MDAs is significant. WIPP personnel would need to review this potential waste stream to determine if its acceptance would remove future flexibility for WIPP to manage other new waste streams.

The significantly increased volumes of solid and chemical wastes would be transported offsite for treatment or disposal. In addition, compared to existing levels, the greatly increased personnel requirements for waste removal would cause increased sanitary system loads.

I.5.10 Transportation

Risks to the public could result from transportation of waste or bulk materials. Risks from transporting waste could include those from radiation exposures under normal transport conditions or from possible accidents resulting in physical injury or radiation exposure from release of radioactive material.

I.5.10.1 No Action Option

There would be continuing use of transportation systems within and near LANL. The transportation implications of continuing the LANL environmental restoration project would generally be comparable with those projected under the Expanded Operations Alternative of the 1999 SWEIS (DOE 1999a).

I.5.10.1.1 Onsite Impacts

The No Action Option should not significantly affect existing traffic patterns within LANL. There would be some impacts associated with transporting low-level radioactive waste to onsite disposal facilities. These impacts are addressed in Section I.5.10.1.2.

I.5.10.1.2 Offsite Impacts

Transportation impacts were determined for the No Action Option using the annual projected waste volumes set forth in Section I.3.6 and the analysis assumptions described in Section I.3.5. Shipment crew and population radiation doses and risks from incident-free transportation and radiological and nonradiological risks from possible transportation accidents are presented in **Table I-95**. The table presents total doses and risks from FY 2007 through FY 2016, total doses and risks from FY 2007 through FY 2011, and the doses and risks for the peak year (2008).

These impacts were determined assuming that all nonradioactive wastes would be sent to offsite facilities, all transuranic wastes would be sent to WIPP, and all low-level and mixed low-level radioactive wastes would be sent to an offsite commercial disposal facility such as the one in Utah. Impacts of incident-free transport are presented in terms of the collective dose in person-rem resulting in excess LCFs. Excess LCFs are the number of cancer fatalities that may be attributed to the proposed project that are estimated to occur in the exposed population over the lifetime of the individuals. If the number of LCFs is smaller than one, the subject population is not expected to incur any LCFs. Impacts of possible transportation accidents are presented in terms of population risks (LCFs) from exposure to releases of radioactivity and fatalities anticipated from traffic accidents. Accident fatalities were estimated from exposure to radiation (LCFs) and from nonradiological injuries caused by collisions.

Table I-95 No Action Option Transportation Impacts Summary

| <i>Time Period</i> | <i>Crew Dose and Risk</i> | | <i>Population Dose and Risk</i> | | <i>Accidents</i> | |
|-------------------------|---------------------------|------------|---------------------------------|------------|---------------------------|---|
| | <i>Person-Rem</i> | <i>LCF</i> | <i>Person-Rem</i> | <i>LCF</i> | <i>Radiological (LCF)</i> | <i>Nonradiological (traffic fatalities)</i> |
| FY 2007 through FY 2016 | 2.2 | 0.0013 | 0.61 | 0.00037 | 0.0000072 | 0.019 |
| FY 2007 through FY 2011 | 1.8 | 0.0011 | 0.49 | 0.00030 | 0.0000067 | 0.018 |
| Peak Year (FY 2008) | 0.75 | 0.00045 | 0.20 | 0.00012 | 0.0000027 | 0.0074 |

LCF = latent cancer fatality, FY = fiscal year.

Note: Numbers have been rounded.

However, low-level and mixed low-level radioactive wastes may be optionally transported to a DOE facility such as the Nevada Test Site or disposed onsite (assuming that mixed low-level radioactive waste capacity would be developed at LANL). Comparative impacts considering these options are presented in **Table I-96** for FY 2007 through FY 2016. The risks of developing excess LCFs are highest for workers under the offsite disposal options. This is because the dose is proportional to the duration of transport, which in turn is proportional to travel distance. Disposal at the Nevada Test Site, which is farthest from LANL, would cause the highest dose and risk, although the dose and risk would be low under all disposal options. Because all LCFs shown in the table are smaller than unity, the analysis indicates that no excess fatal cancers would result, either from dose received from packaged waste on trucks or

potentially received from accidental release. Likewise, no fatalities are expected from traffic accidents.

Table I-96 No Action Option Comparison of On- and Offsite Radioactive Waste Disposal Transportation Impacts (Fiscal Year 2007 through Fiscal Year 2016)

| Low-Level and Mixed Low-Level Waste Destination ^a | Total Distance Traveled (million kilometers) | Crew Dose and Risk | | Population Dose and Risk | | Accidents | |
|--|--|--------------------|------------|--------------------------|------------|-----------------------|--------------------------------------|
| | | Person-Rem | Risk (LCF) | Person-Rem | Risk (LCF) | Radiological (LCF) | Nonradiological Traffic (fatalities) |
| LANL ^b | 0.21 | 0.56 | 0.00034 | 0.18 | 0.00011 | 7.9×10^{-10} | 0.0043 |
| DOE ^c | 1.97 | 2.5 | 0.00015 | 0.69 | 0.00041 | 9.6×10^{-6} | 0.022 |
| Commercial ^d | 1.72 | 2.2 | 0.0013 | 0.61 | 0.00037 | 7.2×10^{-6} | 0.019 |

LCF = latent cancer fatality.

^a All nonradiological wastes would be shipped offsite and all transuranic wastes would be shipped to WIPP.

^b Modeled by assuming an average one-way distance of nine kilometers from the point of generation to the disposal site such as that in Technical Area 54.

^c Modeled by assuming shipment to the Nevada Test Site.

^d Modeled by assuming shipment to the EnergySolutions site in Utah.

Note: To convert kilometers to miles, multiply by 0.62137. Numbers have been rounded.

I.5.10.2 Capping Option

I.5.10.2.1 Onsite Impacts

Site Investigations. Although the site investigation program under the Consent Order may slightly increase vehicular traffic in and near LANL, this additional traffic should not significantly impact current traffic patterns. For example, installation of boreholes or monitoring wells would require the mobilization of equipment to the investigation site, followed by demobilization once installation is completed. Additional traffic would be associated with delivery of supplies and transport of personnel. Thereafter, periodic investigation site visits may be needed to collect samples. Sampling monitoring wells may involve the collection and temporary storage of purged groundwater and decontamination water before approved disposal. Collected water may need to be trucked to treatment facilities.

Remediation of MDAs and Other PRSs. The Capping Option would cause additional traffic in and near LANL. Additional workers would be needed to cap the MDAs, which would mean additional personal vehicles in the LANL vicinity. Additional radioactive and nonradioactive wastes could be sent to LANL treatment and disposal facilities. (Impacts associated with transporting low-level and mixed low-level radioactive waste to onsite disposal facilities are addressed in Section I.5.10.2.2.) Onsite risks from transporting this material could be mitigated or reduced through measures such as traffic control (site security), road closures, or transportation infrastructure improvements.

In addition, the Capping Option would require numerous shipments of tuff, rocks, and similar bulk materials from sources either on the LANL site or within the surrounding community. There could be some additional shipments of materials needed to grout the General's Tanks in MDA A. In addition, depending on remediation decisions, wastewater may be generated from groundwater treatment programs or from decontamination of equipment. There could be an

increase in traffic to transport the wastewater to onsite treatment facilities. This larger number of shipments compared with the No Action Option presents an increased short-term risk to the public and LANL personnel from possible accidents. Risks from transporting this material to onsite personnel could be reduced by measures such as temporary road closures. There would also be small increases in traffic volumes to move equipment, modular structures, or other materials needed to support stabilization and capping operations.

As addressed in Section I.5.4.2.2, compared to the No Action Option, the Capping Option may increase traffic on East Jemez Road if solid waste from LANL’s environmental restoration project is processed through the solid waste transfer station on East Jemez Road and tuff and similar material are procured from the TA-61 borrow pit. It is expected, however, that solid waste from LANL’s environmental restoration project would be sent directly to a landfill without passing through the transfer station.

Another consideration is traffic into and out of DP Mesa for remediation of the TA-21 MDAs. Capping MDAs A, B, T, and U is projected to require slightly over 4 years. The total number of waste, soil, and similar bulk material shipments is shown in **Table I-97** for FY 2007 through FY 2016, as well as FY 2007 through FY 2011. Shipments are two way—for example, trucks delivering tuff and then leaving. Shipments would use DP Road, which intersects with Trinity Road at its western end.

Table I-97 Capping Option Shipments of Waste and Bulk Materials into and out of Technical Area 21 ^a

| Waste and Material Shipments ^b | Fiscal Year | | | | Total Shipments |
|--|-------------|--------|--------|------|-----------------|
| | 2009 | 2010 | 2011 | 2012 | |
| Waste shipments ^b | 1 | 260 | 300 | 1 | 560 |
| Soil and Other Materials ^b | | | | | |
| Minimum cap | 1,200 | 8,400 | 5,300 | 39 | 15,000 |
| Maximum cap | 3,200 | 23,000 | 15,000 | 110 | 41,000 |
| Total Shipments | | | | | |
| Minimum cap | 1,200 | 8,700 | 5,600 | 40 | 16,000 |
| Maximum cap | 3,200 | 23,000 | 15,000 | 110 | 41,000 |
| Total Shipments per Day ^c | | | | | |
| Minimum cap | 4.7 | 35 | 22 | 0.2 | Not applicable |
| Maximum cap | 13 | 93 | 59 | 0.4 | Not applicable |

^a Assuming two-way shipments—that is, trucks entering and leaving Technical Area 21 via DP Road.

^b Conservatively includes shipments for capping MDAs B and U. Current plans are to remove waste from MDA B and capping MDA U may be unlikely considering NMED’s 2006 Corrective Action Complete with Controls certification for SWMUs comprising MDA U (NMED 2006b).

^c Assuming 250 working days per year.

Note: Numbers have been rounded.

Traffic congestion could be reduced by redesigning the intersection of DP Road and Trinity Road.

Borrow Pit. See above discussion.

I.5.10.2.2 Offsite Impacts

Site Investigations. The site investigations program under the Consent Order should have few, if any, offsite impacts.

Remediation of MDSs and Other PRSs. Compared with the No Action Option, there would be additional shipments of radioactive and nonradioactive wastes to offsite treatment and disposal facilities. These shipments would occur over public roads and could therefore present risks to the public. These risks would be managed by packaging and shipping wastes in compliance with U.S. Department of Transportation requirements for shipment of radioactive materials.

Transportation impacts were estimated for the Capping Option using annual projected waste volumes estimated in Section I.3.6 and the assumptions and analysis described in Section I.3.5. Shipping crew and population radiation doses and risks from incident-free transportation and radiological and nonradiological risks from possible transportation accidents are presented in **Table I-98**. The table presents total doses and risks from FY 2007 through FY 2016, total doses and risks from FY 2007 through FY 2011, and doses and risks for the peak year (2008).

Table I-98 Capping Option Transportation Impacts Summary

| <i>Time Period</i> | <i>Crew Dose and Risk</i> | | <i>Population Dose and Risk</i> | | <i>Accidents</i> | |
|-------------------------|---------------------------|------------|---------------------------------|------------|---------------------------|---|
| | <i>Person-Rem</i> | <i>LCF</i> | <i>Person-Rem</i> | <i>LCF</i> | <i>Radiological (LCF)</i> | <i>Nonradiological (traffic fatalities)</i> |
| FY 2007 through FY 2016 | 3.9 | 0.0023 | 1.0 | 0.00062 | 0.000015 | 0.076 |
| FY 2007 through FY 2011 | 2.8 | 0.0017 | 0.75 | 0.00045 | 0.000011 | 0.048 |
| Peak year (FY 2008) | 0.87 | 0.00052 | 0.23 | 0.00014 | 0.0000033 | 0.012 |

LCF = latent cancer fatality, FY = fiscal year.
 Note: Numbers have been rounded.

The impacts for Table I-98 were determined assuming that solid and chemical wastes would be shipped to offsite facilities, transuranic wastes would be shipped to WIPP, and low-level and mixed low-level radioactive wastes would be sent to an offsite commercial facility such as the one in Utah. However, low-level and mixed low-level radioactive wastes may be optionally transported to a DOE facility such as the Nevada Test Site or disposed onsite (hypothetically assuming that mixed low-level radioactive waste capacity would be developed at LANL). Comparative impacts considering these options are presented in **Table I-99** for FY 2007 through FY 2016. The risks of developing excess LCFs are again highest for workers under the offsite disposal options. Disposal at the Nevada Test Site, which is farthest from LANL, would cause the highest dose and risk, although the dose and risk would be low under all disposal options. Because all LCFs would be much smaller than unity, no excess fatal cancers would result from this activity, either from dose received from packaged waste on trucks or potentially received from accidental release. Likewise, no nonradiological fatalities are expected from traffic accidents.

Borrow Pit. Operation of the borrow pit in TA-61 would have no offsite impacts from material transport.

Table I-99 Capping Option Comparison of On- and Offsite Radioactive Waste Disposal Transportation Impacts (Fiscal Year 2007 through Fiscal Year 2016)

| Low-Level and Mixed Low-Level Radioactive Waste Destination ^a | Total Distance Traveled (million kilometers) | Crew Dose and Risk | | Population Dose and Risk | | Accidents | |
|--|--|--------------------|------------|--------------------------|------------|----------------------|--------------------------------------|
| | | Person-Rem | Risk (LCF) | Person-Rem | Risk (LCF) | Radiological (LCF) | Nonradiological Traffic (fatalities) |
| LANL ^b | 2.67 | 0.76 | 0.00045 | 0.24 | 0.00014 | 1.1×10^{-9} | 0.0044 |
| DOE ^c | 6.45 | 4.4 | 0.0026 | 1.2 | 0.00070 | 2.0×10^{-5} | 0.082 |
| Commercial ^d | 5.92 | 3.9 | 0.0023 | 1.0 | 0.00062 | 1.5×10^{-5} | 0.076 |

LCF = latent cancer fatality.

^a All nonradiological wastes would be shipped offsite and all transuranic wastes would be shipped to WIPP.

^b Modeled by assuming an average one-way distance of 9 kilometers from the point of generation to the disposal site such as that in Technical Area 54.

^c Modeled by assuming shipment to the Nevada Test Site.

^d Modeled by assuming shipment to the EnergySolutions site in Utah.

Note: Numbers have been rounded.

I.5.10.3 Removal Option

I.5.10.3.1 Onsite Impacts

Site Investigations. Impacts of site investigations under the Consent Order would be the same as those under the Capping Option.

Remediation of MDAs and Other PRSs. Compared to the Capping Option, this option would cause additional traffic in and near LANL. Additional workers would be needed to remove the wastes from the MDAs and to carry out sorting, characterization, treatment, and packaging activities. This indicates a larger number of personal vehicles in the LANL vicinity, which could cause traffic congestion in some areas, such as on Pajarito Road and other roads near TA-54 or near the intersection of DP and Trinity Roads. There would be additional radioactive and nonradioactive wastes sent to LANL treatment and disposal facilities (see Section I.5.10.3.2). Onsite risks from transporting this material could be mitigated or reduced through measures such as traffic control (site security), road closures, and transportation infrastructure improvements.

In addition, the Removal Option would require numerous shipments of crushed tuff for backfilling excavations. These shipments would be accompanied by shipments of topsoil or soil amendment to promote revegetation. There may also be shipments transporting wastewater generated from groundwater treatment programs or from decontaminating equipment. This larger number of material shipments compared with the No Action Option presents an increased short-term risk to the public and LANL personnel associated with possible accidents. Risks to onsite personnel could be reduced by appropriate road closures and other traffic control measures or transportation infrastructure improvements.

As addressed in Section I.5.4.3.2, compared to the No Action Option, the Removal Option may increase traffic on East Jemez Road if solid waste from LANL’s environmental restoration project is processed through the solid waste transfer station on East Jemez Road and tuff and similar material are procured from the TA-61 borrow pit. It is expected, however, that industrial solid waste generated from LANL’s environmental restoration project would be sent directly to a landfill without passing through the transfer station.

Regarding TA-21, complete removal of MDAs A, B, T, and U is projected to cause two-way shipments of waste, soil, and similar bulk materials, as summarized in **Table I–100**. Average daily shipments for the peak year (2010) would be in the range of those estimated for the Capping Option. As for the Capping Option, traffic congestion could be reduced by measures such as redesigning the intersection of DP Road with Trinity Road.

Table I–100 Removal Option of Wastes and Bulk Materials into and out of Technical Area 21^a

| Waste and Material Shipments ^b | Fiscal Year | | | | | Total Shipments |
|---|-------------|--------|--------|-------|-------------|-----------------|
| | 2008 | 2009 | 2010 | 2011 | 2012 | |
| Waste shipments | 4,000 | 7,300 | 5,500 | 1,700 | 10 | 19,000 |
| Soil and Other Materials | | | | | | |
| Crushed tuff | 3,400 | 6,200 | 4,600 | 1,500 | 10 | 16,000 |
| Additional material | 230 | 440 | 3,209 | 100 | 1 | 1,100 |
| Total shipments | 7,600 | 14,000 | 10,000 | 3,300 | 21 | 35,000 |
| Total shipments per day ^c | 31 | 56 | 42 | 13 | Less than 1 | |

^a Assuming two-way shipments – that is, trucks entering and leaving Technical Area 21 via DP Road.

^b Conservatively includes shipments for removing MDA U. Removing MDA U may be unlikely considering NMED’s 2006 Corrective Action Complete with Controls certification for the SWMUs comprising MDA U (NMED 2006b).

^c Assuming 250 working days per year.

Note: Because all numbers have been rounded, the sums may not equal indicated totals.

Borrow Pit. See above discussion.

I.5.10.3.2 Offsite Impacts

Site Investigations. The site investigations program under the Consent Order should have few, if any, offsite impacts.

Remediation of MDAs and Other PRSs. Compared with the No Action Option, there would be additional shipments of radioactive and nonradioactive wastes to offsite disposal facilities. These shipments would occur over public roads and could therefore present risks to the public. These risks would be managed by packaging and shipping wastes in compliance with U.S. Department of Transportation requirements for shipment of radioactive materials.

Transportation impacts were determined for the Removal Option using annual projected waste volumes estimated in Section I.3.6 and the assumptions and analysis described in Section I.3.5. Shipping crew and population radiation doses and risks from incident-free transportation and radiological and nonradiological risks from possible transportation accidents are presented in **Table I–101**. The table presents total doses and risks for FY 2007 through FY 2016, doses and

risks from FY 2007 through FY 2011, and doses and risks for the peak year during this 10-year period. Smaller doses and risks would occur under the assumption of partial rather than complete removal of waste from MDAs.

Table I-101 Removal Option Transportation Impacts Summary

| <i>Time Period</i> | <i>Crew Dose and Risk</i> | | <i>Population Dose and Risk</i> | | <i>Accidents</i> | |
|-------------------------|---------------------------|------------|---------------------------------|------------|---------------------------|-------------------------------------|
| | <i>Person-Rem</i> | <i>LCF</i> | <i>Person-Rem</i> | <i>LCF</i> | <i>Radiological (LCF)</i> | <i>Nonradiological (fatalities)</i> |
| FY 2007 through FY 2016 | 630 | 0.38 | 190 | 0.12 | 0.0012 | 2.2 |
| FY 2007 through FY 2011 | 390 | 0.23 | 120 | 0.071 | 0.00064 | 1.2 |
| Peak year (FY 2010) | 160 | 0.10 | 50 | 0.030 | 0.00025 | 0.46 |

LCF = latent cancer fatality, FY = fiscal year.

Note: Offsite shipments of low-level and mixed low-level radioactive wastes (low-activity, remote-handled, and alpha) would be split between disposal facilities. Numbers have been rounded.

The impacts for Table I-101 were determined assuming that solid and chemical wastes would be shipped to offsite facilities, transuranic wastes would be shipped to WIPP, and low-activity low-level and mixed low-level radioactive wastes would be sent to an offsite commercial facility such as the one in Utah. The remaining low-level radioactive wastes (remote-handled and alpha wastes and mixed remote-handled and mixed wastes) would be sent to a DOE facility such as the Nevada Test Site. However, options were considered of shipping all low-level radioactive and mixed low-level radioactive wastes to a DOE facility such as the Nevada Test Site, or disposing of all such waste on the LANL site. Note that the commercial facility in Utah cannot accept wastes having characteristics similar to those assumed in this appendix for remote-handled and alpha-contaminated low-level radioactive and mixed wastes. In addition, there is no current mixed low-level radioactive waste disposal capacity at LANL.

Comparative impacts considering these options are presented in **Table I-102** for FY 2007 through FY 2016. The risks of developing excess LCFs are highest for workers under the offsite disposition options. Disposal at the Nevada Test Site, which is farthest from LANL, would result in the highest dose and risk. Transportation of radioactive wastes would not result in any excess LCFs among the exposed truck crew or population. The largest risk to the population from radioactive waste transport could result from (nonradiological) traffic fatalities resulting from accidents. Considering that the transportation activities would occur over a 10-year period and that the average number of traffic fatalities in the United States is about 40,000 per year, the total traffic fatalities (about two to three) estimated under the Removal Option are small.

Borrow Pit. Operations of the borrow pit would have no offsite impacts from material transport.

Table I–102 Removal Option Comparison of On- and Offsite Radioactive Waste Disposal Transportation Impacts (Fiscal Year 2007 through Fiscal Year 2016)

| <i>Low-Level and Mixed Low-Level Radioactive Waste Destination^a</i> | <i>Total Distance Traveled (million kilometers)</i> | <i>Crew Dose and Risk</i> | | <i>Population Dose and Risk</i> | | <i>Accidents</i> | |
|--|---|---------------------------|-------------------|---------------------------------|-------------------|---------------------------|---|
| | | <i>Person-Rem</i> | <i>Risk (LCF)</i> | <i>Person-Rem</i> | <i>Risk (LCF)</i> | <i>Radiological (LCF)</i> | <i>Nonradiological Traffic (fatalities)</i> |
| LANL ^b | 11.1 | 65 | 0.039 | 20 | 0.012 | 8.6×10^{-8} | 0.16 |
| DOE ^c | 241 | 660 | 0.40 | 200 | 0.12 | 1.5×10^{-3} | 2.4 |
| Commercial ^d | 220 | 630 | 0.38 | 190 | 0.12 | 1.3×10^{-3} | 2.2 |

LCF = latent cancer fatality.

^a All nonradiological wastes would be shipped offsite and all transuranic wastes would be shipped to WIPP.

^b Modeled by assuming an average one-way distance of 9 kilometers from the point of generation to the disposal site such as that in Technical Area 54.

^c Modeled by assuming shipment to the Nevada Test Site.

^d Modeled by assuming shipment of bulk low-level and mixed low-level radioactive wastes to the EnergySolutions site in Utah, and the remaining low-level and mixed low-level radioactive wastes to the Nevada Test Site.

Note: Numbers have been rounded.

I.5.11 Environmental Justice

I.5.11.1 No Action Option

The primary route designated by the State of New Mexico to be used for radioactive and other hazardous material shipments to and from LANL is the approximately 40-mile (64-kilometer) corridor between LANL and I-25 at Santa Fe. This route passes through the Pueblos of San Ildefonso, Pojoaque, Nambe, and Tesuque and is adjacent to the northern segment of Bandelier National Monument. This primary transportation route bypasses the city of Santa Fe on New Mexico 599 to I-25. Minority populations dominate these communities. Total waste shipments under the No Action Option, assuming all environmental restoration project waste is shipped offsite, are estimated at 1,050 shipments, or 2,100 total truck trips. (Half of the total trips would consist of empty returning trucks.) The highest number of waste shipments is projected to be 400 shipments (800 total truck trips) in 2008, or approximately 3 truck trips per working day (assuming 250 working days per year).

Table 4–52 in Chapter 4 of this SWEIS shows average daily vehicle trips eastbound on NM 502 east of its intersection with NM 4. Eastbound trips averaged 10,100 per day, while westbound trips averaged 7,765 per day (totaling 17,865 vehicle trips). Waste shipments consisting of about 3 truck trips per working day under the No Action Option would represent 0.02 percent of the total traffic (17,865 vehicle trips) on NM 502.

I.5.11.2 Capping Option

Additional wastes would be generated at LANL under the Capping Option, and, to the extent that the wastes must be trucked offsite for treatment or disposal, additional impacts could potentially occur on minority communities through which these waste shipments would pass. Assuming that all waste is shipped offsite through these affected communities, there would be approximately 7,200 waste shipments, or 14,400 total truck trips via NM 502 through 2016. (Half of the total trips would consist of empty returning trucks.) The largest number of waste shipments is

projected to be 970 shipments (1,940 total truck trips) in 2008, or approximately 8 truck trips per working day (assuming 250 working days per year). Waste shipments consisting of 8 truck trips per working day under the Capping Option would represent 0.04 percent of the total traffic (17,865 vehicle trips) on NM 502.

I.5.11.3 Removal Option

Additional wastes would be generated at LANL under the Removal Option, and to the extent that the wastes must be trucked offsite for treatment or disposal, additional impacts could potentially occur on minority communities through which these waste shipments would pass. Assuming that all waste is shipped offsite through these affected communities, there would be approximately 110,000 waste shipments, or 220,000 total truck trips via NM 502 through 2016, an average of 11,000 shipments (22,000 truck trips) per year. (Half of the total trips would consist of empty returning trucks.) The highest number of waste shipments is projected to be 22,000 shipments (44,000 total truck trips) in 2010, or approximately 180 truck trips per working day (assuming 250 working days per year). Fewer shipments would occur if partial, rather than full, removal of MDAs took place, or if onsite disposal is used for some waste. Waste shipments consisting of 180 truck trips per working day under the Removal Option would represent about 1 percent of the total traffic (17,865 vehicle trips) on NM 502.

I.5.12 Accidents

The primary focus of this section is the risk-dominant accidents under the Removal Option.

Before any of the corrective measure options described in this appendix take place, appropriate planning and safety reviews would occur. The extent of the planning, safety review, and related preparatory activities would be commensurate with the size of the task and the extent of the possible hazard. Preparatory activities would include assessments similar to those conducted for remediation of MDA H by Omicron, Inc. (Omicron 2001). In this study, slightly more than 150 potential accident scenarios were postulated for the proposed MDA H corrective measure options. Process hazard analyses were performed on postulated accidents that were not screened out based on the likelihood of their occurrence and their potential effect on human health. Unmitigated and mitigated public, worker, and transportation risks associated with excavating MDA H were assessed. Activities included site preparation; site excavation; sorting and segregation of waste; declassification, packing, and loading of waste; waste transportation; and site restoration. The spectrum of hazards considered included industrial hazards, fires, explosions, spills, and penetrating radiation (DOE 2004b).

The Omicron assessment concluded that accidents involving the exposure of the public to radioactive or hazardous materials left in place at MDA H were not credible (a chance of occurrence of less than 1 in 1 million). Excavation and removal corrective measure options (including associated transportation) posed the greatest risk to members of the public, albeit a small one. The risk to the public from all other activities was negligible. The risk to workers was dominated by standard industrial accidents, followed by possible explosion accidents (Omicron 2001).

Safety analyses consistent with the likely level of hazard and the scope of the corrective measure contemplated would be performed for each of the MDAs and PRSs considered in this SWEIS.

I.5.12.1 Risks to Public

There would be low risks to the public from accidents involving radioactive or hazardous materials left in place in the MDAs. For neither the No Action Option nor the Capping Option would waste and hazardous constituents within the MDAs be disturbed. Materials that could be present in sufficient concentrations to potentially react in a manner involving violent dispersal of contamination (for example, chunks of high explosive, pyrophoric uranium, uranium hydride) are buried. The buried materials would generally lack sufficient oxygen to support combustion or ignition. In addition, most of the MDAs are relatively distant from residential areas. The MDAs closest to a residential area are in TA-21. Of these MDAs, MDA B is about 0.2 miles distant, and the remaining MDAs in TA-21 are typically about 0.4 miles distant. (MDA B, however, is near businesses on DP Road in TA-21.)

The principal risk to the public from accidents under the Capping Option would be from transportation accidents involving shipments of bulk materials and waste. Much of the transportation of materials and waste would take place within LANL, as crushed tuff is trucked from onsite borrow areas. Some materials may be acquired from locations nearby, but outside of, LANL. In this case, there could be small levels of increased risks to the public from transportation accidents. These risks could be mitigated by measures such as those described in Section 1.5.10.2.1.

Risks to the public from accidents from shipments of waste to locations outside of LANL have been addressed in Section I.5.10.1.2 for the No Action Option and Section I.5.10.2.2 for the Capping Option.

In addition to the risks from waste and bulk material transportation, removing waste from the MDAs would disturb buried materials and possibly cause conditions that would increase the likelihood of an undesired chemical reaction or release of materials. Materials such as high explosive and pyrophoric uranium may be present. The assessment for excavation of MDA H determined that of the 33 hazards analyzed (most with two or more initiating events), only an offsite transportation accident posed a credible threat to the public. The most serious effects were death or serious injury from the physical force of the accident. Risks from accidents involving transporting waste under the Removal Option to locations away from LANL have been addressed in Section I.5.10.3.2.

Site-specific assessments would consider the potential for such risks and mitigative actions. But for purposes of this appendix, bounding accidents that might occur during complete removal of two MDAs were addressed. Accidents involving airborne dispersal of radioactive materials were considered for MDA G because it has the largest estimated radionuclide inventory at LANL. Accidents involving airborne dispersal of radiological materials and toxic chemicals were considered for MDA B because of its proximity to the LANL site boundary.

Accidents Involving Release of Radioactive Materials. Removal of waste and contamination from MDAs would probably occur under enclosures for which any contaminant that may be

dispersed into the air during removal would be passed through HEPA filtration systems before release. An explosion was assumed to occur at MDA G that breaches the enclosure and bypasses the HEPA filters. It was assumed that accident mitigation would not be completed for 24-hours; thus, suspension of the waste for this time period was included with the initial explosive release.

Although several fires occurred while operating MDAs B and C, and in one reported event several cartons gave off minor explosions, there is no experience at LANL with explosions associated with MDA remediation or removal. The documented fires and minor explosions involved packages of fresh waste containing unauthorized or reactive materials before their burial. Materials postulated for removal from MDAs B and G will have been covered and mixed with soil for up to 60 years. Therefore, past occurrences of fires and minor explosions during MDA operation are not an indication of the frequencies of fires and explosions that could occur during removal. In addition, the documented fires and explosions during past operations all involved far smaller quantities of materials at risk than those assumed for the SWEIS (see below). Also as noted below, removal operations would be conducted so that the quantities of materials at risk being removed at any one time would be smaller than those quantities assumed for the accident analysis.

The potential for explosive blast accidents associated with operations at LANL facilities that process high explosives was assessed, and, again, as of the 1999 SWEIS, no such experience was identified at LANL (DOE 1999a). (High explosive processing includes storage, synthesis, formulation, pressing, machining, assembly, quality assurance processes, shipping and receiving of high explosives, and disposal at facilities in several LANL TAs.) Based on site-specific experience at Pantex, an annual accident frequency range of 10^{-3} to 10^{-2} was assumed for the No Action Alternative for the 1999 SWEIS (DOE 1999a). An annual accident frequency of 10^{-2} was assumed for possible explosive accidents under the MDA G Removal Option.

It is believed that MDA B does not contain a sufficient quantity of explosives that could result in a significant release (LANL 2006c). At the time MDA B was operating, explosives production and test areas used what is now called MDA R in TA-16 for disposal of explosive waste (LANL 2007g). The chosen accident scenario for this MDA is a fire that results in releases that breach the enclosure and the HEPA filters. The specific materials and quantities of chemicals and fire sources in the MDA are poorly known, and, therefore, so is the frequency of occurrence of the hypothesized scenario. The frequency used for the explosion scenario at MDA G was ascribed to the fire at MDA B to facilitate radiological risk calculations.

Radiological accident impacts were determined using the MELCOR Accident Consequence Code System, Revision 2, Version 1.13.1 (MACCS2), using parameter assumptions appropriate for the LANL region. The impacts estimated from the analysis are presented in terms of consequences and risks. All consequences were determined assuming that the accident does occur and, therefore, the frequency or probability that the accident occurs was not taken into account. The risks of the accident do reflect the frequency of occurrence and were calculated by multiplying the accident's frequency (1×10^{-2} per year) by its consequences. Dose consequences, in rem for an individual or person-rem for a group of individuals, were estimated for the MEI located at the site boundary (390 yards [355 meters] from MDA G and 49 yards [45 meters] from MDA B), the offsite population out to a distance of 50 miles (80 kilometers), and a noninvolved worker located about 110 yards (100 meters) from the accident. Consequences are also

expressed in terms of the likelihood of an LCF for the MEI and noninvolved worker and in terms of the number of additional fatalities for the surrounding populations. A conversion factor of 0.0006 LCFs (or number of LCFs) per rem (or person-rem) was used to convert dose to health effects; this factor is doubled for dose to an individual in excess of 20 rem.

For MDA G, the source term was assumed to be given by one of the early disposal pits in which transuranic-contaminated waste was disposed of. This waste was disposed of before the 1970 decision to place transuranic-contaminated material into retrievable storage. The radionuclide inventory for pits 1 through 6 at MDA G has been estimated in the performance assessment and composite analysis for the Area G low-level radioactive waste disposal site (LANL 1997). Because there was no information about the distribution of radionuclides between pits, a material at risk corresponding to one-sixth of the inventory in pits 1 through 6 was assumed, reflecting the assumption that no more than a single pit would be involved in the accident.⁸⁵

MDA B was one of the earliest disposal sites at LANL and operated when radioactive material, particularly plutonium, was scarce and expensive. The estimated plutonium inventory in MDA B (about 100 grams) is considered to be conservative (LANL 2006i). The distribution of radionuclide contamination throughout MDA B is unknown. As noted in Section I.3.3.2.7, MDA B may consist of several (up to six) small disposal pits plus two chemical trenches and two areas of contamination. The material at risk was conservatively assumed to consist of one-half of the total estimated MDA B inventory to reflect the possibility that the contamination in MDA B may be concentrated in only a few small pits.

For both of these MDAs, the radionuclides considered in the analysis were limited in accordance with a screening process to the principal dose-contributing radionuclides. **Table I-103** shows the list of radionuclides plus other analytical parameters used in the accident analysis.

The estimated consequences and annual risks from an explosion at MDA G or a fire at MDA B are shown in **Tables I-104** and **I-105**. These tables include doses and risks as calculated for a noninvolved worker assumed to be 109 yards (100 meters) from the accident.

MDA G consequences and risks bound those of MDA B because of the larger source term in MDA G (see Table I-103). For the MEI, the difference in doses and risks between these two MDAs is smaller than would be expected from the source term difference because of the much closer distance to the MEI for MDA B than for MDA G.

⁸⁵ It may be argued that the radionuclide inventory may be concentrated in a few of the six pits. However, there is little information with which to estimate this possibility. In any event, if the MDA was removed, only a small portion of any pit would be exposed at any one time. Also note that the early pits at MDA G were large in size (far larger in size than those projected for MDA B). Hence, it is very unlikely that the entire contents of any single pit at MDA G would be involved in any accident involving an explosion or similar reactive event.

Table I-103 Analytical Parameters for Assumed Accidents at Material Disposal Area G and Material Disposal Area B

| MDA | Accident Phase | Nuclide | MAR (Ci) | DR ^{a, b} | ARF ^b | RF ^b | ARR (/hr) ^b | LPF | ST-Ci | DEL T (min) | | |
|---------------|----------------|----------------|-------------------|--------------------|------------------|-----------------|------------------------|-----|-----------------------|-------------|-----------------------|-------|
| MDA G | Explosion | Americium-241 | 352 | 0.02 | 0.005 | 0.3 | | 1 | 0.014 | 1 | | |
| | | Gadolinium-148 | 0.466 | 1 | 0.005 | 0.3 | | 1 | 0.000699 | 1 | | |
| | | Thorium-230 | 2.67 | 1 | 0.005 | 0.3 | | 1 | 0.00401 | 1 | | |
| | | Actinium-227 | 0.0430 | 1 | 0.005 | 0.3 | | 1 | 0.0000645 | 1 | | |
| | | Plutonium-238 | 591 | 0.88 | 0.005 | 0.3 | | 1 | 0.780 | 1 | | |
| | | Plutonium-239 | 319 | 0.96 | 0.005 | 0.3 | | 1 | 0.459 | 1 | | |
| | | Plutonium-240 | 74.7 | 1 | 0.005 | 0.3 | | 1 | 0.112 | 1 | | |
| | | Plutonium-241 | 219 | 1 | 0.005 | 0.3 | | 1 | 0.329 | 1 | | |
| | | Uranium-233 | 1.03 | 0 ^c | 0.005 | 0.3 | | 1 | 0 | 1 | | |
| | | Uranium-234 | 0.392 | 1 | 0.005 | 0.3 | | 1 | 0.000588 | 1 | | |
| | | Uranium-238 | 1.72 | 1 | 0.005 | 0.3 | | 1 | 0.00258 | 1 | | |
| | | MDA B | Suspension | Americium-241 | 352 | 0.02 | | 1 | 4.00×10^{-6} | 1 | 0.000659 | 1,440 |
| | | | | Gadolinium-148 | 0.464 | 1 | | 1 | 4.00×10^{-6} | 1 | 0.0000445 | 1,440 |
| Thorium-230 | 2.66 | | | 1 | | 1 | 4.00×10^{-6} | 1 | 0.000255 | 1,440 | | |
| Actinium-227 | 0.0428 | | | 1 | | 1 | 4.00×10^{-6} | 1 | 4.11×10^{-6} | 1,440 | | |
| Plutonium-238 | 588 | | | 0.88 | | 1 | 4.00×10^{-6} | 1 | 0.0497 | 1,440 | | |
| Plutonium-239 | 318 | | | 0.96 | | 1 | 4.00×10^{-6} | 1 | 0.0292 | 1,440 | | |
| Plutonium-240 | 74.3 | | | 1 | | 1 | 4.00×10^{-6} | 1 | 0.00714 | 1,440 | | |
| Plutonium-241 | 218 | | | 1 | | 1 | 4.00×10^{-6} | 1 | 0.0209 | 1,440 | | |
| Uranium-233 | 1.03 | | | 0 ^c | | 1 | 4.00×10^{-6} | 1 | 0 | 1,440 | | |
| Uranium-234 | 0.390 | | | 1 | | 1 | 4.00×10^{-6} | 1 | 0.0000374 | 1,440 | | |
| Uranium-238 | 1.71 | | | 1 | | 1 | 4.00×10^{-6} | 1 | 0.000164 | 1,440 | | |
| MDA B | Fire | | | Actinium-227 | 0.000159 | 1 | 0.0005 | 1 | | 1 | 7.95×10^{-8} | 1 |
| | | | | Americium-241 | 3.01 | 1 | 0.0005 | 1 | | 1 | 0.00151 | 1 |
| | | Tritium | 116 | 1 | 1 | 1 | | 1 | 116 | 1 | | |
| | | Plutonium-238 | 4.15 | 1 | 0.0005 | 1 | | 1 | 0.00208 | 1 | | |
| | | Plutonium-239 | 3.10 ^d | 1 | 0.0005 | 1 | | 1 | 0.00155 | 1 | | |
| | | Plutonium-240 | 0.671 | 1 | 0.0005 | 1 | | 1 | 0.000336 | 1 | | |

| MDA | Accident Phase | Nuclide | MAR (Ci) | DR ^{a, b} | ARF ^b | RF ^b | ARR (/hr) ^b | LPF | ST-Ci | DEL T (min) |
|-----|----------------|---------------|----------|--------------------|------------------|-----------------|------------------------|-----|-----------------------|-------------|
| | | Plutonium-241 | 0.428 | 1 | 0.0005 | 1 | | 1 | 0.000214 | 1 |
| | | Uranium-233 | 0.0211 | 1 | 0.0005 | 1 | | 1 | 1.06×10^{-5} | 1 |
| | | Uranium-234 | 0.00712 | 1 | 0.0005 | 1 | | 1 | 3.56×10^{-6} | 1 |
| | | Uranium-238 | 0.0687 | 1 | 0.0005 | 1 | | 1 | 3.44×10^{-5} | 1 |
| | Suspension | Actinium-227 | 0.000159 | 1 | | 1 | 4.00×10^{-6} | 1 | 1.53×10^{-8} | 1440 |
| | | Americium-241 | 3.01 | 1 | | 1 | 4.00×10^{-6} | 1 | 0.000289 | 1440 |
| | | Tritium | 0 | 1 | | 1 | 4.00×10^{-6} | 1 | 0 | 1440 |
| | | Plutonium-238 | 4.15 | 1 | | 1 | 4.00×10^{-6} | 1 | 0.000398 | 1440 |
| | | Plutonium-239 | 3.10 | 1 | | 1 | 4.00×10^{-6} | 1 | 0.000297 | 1440 |
| | | Plutonium-240 | 0.671 | 1 | | 1 | 4.00×10^{-6} | 1 | 0.0000644 | 1440 |
| | | Plutonium-241 | 0.428 | 1 | | 1 | 4.00×10^{-6} | 1 | 0.0000411 | 1440 |
| | | Uranium-233 | 0.0211 | 1 | | 1 | 4.00×10^{-6} | 1 | 2.02×10^{-6} | 1440 |
| | | Uranium-234 | 0.00712 | 1 | | 1 | 4.00×10^{-6} | 1 | 6.83×10^{-7} | 1440 |
| | | Uranium-238 | 0.0687 | 1 | | 1 | 4.00×10^{-6} | 1 | 6.59×10^{-6} | 1440 |

MDA = material disposal area, MAR = material at risk (units of curies); DR = damage ratio; ARF = airborne release fraction; RF = respirable fraction; ARR = airborne release rate; LPF = leakpath factor; ST-Ci = source term (units of curies); DEL T = time period of exposure (minutes).

^a DR smaller than unity indicates presence of nondispersable (concrete and sludge) waste forms.

^b Values for DR, ARF, ARR, and RF were assumed from information in the DOE handbook for airborne release fractions and rates (DOE 1994), and from comparison to other environmental statements addressing similar accidents involving plutonium-contaminated materials (DOE 1998a, 1999f).

^c DR is zero for uranium-233 because all uranium-233 was disposed within nondispersable (concrete and sludge) waste forms.

^d A 2007 document estimates a total plutonium-239 inventory in MDA B ranging from 1.5 to about 15 curies, with an estimated 7.08 curies at the 50th percentile and 10.6 curies at the 90th percentile. The inventory distributed among gloves, personal protective equipment, glassware, lab debris, and liquid containers is estimated to be 2.55 curies at the 50th percentile and 4.73 curies at the 90th percentile (LANL 2007g). For accident analysis purposes, the balance of the inventory distributed in interstitial soil and fill would be less likely to disperse in a fire than the inventory distributed in the other material. If all of the other material was involved in the fire, the plutonium-239 material at risk would be about 50 percent higher at the 90th percentile than that assumed for the analysis.

Table I-104 Material Disposal Area Explosion or Fire: Radiological Accident Consequences

| Accident Location | Maximally Exposed Individual | | Offsite Population to 80 Kilometers | | Noninvolved Worker (at 100 meters) | |
|--------------------|------------------------------|-------------------------------------|-------------------------------------|--|------------------------------------|-------------------------------------|
| | Dose (rem) | Latent Cancer Fatality ^a | Dose (person-rem) | Latent Cancer Fatality ^{b, c} | Dose (rem) | Latent Cancer Fatality ^a |
| MDA G | 55 | 0.066 | 770 | 0.46 | 410 | 0.49 |
| MDA B ^d | 7.1 | 0.0043 | 7.8 | 0.0047 | 1.6 | 0.00095 |

MDA = material disposal area.

^a Increased risk of an LCF to an individual, assuming the accident occurs.

^b Increased number of LCFs for the population, assuming the accident occurs.

^c Offsite population size out to a 50-mile (80-kilometer) radius is approximately 343,000 from MDA G and 271,600 from MDA B.

^d The calculated impact could be up to 50 percent higher (see Table I-103).

Table I-105 Material Disposal Area Explosion or Fire: Radiological Accident Risks

| Accident Scenario | Latent Cancer Fatality Risk per Year of Operation | | |
|--------------------|---|--|---|
| | Maximally Exposed Individual ^a | Offsite Population (to 50 Miles) ^{b, c} | Noninvolved Worker (at 100 meters) ^a |
| MDA G | 0.00066 | 0.0046 | 0.0049 |
| MDA B ^d | 4.3×10^{-5} | 4.7×10^{-5} | 9.5×10^{-6} |

MDA = material disposal area.

^a Increased risk of an LCF to an individual per year. Risks were determined by conservatively assuming an accident frequency of 1×10^{-2} per year.

^b Increased number of LCFs for the population per year.

^c Offsite population size out to a 50-mile (80-kilometer) radius is approximately 343,000 from MDA G and 271,600 from MDA B.

^d The calculated impact could be up to 50 percent higher (see Table I-103).

The MEI for MDA B is a hypothetical maximally exposed individual assumed to be positioned 45 meters from the accident at MDA B. Because this individual is hypothetical and certain very conservative assumptions are attributed to him (see Appendix D), he is not included in the calculation of population dose.

These calculated doses and risks are conservative. For example, the assumed airborne release and respirable release fractions for MDA B are the same as those used in other analyses for fires involving newly generated combustible materials (for example, DOE 1998a, 1999f), an assumption that discounts the effects of decades of exposure of the buried waste to the environment. Furthermore, before removal would actually occur at any MDA, thorough safety reviews would take place with the intent of identifying hazard scenarios and the barriers associated with preventing or mitigating each postulated hazard scenario. If it is determined that a possible hazard would actually be credible and significant, then measures would be taken to address the hazard. For example, if an explosion or similar reactive event was deemed credible and significant, exhumation could take place in an inert atmosphere, as has been considered as an option for MDA H (DOE 2004b). For removal of MDA B, several technical and administrative controls will be imposed to ensure safety, including visual inspections, use of several or remote sensing tools to monitor for radiation or hazardous constituents, and controls that limit the plutonium equivalent that may be present in different areas associated with MDA B removal. These areas and their plutonium equivalent include the dig face and excavation enclosure

(2.4 grams [0.15 curies]); the Definitive Identification Facility and field laboratory (7.0 grams [0.43 curies]); onsite transportation (2.4 grams [0.15 curies]); waste container storage area number 1 (7.0 grams (0.43 curies); and waste container storage area number 2 (28.0 grams [1.7 curies]) (LANL 2006a). The plutonium equivalent limits for each of these areas are smaller than the material at risk for the accident analysis presented here for MDA B removal. For the dig face and excavation enclosure the limit is 5 percent of the assumed material at risk.

Accidents Involving Release of Toxic Chemicals. A toxic chemical accident analysis for the MDAs was performed using the ALOHA code⁸⁶ and a conservative accident scenario postulated to result in the maximum human health effects of the atmospheric release of toxic chemicals. MDA B was chosen for this analysis because of its proximity to members of the public. Chemical releases from possible accidents at other MDAs having chemical inventory uncertainties equivalent to MDA B (see below) are expected to result in smaller impacts because of their greater distances to members of the public.

LANL staff have postulated that over 200 different chemicals may have been placed in MDA B for disposal of substances prior to its closure. There are no definitive records of the types or quantities of chemicals that were disposed of in MDA B. Therefore, conservative assumptions were made about the presence and quantity of toxic chemicals in the MDAs. That is, a hazardous chemical accident analysis was developed based on selecting the more toxic chemicals that could be present at MDA B and a quantity commensurate with current knowledge of the historical uses of these chemicals. The release scenario, a fire that breaches the enclosure and bypasses the HEPA filter, is consistent with that used to analyze radiological releases. The thermal energy that would accompany such a fire and that would tend to loft the plume over potential nearby receptors was conservatively ignored. (An explosion would also loft chemicals over potential nearby receptors.)

Within the context of the aforementioned data limitations, the list of possible chemicals was evaluated in terms of their potential effects on human health. A number of chemicals, either alone or in combination with others, could cause a fire. A fire is expected to release larger quantities of chemicals to the atmosphere than most other realistic accident initiators.

A measure of a chemical's relative toxicity is the numerical value of its Emergency Response Planning Guideline (ERPG), which is an air concentration value associated with a specific human health response. A lower ERPG indicates a more toxic chemical (see Appendix D). The list of chemicals that may be present in MDA B was reviewed for those chemicals with the lowest ERPG values, in addition to their maximum possible quantity. This review identified gases (sulfur dioxide, hydrogen chloride, hydrogen bromide), liquids (hydrofluoric acid, hydrochloric acid), and a solid (beryllium powder) having restrictive ERPG concentrations. Each of these chemicals was assumed to be disposed of in quantities consistent with their historical use. Sulfur dioxide and beryllium were found to be the most restrictive of these and were considered further. The identification of sulfur dioxide as the most restrictive non-solid-phase chemical was in agreement with a LANL determination, based on a detailed assessment of over 200 chemicals, of the aboveground inventory limits for chemicals to be staged or stored in a DIF

⁸⁶ The ALOHA code is a public domain code developed by EPA and the National Oceanic and Atmospheric Administration and used to plan for and respond to chemical emergencies. The code is widely used throughout the DOE complex for safety analysis applications.

and surrounding storage and staging area (LANL 2006c). The DIF will be constructed and operated to support the investigation and remediation program for MDA B.

Given the dearth of information on specific chemicals present, their quantity, degradation over more than 50 years, or environmental transport from the MDA, this accident analysis serves to quantify an approximate distance within which significant human health impacts may occur for relatively conservative quantities and types of chemicals that may be present during MDA B restoration activities. The aforementioned information does not support the estimate of an accident frequency at MDA B.

Table I-106 shows the accident risks posed from these two chemicals during MDA B waste retrieval. As noted, the frequency of an accident involving releases of these chemicals is unknown because the probability of their presence in the MDA is unknown. The direction traveled by the chemical plume will determine what segment of the worker and offsite populations would be at risk of exposure, and this direction will depend upon meteorological conditions at the time of the accident. The ERPG-3 concentration limit is defined in terms of 1-hour exposure and corresponds to the maximum airborne concentration below which nearly all individuals could be exposed for up to 1 hour without experiencing or developing life-threatening health effects (DOE 2004a). The exposure duration to releases from an explosion event would be for a much shorter period of time and, therefore, is expected to result in smaller health effects than that indicated by the ERPG value.

Table I-106 Material Disposal Area B Waste Retrieval Chemical Accident Consequences

| Chemical | Frequency (per year) | Quantity Released | ERPG-2 ^a | | ERPG-3 ^b | |
|------------------|----------------------|--|-------------------------|---|-----------------------|---|
| | | | Value | Impact | Value | Impact |
| Sulfur dioxide | unknown | 1 pound (454 grams) | 3 ppm | Risk of workers or public within 90 yards (83 meters) of facility receiving exposures in excess of limit. Public access is at 49 yards (45 meters) and beyond this limit. | 15 ppm | Risk of workers within 37 yards (34 meters) of facility receiving exposures in excess of limit. Public access is at 49 yards (45 meters). |
| Beryllium powder | unknown | 0.0013 pounds (0.6 grams) ^c | 0.025 mg/m ³ | Risk of workers within 25 yards (23 meters) of facility receiving exposures in excess of limit. Public access is at 49 yards (45 meters). | 0.1 mg/m ³ | Risk of workers within 10 yards (9 meters) of facility receiving exposures in excess of limit. Public access is at 49 yards (45 meters). |

ERPG = Emergency Response Planning Guideline, ppm = parts per million, mg/m³ = milligrams per cubic meter.

^a ERPG-2 is the maximum airborne concentration below which nearly all individuals could be exposed for up to 1 hour without experiencing or developing irreversible or other serious health effects or symptoms that could impair their abilities to take protective action (DOE 2004a).

^b ERPG-3 is the maximum airborne concentration below which nearly all individuals could be exposed for up to 1 hour without experiencing or developing life-threatening health effects (DOE 2004a).

^c Based on a respirable release fraction of 6×10^{-5} of the total powder at risk and under thermal stress (DOE 1994), and on consideration of respiration release fractions assumed in other environmental statements (DOE 1998a, 1999f).

I.5.12.2 Risks to Workers

Workers would carry out tasks under the No Action and Capping Options that would be little different than those that have taken place for years at LANL. Continued work under LANL's

environmental restoration project would subject workers to risks such as exposure to radioactive and hazardous constituents and standard industrial accidents. Workers receive training to recognize and avoid hazards and would wear personal protective equipment as appropriate. Capping the MDAs could result in slightly increased levels of risks because of extensive use of heavy construction machinery.

The most significant risks to workers would come from complete excavation and removal of the MDAs. Accidents that could result in severe worker injuries could include vehicle accidents, explosions, equipment failures, lightning strikes, electrocution, and operator errors. Removal procedures would be developed for the MDAs based on the experience and technology developed at LANL, Idaho National Laboratory, Hanford, and other DOE sites. Hazards associated with removal of waste and materials from the MDAs could be avoided or mitigated using techniques such as personal protective equipment, water sprays to separate high explosive from a waste matrix, excavation under an inert atmosphere, remotely controlled or shielded excavators, remotely controlled or shielded manipulators for waste sorting, designated safe areas and explosion shields, and other techniques.

Section I.5.12.1 summarizes the radiological consequences and risks to members of the public and, for convenience, to noninvolved workers from two bounding radiological accidents involving removal of wastes from MDAs G and B. Section I.5.12.1 also addresses possible public and worker consequences from two hypothetical accidents at MDA B involving release of chemicals.

Risks to workers from industrial accidents were determined using the procedures outlined in Section I.3.6.4. Industrial accident risks are summarized in **Table I-107** for each of the three options assuming statistical information pertaining to DOE construction workers and the general construction industry. **Table I-108** presents similar risks only for operation of the TA-61 borrow pit. Risks are presented as summed for FY 2007 through FY 2016 and for FY 2007 through FY 2011. DOE statistics indicate a favorable safety record compared to the construction industry as a whole.

The activities resulting in the largest industrial accident risks are those associated with removal of the MDAs, particularly MDA G. Risks for removal of MDA G are listed in **Table I-109**, along with risks for removal of all MDAs (A, B, T, and U) in TA-21.

I.5.13 Cumulative Effects

Several resource areas would not be appreciably affected by any of the options in this project-specific analysis and, therefore, would not contribute significantly to cumulative effects because they would not have major long-term or irreversible effects. These resource areas include: cultural, visual, and biological resources; air quality; noise; human health; transportation; environmental justice; and socioeconomics. The options could frequently have a negative effect on each of the resource areas, but the effect would be temporary. Resource areas receiving additional consideration are land use, geology, water quality, waste management, and infrastructure.

Land Use. All options would have a net positive effect on land use. Continuing the environmental restoration project under the No Action Option would remove contamination from land and property throughout LANL or fix it in place. This action provides greater freedoms in determining future uses for the land and property. The Capping and Removal Options would have additional positive effects.

Table I-107 Industrial Accident Risks for Remediation Options

| Option | Construction Industry | | | DOE Construction | | |
|--|-----------------------|---------------|------------|---------------------|---------------|------------|
| | Recordable Injuries | Lost Workdays | Fatalities | Recordable Injuries | Lost Workdays | Fatalities |
| Fiscal Year 2007 through Fiscal Year 2016^a | | | | | | |
| No Action | 1.9 | 20 | 0.0045 | 0.49 | 1.6 | – |
| Capping ^a | | | | | | |
| Thin cap | 51 | 550 | 0.12 | 14 | 45 | – |
| Thick cap | 83 | 900 | 0.20 | 22 | 73 | – |
| Removal ^b | 1,300 | 14,000 | 3.2 | 350 | 1,200 | – |
| Fiscal Year 2007 through Fiscal Year 2011^a | | | | | | |
| No Action | 1.8 | 19 | 0.0043 | 0.47 | 1.6 | – |
| Capping ^a | | | | | | |
| Thin cap | 25 | 270 | 0.060 | 6.5 | 22 | – |
| Thick cap | 40 | 430 | 0.097 | 11 | 35 | – |
| Removal ^b | 560 | 6,000 | 1.4 | 150 | 500 | – |

^a Includes borrow pit operations.

^b Includes borrow pit operations, capping the remaining disposal units in the existing Area G footprint following MDA G removal, and capping areas in TA-49. Thick caps are assumed.

Note: Numbers have been rounded.

Table I-108 Industrial Accident Risks for Technical Area 61 Borrow Pit Operations

| Option | Construction Industry | | | DOE Construction | | |
|--|-----------------------|---------------|----------------------|---------------------|---------------|------------|
| | Recordable Injuries | Lost Workdays | Fatalities | Recordable Injuries | Lost Workdays | Fatalities |
| Fiscal Year 2007 through Fiscal Year 2016 | | | | | | |
| Capping | | | | | | |
| Thin cap | 12 | 130 | 2.9×10^{-2} | 3.2 | 11 | – |
| Thick cap | 31 | 340 | 7.7×10^{-2} | 8.4 | 28 | – |
| Removal ^a | 31 | 330 | 7.5×10^{-2} | 8.2 | 27 | – |
| Fiscal Year 2007 through Fiscal Year 2011 | | | | | | |
| Capping | | | | | | |
| Thin cap | 5.8 | 63 | 1.4×10^{-2} | 1.5 | 5.1 | – |
| Thick cap | 15 | 160 | 3.6×10^{-2} | 3.9 | 13 | – |
| Removal ^a | 15 | 160 | 3.7×10^{-2} | 4.0 | 13 | – |

^a Includes borrow pit operations, capping the remaining disposal units in the existing Area G footprint following MDA G removal, and capping areas in TA-49. Thick caps are assumed.

Note: Numbers have been rounded.

Table I-109 Industrial Accident Risks for Removal of Material Disposal Area G and Combined Material Disposal Areas A, B, T, and U

| Option | Construction Industry | | | DOE Construction | | |
|--|-----------------------|---------------|------------|---------------------|---------------|------------|
| | Recordable Injuries | Lost Workdays | Fatalities | Recordable Injuries | Lost Workdays | Fatalities |
| Fiscal Year 2007 through Fiscal Year 2016 | | | | | | |
| MDA G | 1,200 | 13,000 | 2.9 | 310 | 1,000 | – |
| MDAs A, B, T, and U | 58 | 630 | 0.14 | 16 | 52 | – |
| Fiscal Year 2007 through Fiscal Year 2011 | | | | | | |
| MDAs G | 450 | 4,900 | 1.1 | 120 | 400 | – |
| MDA A, B, T, and U | 58 | 630 | 0.14 | 16 | 52 | – |

MDA = material disposal area.

^a Includes capping the remaining portion of Area G following MDA removal. A thick cap is assumed.

Note: Numbers have been rounded.

Geology and Soils. All options would have a net positive effect. All options would result in additional contamination being removed from property and soils or stabilized in place. Management of the MDAs under the Capping and Removal Options would be conducted in a manner that addresses mass-wasting concerns such as erosion or cliff retreat.

Water Quality. All options would have a net positive effect. All options would result in additional contamination being removed from property and soils or stabilized in place. These actions would reduce the potential for the contamination to enter surface water pathways and for continued movement of existing contamination in surface water channels. Both the Capping and Removal Options would reduce possible risks to groundwater.

Waste Management Infrastructure. The No Action and Capping Options would not generate wastes in volumes that would significantly tax the existing waste management infrastructure. The Removal Option, however, could impact the waste management infrastructure at LANL and elsewhere. This may require construction of additional and complex waste handling and disposal capacity. Development and use of such capacity would require increased use of utilities such as gas, water, or electricity, increased use of natural resources, and larger personnel requirements. Any structures constructed and used for this purpose would have to be safely decommissioned, which would generate additional quantities of waste to be treated, packaged, shipped, and disposed of. The transuranic waste that would be generated under the Removal Option represents roughly 9 percent of the total transuranic waste volume capacity at WIPP.

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APPENDIX J
IMPACTS ANALYSES OF PROJECTS ASSOCIATED WITH
NEW INFRASTRUCTURE OR LEVELS OF OPERATION

APPENDIX J
IMPACTS ANALYSES OF PROJECTS ASSOCIATED WITH NEW
INFRASTRUCTURE OR LEVELS OF OPERATION

Appendix J presents the project-specific analyses for three proposed projects that would result in either new infrastructure or increased levels of operation at Los Alamos National Laboratory (LANL) within the timeframe under consideration in the *Final Site-Wide Environmental Impact Statement for Continued Operation of Los Alamos National Laboratory, Los Alamos, New Mexico* (SWEIS). These three proposed projects are:

- Security-Driven Transportation Modifications;
- Nicholas C. Metropolis Center for Modeling and Simulation (Metropolis Center) Increase in Levels of Operation; and
- Increase in the Type and Quantity of Sealed Sources Managed at LANL by the Off-Site Source Recovery Project.

These projects are part of the Expanded Operations Alternative, and their implementation could entail changes in the use of resources (such as water and electric power) or new accident types (such as the introduction or movement of new materials at risk [MAR]) not fully addressed in existing National Environmental Policy Act (NEPA) analyses. The proposed timeframes associated with construction and operation of these facilities are depicted in **Figure J-1**.

| Facility or Project Name New Infrastructure or Levels of Operations | Fiscal Year | | | | | |
|---|--------------|------------------|------|-----------|------|---------------|
| | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 & beyond |
| Security-Driven Transportation Modifications | Construction | | | Operation | | |
| Nicholas C. Metropolis Center Increased Levels of Operations | | Gradual Increase | | | | |
| Increase in the Type and Quantity of Sealed Sources Managed at LANL by the Off-Site Source Recovery Project | | Ongoing Activity | | | | |

Figure J-1 Proposed Timeframes for Construction and Operation of Projects to Add New Infrastructure or Increase Levels of Operation

The projects included in this appendix are categorized into two broad groups: (1) those that would add new elements to LANL’s present infrastructure; and (2) those that would increase the present operating levels at existing LANL facilities. A brief introduction to each project is presented below, with detailed analysis of the environmental consequences associated with each project presented in the following sections.

New Infrastructure. The *Security-Driven Transportation Modifications* Project is part of LANL's ongoing physical protection efforts around critical assets that directly support nuclear weapons, homeland security, and other nuclear-related national security missions. Since the September 11, 2001, terrorist attacks, security-related issues have risen in prominence and have been a driving consideration in LANL planning. As part of this ongoing security improvement effort, the National Nuclear Security Administration (NNSA) determined that there is a continuing need for upgrade physical protection in the area of the Pajarito Corridor West. This would involve restricting vehicle access, according to the security level, to LANL's core nuclear science and materials area between Technical Area (TA) 48 and TA-63. Staff and visitors would access this area through an internal shuttle system linked to parking areas in TA-48 and TA-63.

Increased Levels of Operation. The *Metropolis Center* is an existing facility that houses one of the world's largest and most advanced computers. It is part of an integrated tri-lab (LANL, Lawrence Livermore National Laboratory, and Sandia National Laboratories) effort to run supercomputers that allows researchers to integrate past weapons test data, materials studies, and current simulation experiments, thereby serving as an alternative to underground testing. While the computing capacity of the Metropolis Center is currently between 30 and 50 teraflops (30 to 50 trillion floating point operations per second), the long-term goal was to develop a computer system capable of performing up to at least 100 teraflops. With this goal in mind, the infrastructure was originally designed so that this projected computing capacity could be added without expanding the building. Since the 1998 *Environmental Assessment for the Proposed Strategic Computing Complex (SCC EA)* (DOE/EA-1250), NNSA has made the programmatic decision that in order to ensure the safety, reliability, and performance of the nation's nuclear weapons stockpile, the Metropolis Center's operations need to be upgraded to 100 teraflops, with the possibility that a future operating level of approximately 1,000 teraflops (1 petaflops) might be requested.

The *Increase in the Type and Quantity of Sealed Sources Managed at LANL by the Off-Site Source Recovery Project* is an ongoing effort that involves the recovery and storage of excess and unwanted radiological sources licensed by the U.S. Nuclear Regulatory Commission (NRC) to public or private organizations. As requested by the NRC, from 1979 to 1999, the U.S. Department of Energy (DOE) retrieved, on a case-by-case basis, approximately 1,100 sealed sources and sent them to LANL. The increased costs and inefficiencies associated with this case-by-case approach prompted DOE to formulate a management strategy that was addressed in the *Environmental Assessment for the Radioactive Source Recovery Program* (DOE 1995). In 2000, NNSA prepared the *Supplement Analysis, Site-Wide Environmental Impact Statement for Continued Operation of Los Alamos National Laboratory, Modification of Management Methods for Certain Unwanted Radioactive Sealed Sources at Los Alamos National Laboratory*, DOE/EIS-0238-SA-01 (DOE 2000). Sealed sources would be packaged in multifunctional shielded containers (at the origination point or consolidated at a licensed commercial facility under contract to DOE) and shipped directly to LANL for storage as waste items.

In response to the events of September 11, 2001, NRC conducted a risk-based evaluation of potential terrorist threats and concluded that unwanted radiological sealed sources constituted a potential vulnerability. In order to meet this security need, NNSA's recovery mission was expanded, thereby necessitating the management of additional numbers and types of sealed

sources. While NNSA intends to use commercial organizations and their facilities where appropriate, LANL site facilities would be utilized when commercial storage was not appropriate to fulfill the national security mission of the Off-Site Source Recovery Project.

J.1 Security-Driven Transportation Modifications Impacts Assessment

This section provides an assessment of the potential environmental impacts associated with proposed security-driven transportation modifications in the Pajarito Corridor West and nearby areas at LANL. Section J.1.1 provides background information including the purpose and need for the proposed security-driven transportation modifications. Section J.1.2 provides a summary of the Proposed Project and presents the option being considered, plus auxiliary actions to extend roadways across canyons to connect with mesas to the north. Section J.1.3 describes the affected environment in the Pajarito Corridor West and the mesas to the north, and impacts associated with the options and auxiliary actions.

J.1.1 Introduction, Purpose, and Need for Agency Action

Security-related issues have risen in prominence in the United States following the terrorist attacks of September 11, 2001. Similarly, security is figuring prominently in planning at LANL, affecting current and future concepts for controlling traffic on the site. Transportation planning at LANL is being conducted in response to updated NNSA security requirements and guidance.

Background

The current proposal is to implement security-driven transportation modifications that would further enhance security by restricting, according to the security level, privately-owned vehicles along portions of the Pajarito Corridor West between TA-48 and TA-63. Under this planned approach, vehicle traffic in the Pajarito Corridor West could be limited, according to the security level, to only government vehicles and physically inspected service vehicles. Access for staff and visitors to this controlled area would be provided by an internal shuttle system linked to large parking areas at TA-48 and TA-63. In addition to controlling potential vehicle-borne threats, this approach provides an opportunity for LANL to use transit systems to reduce onsite vehicle use, related resource consumption, and impacts on air quality. **Figure J–2** provides an overview of the proposed Pajarito Corridor West security-driven transportation plan.

This transportation plan reflects proposed modifications that would be implemented over the near term – that is, primarily over the next 5 years. Further development of the West Pajarito Corridor is expected, and a comprehensive development concept has been issued covering the next 20 to 30 years for the West Pajarito Corridor Planning Area (LANL 2006a). Further NEPA analyses would be needed for proposals developed from this long-term conceptual plan that are not addressed in this SWEIS.

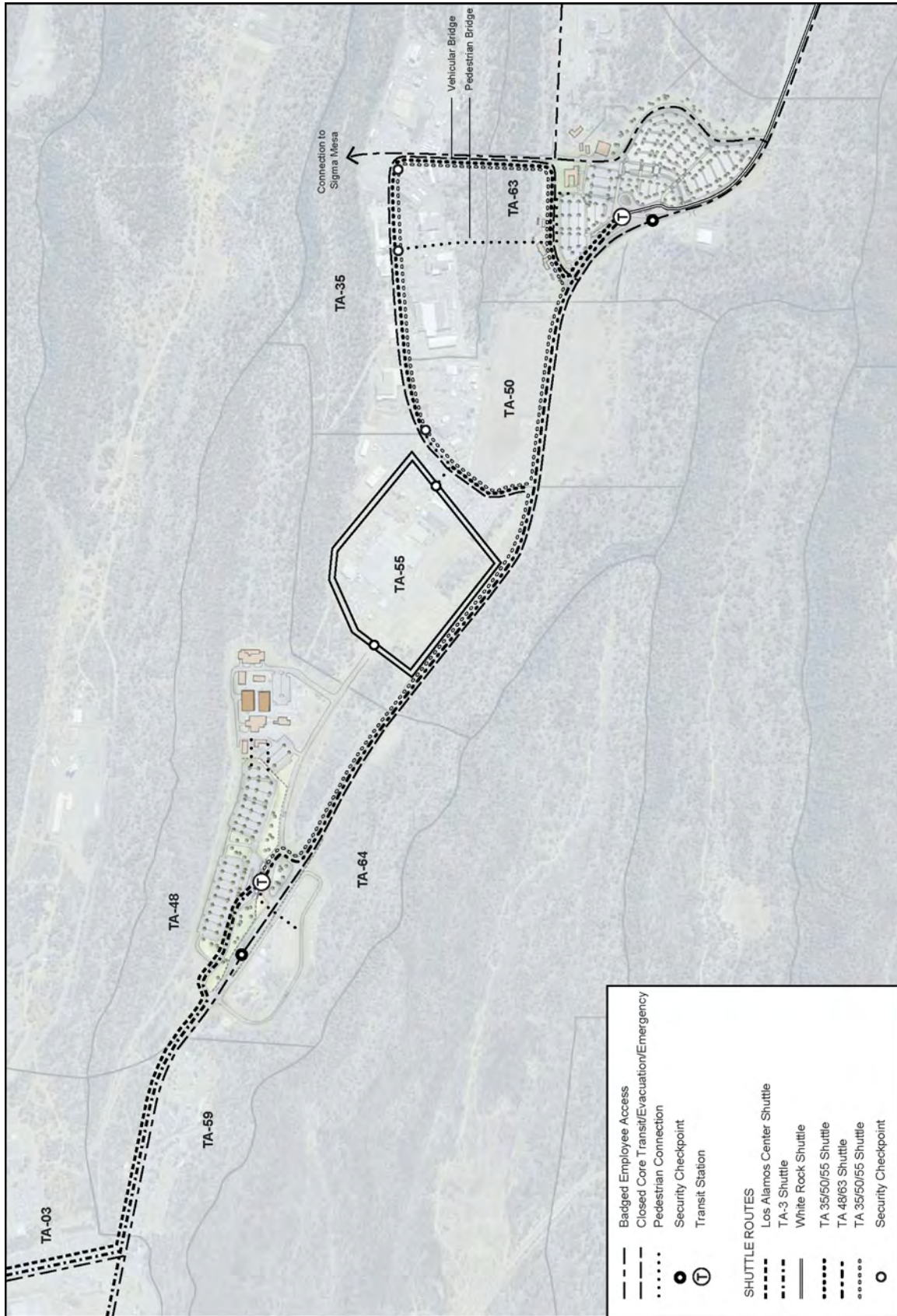


Figure J-2 Proposed Pajarito Corridor West Security-Driven Transportation Plan

Several NEPA documents are related to the Proposed Project. The *Environmental Assessment for Proposed Access Control and Traffic Improvements at Los Alamos National Laboratory, Los Alamos, New Mexico*, DOE/EA-1429 (DOE 2002) evaluated the impacts of constructing and implementing traffic control measures that would, according to the security level, restrict vehicle traffic in the vicinity of the core area of LANL, including the main administrative and technical area at TA-3.

The *Environmental Impact Statement for the Chemistry and Metallurgy Research Building Replacement Project at Los Alamos National Laboratory, Los Alamos, New Mexico*, DOE/EIS-0350 (DOE 2003), analyzed alternatives for upgrading or replacing the Chemistry and Metallurgy Research Building. The Record of Decision (ROD) issued in the *Federal Register* (FR) on February 12, 2004, (69 FR 6967) selected the Preferred Alternative, which is the construction of a new Chemical and Metallurgy Research Replacement facility at TA-55. Implementation of the ROD would result in the construction of a new nuclear Hazard Category 2 facility along the Pajarito Corridor West.

The Plutonium Facility Complex Refurbishment Impacts Assessment (see Appendix G of this SWEIS) evaluates the environmental consequences of a multi-year project to modernize and upgrade facilities and infrastructure at the TA-55 complex. The project would be implemented through a series of subprojects. The subprojects are all infrastructure- or facility-related as opposed to adding programmatic capabilities. They range from relatively simple emergency lighting replacement to more complex fire and criticality alarm systems upgrades and exhaust stack replacement.

The TA-Radiography Facility Impacts Assessment (see Appendix G of this SWEIS) evaluates the impacts of locating a radiography facility in TA-55 to serve pit production and surveillance programs needs. This project would result in a minor increase in the number of personnel in TA-55.

The Radiological Sciences Institute Impacts Assessment (see Appendix G of this SWEIS) evaluates the environmental consequences of consolidating radiochemistry and other related activities into a complex in TA-48. Currently the functions to be consolidated are distributed among a number of facilities in multiple TAs including the Sigma Complex and the radiological Machine Shops in TA-3, the Pajarito Site in TA-18, the Radiochemistry Laboratory in TA-48, and other facilities in TA-35, TA-46, and TA-59. This consolidation would result in demolition of old, and construction of new, facilities in TA-48 and an increase in the number of personnel in TA-48.

Other related activities in the vicinity of the Proposed Project are the Nuclear Materials Safeguards and Security Upgrades Project Phases I and II involving activities that were determined to be categorically excluded from NEPA evaluation. Phase I involves installing the data and communications backbone for the security system to the central and secondary alarm stations. Phase II will upgrade the security system at TA-55.

Purpose and Need

LANL's primary mission is to support national security. To carry out that and other assigned missions, LANL staff operates a number of nuclear and radiological facilities in the TAs along the upper end of Pajarito Road, or the Pajarito Corridor West, including the facilities in TA-35, TA-48, TA-50, and TA-55. Current planning includes moving nuclear and radiological capabilities from other locations at LANL into this area. This includes constructing a new facility in TA-55 to which most of the operations of the Chemistry and Metallurgy Research Building would be moved and a Proposed Project evaluated in this SWEIS to consolidate radiochemistry work in TA-48 (see Appendix G, Section G.3).

In recognition of increased and changing threats, NNSA determined that there is a continuing need to upgrade physical protection around critical assets that house quantities of nuclear and radiological materials and directly support LANL's core missions. Facilities and operations in this area are among the most sensitive to LANL nuclear weapons, homeland security, and other nuclear-related missions. LANL management has determined that an effective means of enhancing security would be to control threats that could be transported by vehicles into the area of the Pajarito Corridor West.

J.1.2 Options Descriptions

The two options identified for the Pajarito Corridor West Security-Driven Transportation Modifications Project are the No Action and the Proposed Project to construct and operate the Security-Driven Transportation Modifications. If the Proposed Project were implemented, two auxiliary actions could be implemented. Auxiliary Action A involves the construction of a two-lane bridge crossing between TA-35 and Sigma Mesa (in TA-60), with a new road proceeding west through TA-60 toward TA-3. Auxiliary Action B involves a two-lane bridge crossing between TA-60 and TA-61, with a new road proceeding northward to East Jemez Road.

J.1.2.1 No Action Option

Under this option, no action would be taken to change the current physical control of personally-owned vehicles entering the TAs along the Pajarito Corridor West. Transportation-related upgrades aimed at addressing the increased and changing needs for physical protection around facilities in TA-35, TA-48, TA-50, and TA-55 would not be undertaken. Vehicle traffic would continue to be screened at the existing access control stations located on Pajarito Road near Diamond Drive and near Route 4. Staff and visitors with DOE-issued security badges would continue to traverse Pajarito Road and be allowed to drive vehicles in the proximity of the facilities in TA-35, TA-48, TA-50, and TA-55.

J.1.2.2 Proposed Project: Construct Security-Driven Transportation Modifications in the Pajarito Corridor West

Under the Proposed Project, a comprehensive planned approach would be implemented to upgrade and enhance security in the Pajarito Corridor West area (LANL 2006d). In the near-term, this would include restricting, according to the security level, private through traffic along Pajarito Road at and between TA-48 and TA-63. Surface parking lots would be constructed at

these two termini. Provision would be made at these two parking lots for incoming commuter buses. Within this secure project area, a shuttle bus system would be deployed; this would necessitate the modification of some existing roads as well as the construction of some new roads. Retaining walls and security barriers would be constructed, as needed, to provide physical separation of the security-controlled portion of the Pajarito Corridor West from the parking areas and other roadways. A pedestrian and bicycle pathway system also would be provided in this secure area. Shelters and related amenities (benches, bicycle racks, lighting, landscaping, etc.) would be provided at various locations within the project area. Finally, both a pedestrian crossing and a vehicular crossing would be constructed between TA-63 and TA-35.

West Pajarito Transit-Based Concept. The West Pajarito transit-based concept would create two large park-and-ride locations, one at TA-48 and the other at TA-63, with a shuttle transit system running between, transporting people to all the facility areas in TA-35, TA-48, TA-50, and TA-55.

During peak transit hours in the morning and afternoon, the shuttles would operate on intervals of 2 to 5 minutes. During nonpeak hours of operation, the shuttle intervals would be 15 to 30 minutes. Proposed routes for the shuttle system are as follows:

- A route originating from the TA-48 parking area circulating to TA-55, TA-50, and TA-35;
- A route originating from the TA-63 parking area circulating to TA-55, TA-50, and TA-35; and
- A loop between TA-48 and TA-63.

The shuttles would meet Americans with Disabilities Act requirements and allow for bicycle transport as well.

At each of the proposed TA-48 and TA-63 parking areas, transfer locations to local and regional buses would be provided to encourage and make practical the use of public transportation as a method of arriving to the site for employees and visitors. Because the proposed TA-48 and TA-63 parking locations are within a 5-to-10 minute walk of the secure zone, wide well-designed pedestrian walkways and connections would be provided as part of the basic infrastructure improvements of this plan. This would allow and encourage walking as an alternate during much of the year when weather permits. An all-weather pedestrian connection would be included connecting the parking area at TA-63 to the west end of TA-35 to further encourage walking as an alternate transportation mode.

Improvements West of TA-55. The Security-Driven Transportation Modifications Project improvements proposed in the areas west of TA-55 are described below. **Figure J-3** shows the conceptual plan for the proposed modifications around TA-48.

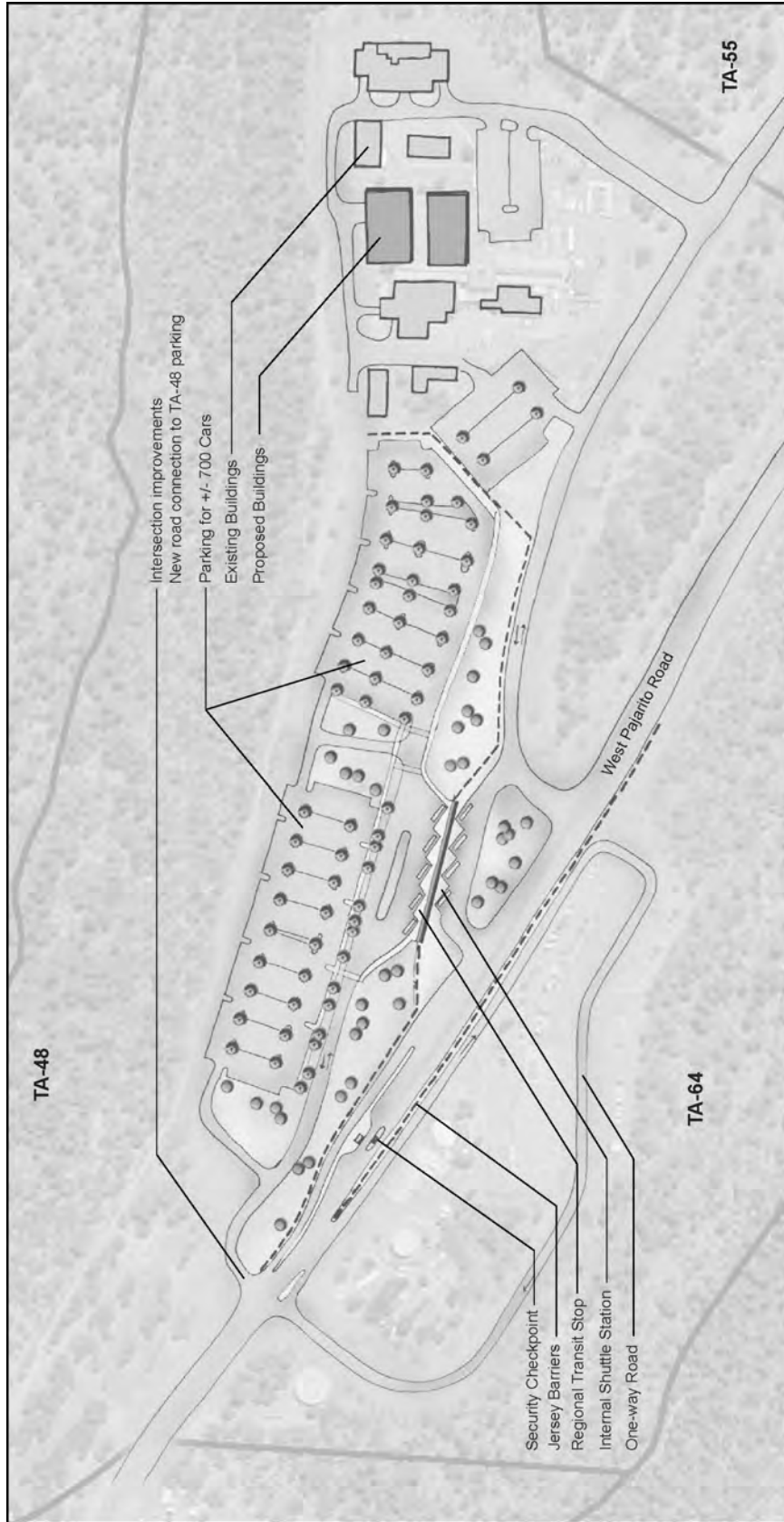


Figure J-3 Proposed Technical Area 48 Security-Driven Transportation Modifications

- A new intersection would be built west of the current guard gate creating the entrance to the TA-48 parking lot and TA-64. The total area to be covered by this new intersection would be approximately one-half acre (0.2 hectares). A standard signalized intersection or a roundabout would be used to control traffic. Vehicle types traveling through this intersection generally would be cars, light- and medium-duty trucks, vans, tank trucks, dump trucks, and sometimes forklifts and cranes. The existing guard gate would remain unchanged.
- A new paved one-way route through TA-64 would be established. The route would go east from the new intersection, running parallel and adjacent to Pajarito Road, then enter TA-64 at its current entrance. The route would circle through the TA-64 parking lot and head west back to the new intersection on a new paved road constructed on an existing dirt road. Much of the land for the new route is currently used as roadway. New sections of this road would be approximately 20 feet (6 meters) wide; retaining walls and side safety barriers would be installed as needed to separate this route from Pajarito Road.
- A new paved two-way road going north from the new intersection would be constructed to provide access to the expanded parking lots in TA-48. This road would be approximately 26 feet (7.9 meters) wide and 400 feet (122 meters) long. Retaining walls and side safety barriers would be built, as needed. The retaining walls could be substantial at the initial turn.
- New surface parking would be constructed at TA-48 to provide parking for approximately 700 cars. Grading and construction of the parking area would disturb approximately 11 acres (4.5 hectares) of land, some of which is currently undisturbed.
- A transit stop would be built at the edge of the TA-48 parking lot where commuters would catch the shuttles to the TAs in the secure area or transfer between buses and shuttles. Amenities would include shade and wind shelters, landscaping, benches, bicycle racks, lighting, phones, and emergency access. Approximately one-half acre (0.2 hectares) of land would be used for the transit stop, shuttle transfer, and associated amenities.
- New short connecting roads would be constructed between the transit stop and the existing road in the TA-48 area.
- An improved walkway would be built to connect the parking lot to the TA-48 complex. This walkway would be at least 10 feet (3 meters) wide and would incorporate rest sites along its length. The 10-foot width would accommodate bicycle use.

Improvements East of TA-55. The Security-Driven Transportation Modifications Project improvements proposed in the areas east of TA-55 are described below. **Figure J-4** shows the conceptual plan for the proposed transportation modifications around TA-35 and TA-63.

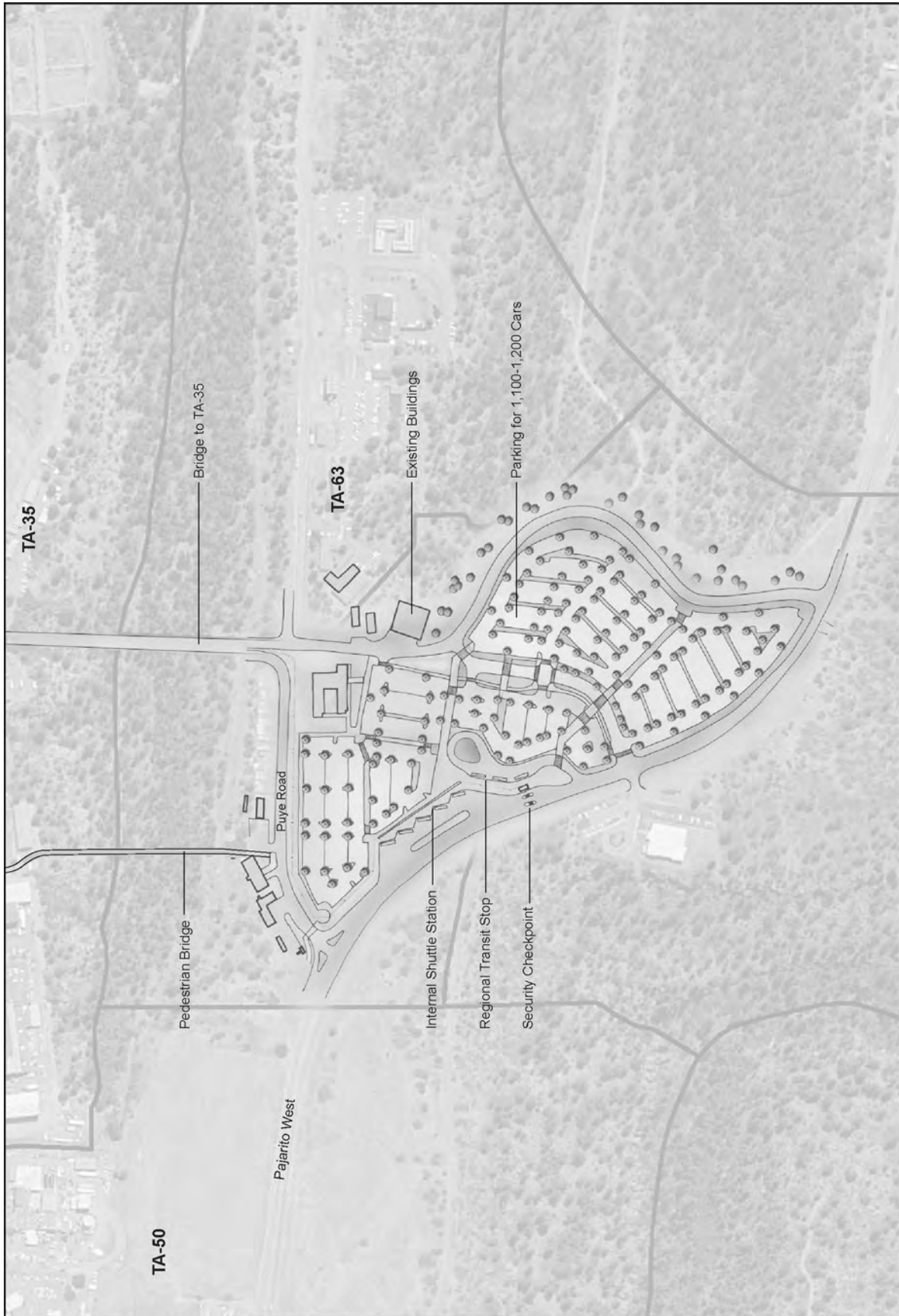


Figure J-4 Proposed Technical Area 35 and Technical Area 63 Security-Driven Transportation Modifications

- A new intersection east of TA-63 would be constructed to provide access to the proposed parking lot and other areas outside the secure area. The new intersection would cover approximately one-half acre (0.2 hectares), a portion of which is undisturbed land. Vehicle types traveling through this intersection generally would be cars, light- and medium-duty trucks, vans, tank trucks, dump trucks, and sometimes forklifts and cranes.
- A new paved two-lane road heading north from the new intersection on Pajarito Road would be constructed. The road would skirt the east edge of TA-63 going northward, and would be 26 feet (7.9 meters) wide and 1,250 feet (380 meters) long.
- A new vehicle crossing would be constructed between TA-63 and TA-35 over a branch of Mortandad Canyon (known locally as Ten Site Canyon). This crossing would align with the new road leading north from TA-63. The new vehicle crossing would be four lanes wide (48 feet [7.3 meters]), approximately 600 to 800 feet (180 to 240 meters) long, and would be about 100 feet (30 meters) above the canyon bottom. The bridge would have dividers down the center; the two west lanes would be for secured traffic traveling among TA-35, TA-48, TA-50 and TA-55; and two east lanes would be for limited secured traffic which would include personally-owned vehicles. **Figure J–5** shows the upper end of Ten Site Canyon that would be spanned by the vehicle bridge and a neighboring pedestrian bridge (described below). A variety of design alternatives would be investigated, including a land bridge and a span bridge.



Figure J–5 Photograph of Canyon to be Bridged between Technical Area 35 and Technical Area 63

- A redesigned road would be built from the end of the vehicle crossing to the north edge of TA-35. The total length of this redesigned road would be approximately 800 feet (240 meters). Routing of this road would likely require the removal of transportables, transportainers, and permanent structures.
- New surface parking additions, or modification of existing parking, would be constructed to accommodate approximately 1,100 to 1,200 cars at TA-63. The parking would be built in two phases, with approximately 450 parking spaces built in the first phase (LANL 2006d). A 126-foot (38-meter) by 78-foot (24-meter) retention pond would be built immediately south of the parking lot to serve as a catchment for parking lot runoff. Grading and construction would result in ground disturbance of about 19 acres (7.7 hectares). The northern portion of the existing site contains 200 existing parking spaces and two office trailers, while the southern portion is not developed. Two overhead power lines which traverse the site would not be relocated. The existing main water pipe that passes through the site would not be affected by the proposal (DMJM H&H 2005).
- A new transit stop similar to the one described above for TA-48 would be constructed.
- A new access control station would be built on Pajarito Road east of the new intersection for TA-63.
- Puye Road would be rerouted. From the Pajarito Road side, Puye Road would be routed to run parallel to, but not intersect, the new road around TA-63, as the two cross the new bridge.
- A permanent barrier system separating Puye Road from the new road along the east side of TA-63 and the TA-63 parking areas would be installed.
- A new pedestrian bridge connecting the TA-63 parking lot to the west portion of TA-35 would be constructed. This new pedestrian crossing would consist of an 8-foot-(2.4-meter-) wide lane, that would be approximately 200 feet (61 meters) long, and could be as much as 100 feet (30 meters) above the canyon bottom. A variety of design alternatives would need to be investigated, including a land bridge and a span bridge.
- New walkways would be constructed to connect the TA-63 parking lot to TA-55 and the new pedestrian bridge. These improved pedestrian walkways would be a minimum of 10-feet (3-meters) wide and would incorporate rest locations and provide for bicycle use.
- The existing TA-55 footprint would be expanded into the middle of the adjacent section of Pecos Drive, with a corresponding relocation of the TA-50 fence eastward to accommodate a new section of bicycle and walking paths.
- New shuttle stops would be built at TA-35, TA-48, TA-50, and TA-55. The size of these stops would be scaled to the expected populations at each area, and some TAs could require multiple stops. The largest shuttle stop would be at TA-55 and would be as large as, or larger, than the current onsite shuttle shelter. Each shuttle stop would have shelters, benches, bicycle racks, lighting, landscaping, and other amenities.

- Various walkway improvements would be made as needed within TA-35, TA-48, TA-50, and TA-55 to create safe walking systems from the transit stops to the individual facilities.

Auxiliary Actions. Auxiliary Action A would involve continuing from TA-35 across Mortandad Canyon to a roadway that would traverse the spine of TA-60 westward to TA-3. A two-lane bridge would be constructed across Mortandad Canyon from TA-35 to TA-60 (see **Figure J-6**). The bridge would be 600 to 800 feet (180 to 240 meters) long; each lane would be 12 feet (3.6 meters) wide. At this early stage in the planning for this project, the specific location of the crossing has not been determined, so for purposes of analysis, a 1,000-foot- (300-meter-) wide zone across Mortandad Canyon in which the bridge would be built has been identified (see Figure J-6). **Figure J-7** is a view from TA-35 across Mortandad Canyon to Sigma Mesa in the approximate location that the canyon would be crossed. The bridge would be 24 feet (7.3 meters) wide and approximately 100 feet (30 meters) above the canyon bottom. The design of the bridge is yet to be determined. Regardless of the design, construction would be necessary along the mesa edges and possibly in canyons. A new paved two-lane road (about 3,750 feet [1,140 meters] long) would be constructed through TA-60 to connect the road crossing the bridge to a road extended east from TA-3. This new paved road would be constructed along the general alignment of an existing unpaved road. It would meet with an existing paved road located in the western portion of TA-60.

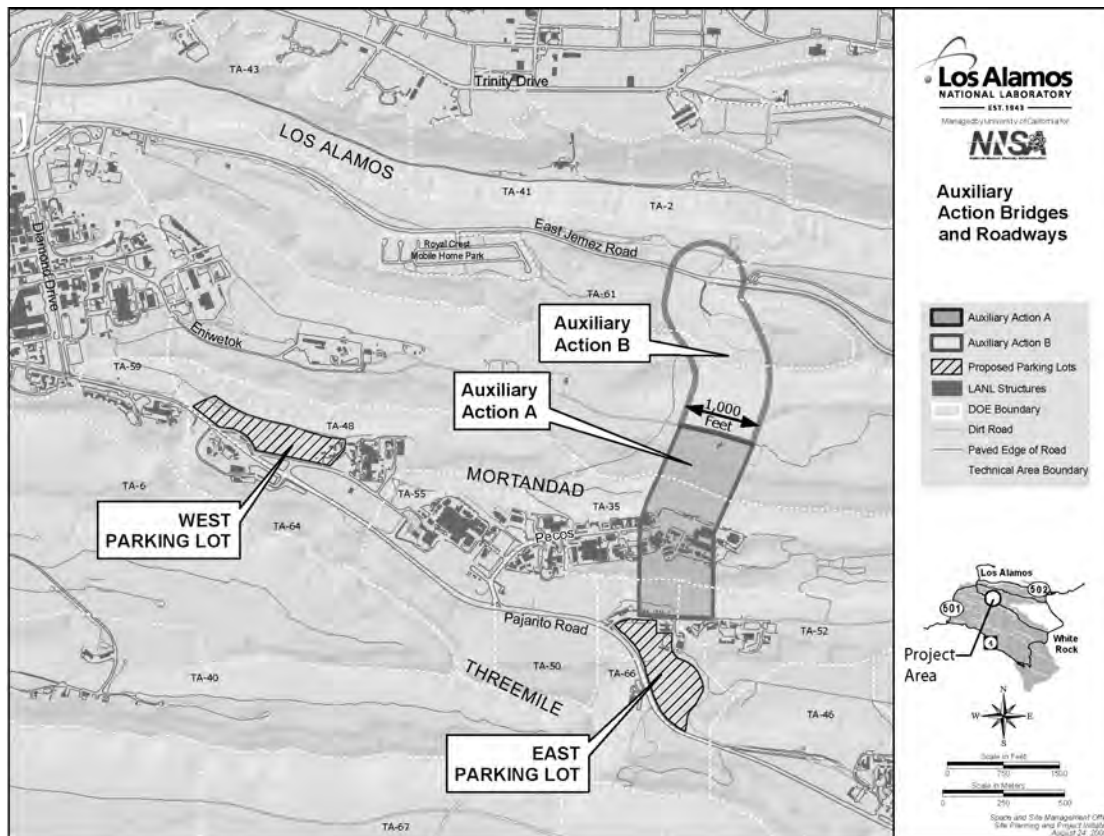


Figure J-6 General Locations of the Auxiliary Action Bridges and Roadways to Technical Area 60 and Technical Area 61



Figure J-7 Photograph Looking North Across Mortandad Canyon in the Area of the Bridge for Proposed Auxiliary Action A

Auxiliary Action B would involve continuing from TA-60 across Sandia Canyon to TA-61, where a new road would connect with East Jemez Road. Auxiliary Action B would provide the most benefit if it were implemented as an augmentation of Auxiliary Action A. A two-lane bridge would be constructed within a 1,000-foot- (300-meter-) wide zone across Sandia Canyon from TA-60 to TA-61 (see Figure J-6). As stated above for Auxiliary Action A, in this early stage of the project, the specific location of the crossing has not been determined, so for purposes of analysis a 1,000-foot- (300-meter-) wide zone across Sandia Canyon, in which the bridge would be built, has been identified (see Figure J-6). The bridge would be 600 to 800 feet (180 to 240 meters) long; each lane would be 12 feet (3.6 meters) wide, with an elevation of approximately 100 feet (30 meters) above the canyon bottom. The design of the bridge is yet to be determined; regardless of the design, however, construction would be necessary along the mesa edges and possibly in canyons. A new two-lane paved road 24 feet (7.3 meters) wide and approximately 750 to 1,000 feet (230 to 300 meters) long would be constructed northward from this bridge's northern terminus and proceed generally northward to meet East Jemez Road.

J.1.3 Affected Environment and Environmental Consequences

The analysis of environmental consequences relies heavily on the affected environment descriptions in Chapter 4 of this SWEIS. Where information specific to the security-driven transportation modifications is available and adds to the understanding of the affected environment, it is included here.

The proposed security-driven transportation modifications are located in the north-central portion of LANL along Pajarito Road between (and including) TA-48 and TA-63. This area includes the facilities in TA-35, TA-48, TA-50, and TA-55. It is anticipated that resource areas potentially affected by the Proposed Project include land resources, geology and soils, water resources, air quality and noise, ecological resources, cultural resources, infrastructure, and waste management.¹ An initial assessment of the potential impacts of the proposed project determined that there would be no or only negligible impacts to the following resource areas and that no further analysis was necessary.

- *Human Health* – There would be no change in practices or procedures associated with radiation exposure or the chemical environment.
- *Socioeconomics and Infrastructure* – It is not anticipated that socioeconomic impacts would occur as a consequence of the Proposed Project. Only infrastructure impacts are included in the impacts discussion.
- *Environmental Justice* – No disproportionately high and adverse environmental impacts on minority or low-income populations would be anticipated to occur.

J.1.3.1 No Action Option

There would be no change in the existing transportation network and no change to practices or procedures under the No Action Option. Therefore, it is anticipated that there would be no new impacts on land resources, visual resources, geology and soils, water resources, air resources, ecological resources, cultural resources, socioeconomics, infrastructure, transportation, or waste management. However, implementing the No Action Option would neither improve transportation flow within the Pajarito Corridor nor provide the needed security upgrades.

J.1.3.2 Proposed Project: Construct Security-Driven Transportation Modifications in the Pajarito Corridor West

Land Resources

Land Use

The Proposed Project would take place on lands in the Pajarito Corridor West. Auxiliary Action A would involve lands in TA-35 and TA-60, and Auxiliary Action B would involve lands in TA-60 and TA-61. The location of these TAs is shown in Chapter 4, Figure 4–3, of this SWEIS.

Pajarito Corridor West – The Pajarito Corridor West is located between Mortandad Canyon on the north and Twomile and Pajarito Canyons on the south, and is immediately southeast of TA-3. It includes TA-35, TA-48, TA-50, TA-52, TA-55, TA-63, TA-64, and TA-66, and totals 831 acres (336 hectares). Activities carried out within the Corridor include nuclear safeguards and chemical processes research and development, theoretical and computational programs

¹ *Plans and facility designs for the Security-Driven Transportation Modifications are conceptual and may be subject to change. To conservatively bound impacts to resource areas such as land use, geology and soils, infrastructure, or waste management, the analysis in this appendix is based on the assumption that the proposed new parking areas in TA-48 and TA-63 and other improvements would cover about one-third more land than the nominal 30 acres included in the project description.*

related to nuclear reactor performance, research and applications in chemical and metallurgical processes relating to plutonium, and industrial partnership activities. Among the goals for the Pajarito Corridor West are a number related to transportation flow along the mesa and development of a pedestrian campus environment. Existing land use within the Pajarito Corridor West varies by TA, with all TAs including at least some areas designated as Reserve. **Table J-1** identifies the present and planned future land use within each TA that makes up the Corridor, as well as development designations as set forth in the *Comprehensive Site Plan 2001* (LANL 2001). Current land use categories are depicted in Chapter 4, Figure 4-4.

Table J-1 Land Use Designations and Development Areas for Technical Areas that Comprise the Pajarito Corridor West

| <i>Technical Area</i> | <i>Current Land Use</i> | <i>Planned Future Land Use</i> | <i>Comprehensive Site Plan Development Designation(s)</i> |
|-----------------------|---|---|--|
| 35 | Experimental Science, Nuclear Materials Research and Development, Physical/Technical Support, Reserve | Experimental Science, Nuclear Materials Research and Development, Reserve | Secondary Development, Potential Infill |
| 48 | Experimental Science, Reserve | Nuclear Materials Research and Development, Reserve | Primary Development, Potential Infill, Parking |
| 50 | Waste Management, Reserve | Waste Management, Reserve | Secondary Development, Potential Infill, No Development (Hazard) |
| 52 | Experimental Science, Reserve | Experimental Science, Reserve | Secondary Development, Potential Infill |
| 55 | Nuclear Materials Research and Development, Reserve | Nuclear Materials Research and Development, Reserve | Primary Development, Potential Infill, Parking |
| 63 | Physical/Technical Support, Reserve | Waste Management, Reserve | Secondary Development, Potential Infill |
| 64 | Physical/Technical Support, Reserve | Physical/Technical Support, Reserve | Potential Infill |
| 66 | Experimental Science, Reserve | Experimental Science, Reserve | Secondary Development, Potential Infill |

Sources: LANL 2001, 2003.

Technical Area 48 – Except for an existing powerline, the western portion of TA-48, where a surface parking lot for 700 cars is proposed, is vacant. Much of this area has been disturbed as a result of previous activities.

Technical Area 63 – The southern and southeastern areas of TA-63, where a surface parking lot for 1,100 to 1,200 cars is proposed, is vacant. Much of the site has been disturbed as a result of previous activities; the northwestern and central portions of the proposed parking lot have existing surface parking areas, and two powerlines traverse the area.

Technical Area 60 – TA-60, Sigma Mesa, is located immediately east of TA-3 and is 445 acres (180 hectares) in size. The area contains physical support and infrastructure facilities, including the Target Fabrication Facility and Rack Assembly and the Alignment Complex (DOE 1999). Presently, most of the central section of the TA is classified as Physical/Technical Support, with a small area designated as Nuclear Materials Research and Development. Land use is not expected to change in the future (LANL 2003). According to the *Comprehensive Site Plan 2001*,

TA-60 is within the Sigma Mesa Development Area (LANL 2001). While developed portions of the TA are classified as Potential Infill, most of the mesa is designated as Primary and Secondary Development. A small corridor of Potential Infill also exists in the eastern part of the TA and connects with a similarly designated area in TA-35. In general, the Plan indicates that considerable development growth is planned for TA-60 and other portions of the Sigma Mesa Area.

Technical Area 61 – TA-61 is located to the northeast of TA-3 and is 297 acres (120 hectares) in size. TA-61 is used for physical support and contains infrastructure facilities, including the Los Alamos County Landfill, which occupies 48 acres (19.4 hectares), and the onsite borrow pit (LANL 2004c). The generalized land use categories within which TA-61 is located are depicted in Chapter 4, Figure 4–4, of the SWEIS, and include Physical/Technical Support and Reserve. According to the *Comprehensive Site Plan 2001*, TA-61 falls within the Sigma Mesa Development Area, an area which could undergo considerable development growth in the future (LANL 2001).

Under the Proposed Project, a number of actions would be implemented within the Pajarito Corridor West. In terms of land area, the largest projects are two parking lots; one in TA-48 and one in TA-63. These would require the disturbance of approximately 11 acres (4.5 hectares) and 19 acres (7.7 hectares), respectively. Some of the land for the proposed parking area in TA-48 has been disturbed from previous activities, and is crossed by an electrical power line. TA-63 has existing parking areas, two temporary structures, and two power lines. Additional actions that would disturb vacant land include a new two-lane road along the east edge of TA-63, new auto and pedestrian crossings connecting TA-63 and TA-35, and a road through the northern edge of TA-35. Other actions associated with this option would involve relatively small areas of land, most of which are disturbed or vacant.

As noted above, the Pajarito Corridor West is highly developed, although vacant land is present. Land use plans for the Corridor have designated some of these vacant areas for future development, including the areas designated for parking. Specifically, the parking area within TA-48 has been designated for Primary Development and that in TA-63 for Secondary Development. Also, the new two-lane road along the eastern edge of TA-63 would pass through areas designated for Secondary Development and Potential Infill. The roadway connecting TA-63 and TA-35 would pass through a corridor designated as Potential Infill, as would the new road along the northern edge of TA-35. However, the new pedestrian walkway connecting the two TAs would not be within an area designated for development in the *Comprehensive Site Plan 2001* (LANL 2001). Many of the other actions under this option would take place largely within developed portions of the Pajarito Corridor West.

While this option would affect future land use by developing currently undeveloped portions of the Pajarito Corridor West, all construction, except the pedestrian walkway between TA-63 and TA-35, would take place within areas designated either for development or for infill. Thus, this option generally would be compatible with land use plans for the Pajarito Corridor West as set forth in the *Comprehensive Site Plan 2001* (LANL 2001).

Visual Environment

Pajarito Corridor West – The TAs that make up the Pajarito Corridor West, along with TA-3, extend along the upper 2.7 miles (4.3 kilometers) of Pajarito Road. Development has taken place within large parts of these TAs. Thus, this area presents the appearance of a mosaic of industrial buildings and structures interspersed with forests along the mesa. Views of the area from a distance are as described in Chapter 4, Section 4.1.2, of this SWEIS. When viewed from along Pajarito Road, the Pajarito Corridor West has an industrial appearance. Mortandad, Twomile and Pajarito Canyons located to the north and south of the mesa, respectively, are wooded and present a natural appearance when viewed from both a distance and nearby.

Technical Area 48 – Most development within TA-48 has occurred in the eastern portion of the TA. Some wooded areas occur in the northern edge of the TA. The proposed surface parking area would be located in the western portion of TA-48; this area is vacant except for a powerline that traverses the northern portion. The area where the proposed parking lot would be sited is readily visible from Pajarito Road.

Technical Area 63 – Most development within TA-63 has occurred in the northern portion of this TA along both sides of Puye Road. The proposed surface parking area would be located in the southern two-thirds of TA-63; this area is vacant except for two powerlines that traverse the site. The area where the proposed parking lot would be sited is readily visible from Pajarito Road.

Technical Area 60 – Most development within TA-60 has occurred within the western portion of the TA. Although some wooded areas occur on the mesa, much of it has been disturbed by a power line and road that runs its length. Additionally, a portion of the mesa is used for the storage of dirt, concrete, and miscellaneous materials. From higher elevations to the west, the mesa appears to be minimally developed; however, due to the power line and road, its appearance contrasts with the adjacent forested canyons. Because of security limitations, near views of the mesa are limited to LANL personnel. Those portions of the TA that include Mortandad Canyon and Sandia Canyon are forested and present a natural appearance.

Technical Area 61 – Most of the mesa within the western portion of TA-61 has been developed, with the Los Alamos County Landfill being the largest facility. The landfill is adjacent to East Jemez Road. Although developed portions of the landfill are not visible from the road, a large berm of stockpiled soil can be seen. The onsite borrow pit is two miles east of the county landfill. The borrow pit is not visible from East Jemez Road due to its location relative to the road, trees bordering the road, and a small hill on the north side of the pit. Although much of TA-61 presents a forested appearance from higher elevations to the west, the landfill and the borrow pit are visible as areas devoid of vegetation. Dust generated from current activities may at times also be visible to the public. Although East Jemez Road passes through the eastern portion of the TA, this part of the TA includes areas of undeveloped woodland both on the mesa and in Pueblo Canyon. This part of TA-61 presents a more natural appearance to those traveling along the road.

The Pajarito Corridor West is a highly developed area that is readily visible from both near and distant locations. While many actions associated with implementing the Security-Driven

Transportation Modifications Project would have little or no visual impact, the construction of the two parking lots, the new roads across TA-63 and TA-35, and the vehicle and pedestrian bridges over the Ten Site branch of Mortandad Canyon would noticeably add to the built-up appearance of the area.

Construction of the two parking lots would disturb approximately 30 acres (12.1 hectares) of land, some previously disturbed and some open and forested. The section of road crossing the eastern portion of TA-35 would disturb open and forested land. However, much of the rest of the roadway would be built within developed portions of the Pajarito Corridor West and would have minimal visual impact. The removal of open and forested land would add to the overall developed appearance of the Pajarito Corridor West as viewed from both nearby and higher elevations to the west. The construction of both the vehicle and pedestrian bridges across a branch of Mortandad Canyon would also have pronounced visual impacts since they would span a forested canyon that has an otherwise natural appearance. These bridges would be readily visible from the canyon where little development is presently apparent; they would also be visible from more distant areas. Careful planning related to site selection and bridge design could help to mitigate these impacts. Most remaining projects associated with the Security-Driven Transportation Modifications Project would be constructed within currently developed portions of the Corridor and, thus, would have little impact on the visual environment.

Geology and Soils

There would be a potential for seismic risk to the facilities constructed under the Security-Driven Transportation Modifications (including the proposed bridges). This risk would be related to seismicity on the nearest fault, the Rendija Canyon Fault (see Chapter 4, Section 4.2.2, of this SWEIS). The bridges under the Proposed Project would be approximately 0.8 miles (1.3 kilometers) east of the Rendija Canyon Fault. The potential for surface rupture at the bridge locations would be low, due in part to the distance from the fault zone, the absence of near-surface faults observed in TA-55 (located between the fault zone and the proposed bridges), and the low recurrence interval of motion on the fault. To minimize the risk of accident, the proposed facilities would be designed and constructed to current DOE seismic standards and applicable building codes.

Soil resources in the area of the Proposed Project include both those disturbed by previous LANL activities and undisturbed soils. The undisturbed soils maintain the present vegetative cover. The arid soils in this area are largely sandy loam material eroded from upslope basalt and tuff units and from underlying geologic units. The soils are generally poorly developed with relatively little horizon differentiation and organic matter accumulation. These factors, combined with the dry moisture regime of the area result in only a limited number of plant species being able to subsist on the soil medium, which in turn supports a very limited number of wildlife species.

Radionuclides are present at near or above background levels in sediments onsite and offsite; however, the overall pattern of radioactivity in sediments has not greatly changed since the *Site-Wide Environmental Impact Statement for Continued Operation of the Los Alamos National Laboratory, Los Alamos, New Mexico (1999 SWEIS)* (LANL 2004b). Although it is not expected that the Proposed Project would result in the release of contaminants, the potential exists for

some contaminated sediments to be disturbed. Prior to ground disturbance, potentially contaminated areas would be surveyed to determine the extent and nature of any contamination and, as necessary, contaminated areas would be remediated.

Construction of the Security-Driven Transportation Modifications would conservatively disturb approximately 240,000 cubic yards (183,000 cubic meters) of soil and rock. Aside from earth moving, deep trenching and excavation, work would generally be limited to that necessary to realign or install new piping, utility lines, and other conveyances that could be affected by this project. Most of the work would be done in areas where these resources already have been disturbed by existing or past activities including the proposed surface parking lots at TA-48 and TA-63. Minor exceptions would be areas along the southern and southeastern edges of the proposed TA-63 parking lot and along the northern edge of the proposed TA-48 parking lot. The undisturbed (native) soil resources would be irretrievably lost as a result of the construction. To mitigate this loss, valuable surface soil in this area may be scraped off of the building sites and stockpiled prior to beginning construction activities. The saved soil stockpiles (and any excavated rock) could then be used at other locations at LANL for site restoration following remediation. If soil or rock stockpiles are to be stored for longer than a few weeks, the stockpiles may be seeded or managed as appropriate to prevent erosion and loss of the resource. In addition, care would be taken to employ all necessary erosion control best management practices during and following construction to limit impact on soil resources adjacent to the construction and building sites.

A number of potential release sites are in the project area. Grading and embankment excavation work, as well as establishing construction laydown pads, would directly impact sediments, soils, and tuff on the mesa and possibly near and in Mortandad Canyon. While no provisions for wet or flooded soils would likely be required, the potential exists for some contaminated sediments to be disturbed within the canyon areas. Prior to commencing any ground disturbance, potentially affected contaminated areas would be surveyed to determine the extent and nature of any contamination and required remediation in accordance with LANL procedures. Proposed parking lots, roadways, walkways, shuttle bus structures, and security facilities would be designed, constructed, and operated in compliance with applicable DOE Orders, requirements, and governing standards that have been established to protect public and worker health and the environment.

Geologic resource consumption would be small under this option and would not be expected to deplete local sources or stockpiles of required materials. Conservatively, about 50,000 cubic yards (38,000 cubic meters) of gravel, 25,000 cubic yards (19,000 cubic meters) of asphalt, and 9,000 cubic yards (6,900 cubic meters) of concrete would be needed during construction. Aggregate resources are readily available from onsite borrow areas and are otherwise abundant in Los Alamos County. Concrete and asphalt would be procured from an offsite supplier.

Facility operations would not result in additional impacts on geologic and soil resources at LANL.

Water Resources

Mortandad Canyon receives natural runoff, as well as effluent from several National Pollutant Discharge Elimination System (NPDES) outfalls. The Radioactive Liquid Waste Treatment Facility at TA-50 discharges treated liquids via NPDES Outfall 051 into Mortandad Canyon (EPA 2001). The volume of treated effluent discharged from the TA-50 Radioactive Liquid Waste Treatment Facility has steadily decreased since the 1999 SWEIS, and LANL is considering options for evaporating rather than discharging this effluent (see Appendix G, Section G.4). Annual flows are shown in Chapter 4, Table 4–9, of this SWEIS.

TA-55 is flanked by Mortandad Canyon to the north and Twomile Canyon to the south (USGS 1984). The site is largely comprised of a heavily developed facility complex with surface drainage primarily occurring as sheet flow runoff from the impervious surfaces within the complex. No developed portions of the complex are located within a delineated floodplain. One TA-55 facility discharges cooling tower blowdown via NPDES Outfall 03A181 directly into Mortandad Canyon (EPA 2000, 2001).

TA-48 and TA-63 do not currently have any NPDES outfalls into Mortandad Canyon or its ancillary canyons. TA-48 and TA-63 are both located on mesa tops and are not within the 100-year or 500-year floodplain boundaries. Storm water flow from the buildings and parking lots in these TAs drain into the Mortandad Canyon system, with some runoff from TA-63 possibly entering Cañada del Buey or Pajarito Canyon.

Ephemeral streams flow in both Mortandad and its ancillary canyon north of TA-63, and in Sandia Canyon. Potential contamination of those streams is minimized by the LANL NPDES Industrial Storm Water Permit Program and the LANL NPDES Storm Water Construction Program.

While nearly every major watershed shows some level of impact from LANL operations, the overall quality of most surface water is described as good. Most samples are within normal ranges or at concentrations far below regulatory standards or risk-based advisory levels (LANL 2004c). Releases from the Radioactive Liquid Waste Treatment Facility have introduced some radionuclide and chemical contamination into surface waters of Mortandad Canyon. This surface water is not used as a drinking source and flows do not normally extend offsite. Beginning in 1999, LANL made significant upgrades to the Radioactive Liquid Waste Treatment Facility treatment system. As a result, for the 6 years ending in 2005, the Radioactive Liquid Waste Treatment Facility has met all DOE radiological standards, all NPDES requirements, and for all but 2 weeks has voluntarily met New Mexico groundwater standards for fluoride, nitrate, and total dissolved solids. In 2005, polychlorinated biphenyls above water quality standards were detected in storm runoff samples from Mortandad Canyon (LANL 2006e).

Effluent discharges have affected perched alluvial groundwater in Mortandad Canyon. Most notably, radionuclide constituents in effluents discharged to Mortandad Canyon from the Radioactive Liquid Waste Treatment Facility at TA-50 have created a localized area of alluvial groundwater with plutonium-238, plutonium-239, plutonium-240, americium-241, tritium, strontium-90, and gross beta measured above the 4-millirem DOE Derived Concentration Guides for drinking water or U.S. Environmental Protection Agency (EPA) drinking water criteria

(LANL 2004c). Nitrate also contained in the effluent has caused alluvial groundwater concentrations to exceed the New Mexico groundwater standard and EPA Maximum Contaminant Level of 10 milligrams per liter.

Perchlorate was detected in Mortandad Canyon in 2002 through 2005, before the EPA issued any water quality standard for this contaminant. In 2005, perchlorate concentrations in four Mortandad Canyon wells exceeded EPA's Drinking Water Equivalent Level of 24.5 micrograms per liter, which was established in January 2006. In 2005, 1,4-dioxane was detected in two perched intermediate aquifer wells in Mortandad Canyon. There is no Federal or State standard for 1,4-dioxane and LANL and the New Mexico Environment Department are currently working to determine the extent and impact of this contaminant. In 2005, a regional aquifer monitoring well in Mortandad Canyon indicated hexavalent chromium levels four times the EPA Maximum Contaminant Level. This is currently being investigated by LANL and New Mexico Environment Department staff and is likely due to past cooling tower discharges in Sandia Canyon (LANL 2006e).

Minimal impacts to surface water are expected during the construction of the Proposed Project. Adverse impacts from constructing the additional parking lots, intersections, and roads required for the Proposed Project would be minimized by the implementation of best management practices described in construction storm water pollution prevention plans. These plans meet the requirements of the NPDES Construction General Permit. Construction of the pedestrian and vehicular crossing between TA-63 and TA-35 would require a bridge over Ten Site Canyon, an ancillary branch of Mortandad Canyon. This bridge construction would require a general or individual 404 Permit from the U.S. Army Corps of Engineers and a New Mexico Environment Department 401 Water Quality Certification for linear transportation projects, because the effluent flows and ephemeral streams in the Mortandad Canyon system are considered "waters of the United States." Construction impacts to these canyon surface water flows and the canyon-bottom floodplains would be mitigated by the provisions provided in the permit and the construction storm water pollution prevention plan.

Minimal impacts to surface water would occur during the operation of the Proposed Project. The presence of large parking lots at TA-48 and TA-63 and additional paved roads would increase the amount of storm water runoff from those sites. Potential storm water contamination from parking lot runoff would be minimized by proper maintenance practices at the facility, including spill response and cleanup. Spill prevention and response procedures would also reduce any potential contamination that could occur as a result of spills on the bridge across TA-48 and TA-63. The Integrated Storm Water Monitoring Program that monitors runoff on a watershed basis would evaluate the effectiveness of these controls.

No adverse affects on groundwater are expected from the implementation of this project. Water used during construction is included in the utility requirements for the project. Groundwater quality would not be affected unless the surface water quality controls fail and contaminated surface water infiltrates through the soil to the groundwater.

Air Quality and Noise

Construction of parking lots, pedestrian walkways, roads, and bridges associated with this option would result in temporary increases in nonradiological air quality impacts from construction equipment, trucks, and worker vehicles. There would also be particulate emissions from disturbance of soil caused by the wind and equipment.

Operation of these facilities would result in emissions of criteria and toxic air pollutants from vehicles, including employee vehicles and shuttle buses. Since the number of employee vehicles is not expected to change as a result of this option, the change in emissions could be small, except for the addition of emissions from shuttle buses.

Construction or operation of these facilities would not result in an increase in the emissions of radiological air pollutants.

Construction of parking lots, pedestrian walkways, roads, and bridges associated with this alternative would result in some temporary increase in noise levels near the new roads from construction equipment and activities. Some disturbance of wildlife near the area could occur as a result of operation of construction equipment. There would be no change in noise impacts to the public outside of LANL as a result of construction activities, except for a small increase in traffic noise levels from construction employees' vehicles and materials shipment.

Operation of these facilities would result in some change in noise levels along the new roadways and bus routes under both options. Some disturbance of wildlife near the area could occur.

Ecological Resources

This section first addresses the ecological setting (that is, terrestrial resources, wetlands, aquatic resources, and protected and sensitive species) of the Pajarito Corridor West and several TAs within it. This is followed by a discussion of the potential impacts on those resources.

Discussions of protected and sensitive species concentrate on those species for which Areas of Environmental Interest have been established, since they receive protection under the Endangered Species Act of 1973. Ecological resources of LANL as a whole are described in Chapter 4, Section 4.5, of the SWEIS and the vegetation zones are depicted in Figure 4–25.

Pajarito Corridor West – The Pajarito Corridor West includes TA-35, TA-48, TA-50, TA-52, TA-55, TA-63, TA-64, and TA-66 (LANL 2001). The entire Corridor falls within the Ponderosa Pine Forest vegetation zone. Thus, vegetation present within the area is dominated by ponderosa pine (*Pinus ponderosa* P. & C. Lawson), gambel oak (*Quercus gambelii* Nutt.), kinnikinnick (*Archostaphylos uva-ursi* L.), New Mexico locust (*Robinia neomexicana* Gray), pine dropseed (*Blepharoneuron tricholepis* Torr Nash), mountain muhly (*Muhlenbergia montana* Nutt A.S. Hitchc), and little bluestem (*Schizachyrium scoparium* Michx.) (DOE 1999). Much of the mesa-top areas of the Pajarito Corridor West are fenced, highly developed industrial areas that are devoid of natural habitat and the wildlife that it typically supports. However, the canyons are very good wildlife habitats.

Nearly the entire Pajarito Corridor West was burned at a Low/Unburned severity level during the Cerro Grande Fire. However, the northern portion of TA-48 (that is, a portion of Mortandad

Canyon) was burned at a Medium severity level. At a Low/Unburned severity level, seed stocks are largely unaffected. Also, the existing species may recover quickly. At a Medium severity level, seed stocks can be adversely affected and erosion can increase due to the removal of vegetation and ground cover. In such areas, recolonization by different species of plants may occur. Wildlife response to the fire could include direct loss of less mobile species and young and displacement of more mobile species. As areas succeed to a more mature state, there is a corresponding change in the diversity, composition, and numbers of wildlife present (LANL 2000b).

Several wetlands occur within the Pajarito Corridor West, including four in TA-48 and one in TA-55. Three of the four wetlands in TA-48 are located between TA-48 and TA-60 in Mortandad Canyon. These wetlands, which total about 1.1 acres (0.4 hectares), are characterized by coyote willow (*Salix exigua* Nutt.), Baltic rush (*Juncus balticus* Willd.), cattail (*Typha* spp.), and wooly sedge (*Carex lanuginosa* Michx.). The fourth wetland is located between TA-48 and TA-55; cattail is the dominant plant. This wetland is smaller than 0.1 acre (0.04 hectares). The wetland within TA-55 is within a branch of Pajarito Canyon between TA-55 and TA-48; it covers 1.2 acres (0.48 hectares). This wetland is dominated by cattails (ACE 2005).

The Pajarito Corridor West falls within portions of the Sandia-Mortandad Canyon, Pajarito Canyon, and Threemile Canyon Mexican spotted owl (*Strix occidentalis lucida*) Areas of Environmental Interest (LANL 2000a). Specifically, parts of TA-48, TA-35, and TA-52 are within the core zone for the Sandia-Mortandad Canyon Areas of Environmental Interest, while portions of TA-55, TA-50, TA-63, and TA-66 are included in the core zone of the Pajarito Canyon Areas of Environmental Interest. No part of the Corridor is within the core zone of the Threemile Canyon Area of Environmental Interest. Since buffer zones extend beyond the core zone, they encompass additional land within the Pajarito Corridor West. In fact, with the exception of the western portions of TA-48 and TA-64, as well as a very small section of TA-55, nearly the entire Corridor falls within the buffer and core zones of the three Areas of Environmental Interest. No portion of the Pajarito Corridor West is within Areas of Environmental Interest for the bald eagle (*Haliaeetus leucocapalus*) or southwestern willow flycatcher (*Empidonax trailii extimus*).

Technical Area 48 – Vegetation and wildlife present would include the same species as noted above for the Pajarito Corridor West. Much of the area proposed for surface parking has been disturbed because of previous activities, with vegetation principally comprising of grasses; the area along the northern edge contains mature conifers.

Technical Area 63 – Vegetation and wildlife present would include the same species as noted above for the Pajarito Corridor West. Much of the area proposed for surface parking has been disturbed because of previous activities; vegetation in undeveloped portions of this area principally comprises grasses and junipers.

Technical Area 60 – Vegetation and wildlife present would include the same species as noted above for the Pajarito Corridor West. Most of TA-60 was burned at a Low/Unburned severity level; however the south central portion of the site (that is, a portion of Mortandad Canyon) was burned at a Medium severity level. As noted above, at a Low/Unburned severity level, seed

sources should remain viable; whereas, at a Medium level, this may not be the case, with the result that recolonization by different species of plants may occur (LANL 2000b).

The Sandia wetland is located between TA-60 and TA-61. Vegetation present within this wetland includes cattails and a number of species of grass. In 2000, the Sandia wetland encompassed 3.5 acres (1.4 hectares); however, this represented a 48 percent reduction in size from 1996. At present it is slightly less than 3 acres (1.2 hectares) in size (Bennett, Keller, and Robinson 2001; ACE 2005).

TA-60 falls within the Sandia-Mortandad Canyon and Los Alamos Canyon Mexican spotted owl Areas of Environmental Interest (LANL 2000a). Most of the eastern portion of the TA falls within either the core or buffer zone of the Sandia-Mortandad Canyon Areas of Environmental Interest, while only the very northern border of the TA is within the buffer zone of the Los Alamos Canyon Areas of Environmental Interest. No portion of TA-60 falls within Areas of Environmental Interest for the bald eagle or southwestern willow flycatcher.

Technical Area 61 – Vegetation and wildlife present would include the same species as noted above for the Pajarito Corridor West. Two major features of the TA are the Los Alamos County Landfill and the borrow pit where all vegetation has been removed. Without cover, the landfill and borrow pit provide minimal habitat for wildlife. Most of TA-61 was unaffected by the Cerro Grande Fire. However the very eastern portion of the TA was burned at a Low/Unburned severity level. At this level, seed sources should remain viable (LANL 2000b). The Sandia wetland located between TA-61 and TA-60 was discussed above in relation to TA-60.

As is the case for TA-60, TA-61 falls within the Sandia-Mortandad Canyon and Los Alamos Canyon Mexican spotted owl Areas of Environmental Interest (LANL 2000a). The southeastern portion of the TA is within the core zone of the Sandia-Mortandad Canyon Areas of Environmental Interest, while the northern edge is within the core zone of the Los Alamos Canyon Areas of Environmental Interest. The rest of the TA is included within the buffer zones of these Areas of Environmental Interest. No portion of the TA-61 is within Areas of Environmental Interest for the bald eagle or southwestern willow flycatcher.

Impacts of the project would be greatest on currently undeveloped land. Although the Pajarito Corridor West falls within the Ponderosa Pine vegetation zone, the area is highly developed, especially on the mesa. Most actions associated with implementing the Security-Driven Transportation Modifications Project would have little or no impact on ecological resources; however, the construction of the two parking lots, a portion of the new road across TA-63, and the vehicle and pedestrian bridges over the branch of Mortandad Canyon would affect undeveloped forest and open land. Other project elements would largely take place in currently developed portions of the Corridor.

Construction of the two parking lots would disturb a total of approximately 30 acres (12 hectares). The parking lot at TA-48 would total approximately 11 acres (4.5 hectares), of land consisting partly of open field and ponderosa pine forest. The parking lot at TA-63 would total approximately 19 acres (7.7 hectares) of land consisting partly of open field and junipers. Both habitats would be lost due to construction of the parking lots as well as a portion of the road around the eastern edge of TA-63. The pedestrian and vehicle bridges connecting TA-63 with

TA-35 would involve some loss of habitat due to construction of approaches and pier foundations. Clearing and grading for these projects would result in the loss of less mobile animals such as small mammals and reptiles. In general, more mobile species would be able to avoid the area during the construction period; however, depending upon the season, nests and young could be destroyed. Indirect impacts to wildlife could also result from equipment noise. During operation, noise and added human presence could cause some species to avoid nearby areas; however, considering the present level of human presence within the corridor it would be expected that many species have already adapted. Wetlands located within TA-48 would not be affected by the Proposed Project, since none are in the immediate area of the parking lots or bridges. Indirect impacts (such as sedimentation) to the wetland located between TA-48 and TA-60 from construction of the parking lot in TA-48 would be prevented by using best management practices. There are no aquatic resources on the mesa, therefore impacts to these resources would not occur.

As noted above, portions of the Pajarito Corridor West are within the Sandia-Mortandad Canyon, Pajarito Canyon, and Threemile Canyon Areas of Environmental Interest for the Mexican spotted owl. The parking lot and associated activities in TA-48 are not located in threatened or endangered species habitat. However, the parking lot in TA-63, the road across the eastern edge of TA-63, and the pedestrian and vehicle bridges fall within buffer habitat and a portion of the parking lot is within core habitat. A biological assessment prepared by NNSA determined that up to 18.8 acres (7.6 hectares) of buffer and 1 acre (0.4 hectares) of core Mexican spotted owl habitat consisting of disturbed grassland and ponderosa pine woodland would be lost. Additionally, the assessment noted that the project had the potential to disturb the Mexican spotted owl due to excess noise or light. Therefore, the biological assessment concluded that activities associated with the project may affect, and were likely to adversely affect, the Mexican spotted owl. Nevertheless, the biological assessment noted that reasonable and prudent alternatives should be implemented such as ensuring that all lighting complies with the New Mexico Night Sky Protection Act, employing appropriate erosion and runoff controls, avoiding unnecessary disturbance to vegetation, and revegetating all exposed soils as soon as feasible. Additionally, consultation with the U.S. Fish and Wildlife Service (USFWS) would be reinitiated if a land bridge instead of a span bridge were used over Ten Site Canyon (LANL 2006c). After reviewing the biological assessment, the USFWS concluded that the effects to the owl from construction activities associated with the Security-Driven Transportation Modifications Project would be insignificant and discountable, and would not result in adverse effects. This assessment was based on the fact that: 1) the parking lot in TA-48 would not be located in listed species habitat; 2) the parking lot at TA-63 consists of open field, junipers and ponderosa pine woodland.; and 3) reasonable and prudent alternatives would be implemented to reduce or avoid potential impacts (see Chapter 6, Section 6.5.2).

Areas disturbed by the Security-Driven Transportation Modifications Project do not fall within Areas of Environmental Interest for either the bald eagle or southwestern willow flycatcher. However, recognizing that the bald eagle forages over all of LANL and that some habitat degradation is associated with the project, the biological assessment concluded that provided appropriate reasonable and prudent alternatives were implemented to protect adjacent foraging habitat, the project may affect, but is not likely to adversely affect, the bald eagle. In addition to the reasonable and prudent alternatives noted above for the Mexican spotted owl, those for the bald eagle could include not disturbing winter roosting trees, monitoring the presence or absence

of eagles during project activities, and keeping noise and disturbance to a minimum. Because the southwestern willow flycatcher Area of Environmental Interest is more than 2 miles (3.3 kilometers) from the project site, the biological assessment concluded that the proposed project would have no direct, indirect, or cumulative impacts on this species (LANL 2006c). The USFWS has concurred with the biological assessment as it relates to the bald eagle and southeastern willow flycatcher (see Chapter 6, Section 6.5.2).

Cultural Resources

Cultural resource surveys have been conducted within the TAs involved in the Security-Driven Transportation Modifications Project, including those within the Pajarito Corridor West (TA-35, TA-48, TA-50, TA-52, TA-55, TA-63, TA-64, and TA-66), TA-60, and TA-61. Due to the sensitive nature of cultural resource sites, only their general nature and National Register of Historic Places eligibility is discussed below; specific resource locations are not provided.

Pajarito Corridor West – A total of 22 archaeological resource sites have been identified within the Pajarito Corridor West. These sites include rock features, cavates, 1 to 3-room structures, lithic scatters, rock shelters, rock art, rock and wood enclosures, and article and artifact scatters. Of these sites, 1 has been excavated, 11 have been determined to be eligible for listing on the National Register of Historic Places, and 4 are of undetermined eligibility. One National Register of Historic Places-eligible building is located in the Pajarito Corridor West in TA-55.

Technical Area 48 – TA-48 contains 2 cultural resource sites. Neither of these sites is located at or in the vicinity of the proposed parking lot.

Technical Area 63 – TA-63 contains 2 cultural resource sites, one of which is an historic site situated near an area to be disturbed by the proposed parking lot.

Technical Area 55 – TA-55 contains 3 archaeological resource sites. One site is a prehistoric lithic scatter, while the other two sites are historic structures. Only one site is National Register of Historic Places-eligible. There are no buildings or structures located in TA-55 that are eligible for listing on the National Register of Historic Places.

Technical Area 60 – A total of 13 archaeological resource sites have been documented in TA-60. These resources include 1 to 3-room structures, rock features, lithic and ceramic scatters, and historic structures. Eight of these sites are eligible for the National Register of Historic Places, while 6 are of undetermined eligibility. Historic resources include homesteads and sites of an undetermined nature. There are no National Register of Historic Places-eligible buildings or structures located in TA-60.

Technical Area 61 – TA-61 contains 6 archaeological resource sites, 4 of which include a trail and stairs, cavates, and a historic structure. Four of the sites are National Register of Historic Places-eligible, while one is of undetermined status.

In terms of activities that would result in the disturbance of land, the largest projects associated with the Security-Driven Transportation Modifications Project are two parking lots, one in TA-48 and one in TA-63. These would require the disturbance of approximately 11 acres (4.5 hectares) and 19 acres (7.7 hectares), respectively. Additional actions that would disturb

land include a new two-lane road along the east edge of TA-63, new auto and pedestrian crossings connecting TA-63 and TA-35, and a new road through the northern edge of TA-35. Other actions associated with this alternative would involve relatively small areas of land, most of which is disturbed or vacant (see Section J.1.3.2).

Implementation of these construction projects would not impact cultural resources within the Pajarito Corridor West. This is the case since no known cultural sites are located within any of the areas to be disturbed. A historic site is situated near an area to be disturbed within TA-63; however, direct impacts would be unlikely. In order to protect the site from indirect impacts, boundaries would be marked and the site fenced, as appropriate. Fencing would prevent accidental intrusion and disturbance of the site.

As noted in the above Visual Resources narrative, the proposed vehicle and pedestrian bridges would be highly visible from both nearby and distant locations. Thus, the potential exists for them to conflict with views of the affected branch of Mortandad Canyon from sites identified by Native American and Hispanic communities as traditional cultural properties. Although the specific locations have not been identified due to their sensitivity, 54 such locations are present on or near LANL (see Chapter 4, Section 4.7.3, of this SWEIS). Prior to construction of the proposed bridges, it would be necessary to consult with these groups so that potential impacts to traditional cultural properties could be taken into account early in the planning process.

Socioeconomics and Infrastructure

Within the proposed project area, 115-kilovolt and 13.2-kilovolt power lines now cross the proposed TA-63 parking area. In addition, there is a 13.2-kilovolt line along the northern portion of the proposed TA-48 parking area and a north-south 115-kilovolt line just west of the existing guard station.

Utility resource requirements to support proposed Security-Driven Transportation Modifications are expected to have a minor impact on site infrastructure. Approximately 3.4 million gallons (13 million liters) of liquid fuels (diesel and gasoline) would be consumed for site work (mainly by heavy equipment), including construction of new structures. Liquid fuels would be procured from offsite sources and therefore would not be limited resources. In addition, it is anticipated that approximately 16.6 million gallons (63 million liters) of water would be needed for construction, mainly for dust suppression and soil compaction. The existing LANL water supply infrastructure would be capable of handling this demand.

Some existing utilities, including water and telecommunications, might be relocated or rerouted. While this would have no long-term effect, it would involve trenching and placement of new lines and the capping and abandonment of existing lines or removal of the lines. Most of the trenching that would impact traffic would occur along Pajarito Road to serve the access-control and shuttle bus transit stations.

Waste Management

Key facilities within TA-35, TA-48, TA-50, and TA-55 produce large quantities of radioactive or chemical wastes that currently must be transported outside the Pajarito Corridor West for

disposal. Wastes generated by these facilities are either shipped directly offsite for treatment and disposal or are transferred to the waste management facilities at TA-54 for later shipment offsite or disposal onsite (low-level radioactive waste only). A proposed project could result in the establishment of a transuranic waste management facility within the Pajarito Corridor West (see Appendix H, Section H.3, of this SWEIS).

During construction for the Proposed Project, a relatively small amount of construction-related waste would be generated. Approximately 1,300 cubic yards (990 cubic meters) of construction debris would be generated as a consequence of this option.

Once implemented, this option would impose restrictions, according to the security level, on transportation to and from TA-35, TA-48, TA-50, and TA-55. Wastes generated within these TAs are either shipped directly offsite for treatment and disposal or are transferred to the waste management facilities at TA-54. Because the Pajarito Corridor West would still be available for use by government vehicles and physically inspected service vehicles, the proposed transportation modifications would not have a major impact on waste transport trucks. Some minor delays would occur as vehicles are inspected, and some additional administrative controls might be imposed. The impacts associated with management and transportation of chemical and radioactive wastes in these affected TAs would remain the same as under the No Action Option.

Transportation

Traffic counts were taken in 2004 at specific locations throughout LANL. **Table J–2** presents the traffic counts taken along Pajarito Road at TA-48 and TA-63, approximately at the west terminus of the Proposed Project where traffic controls and a new security access station would be located. **Table J–3** presents the traffic counts taken along Pajarito Road immediately east of TA-63, which would be the eastern end of the proposed Security-Driven Transportation Modifications Project.

Table J–2 2004 Traffic Counts Along Pajarito Road at Technical Area 48 and Technical Area 64

| <i>Location</i> | <i>Average Vehicles per Weekday</i> | <i>Average Vehicles per Weekend Day</i> | <i>AM Westbound Peak Vehicles per Hour</i> | <i>Noon Westbound Peak Vehicles per Hour</i> | <i>PM Westbound Peak Vehicles per Hour</i> |
|----------------------------------|-------------------------------------|---|--|--|--|
| Pajarito Road at TA-48 and TA-64 | 9,119 | 942 | 570 | 562 | 440 |

TA = technical area.
Source: KSL 2004.

Table J–3 2004 Traffic Counts Along Pajarito Road Immediately East of Technical Area 63

| <i>Location</i> | <i>Average Vehicles per Weekday</i> | <i>Average Vehicles per Weekend Day</i> | <i>AM Eastbound Peak Vehicles per Hour</i> | <i>PM Eastbound Peak Vehicles per Hour</i> |
|---|-------------------------------------|---|--|--|
| Pajarito Road immediately east of TA-63 | 5,758 | 674 | 859 | 825 |

TA = technical area.
Source: KSL 2004.

Because new roads would be constructed around TA-48 and TA-63, the Proposed Project would have some long-term effects on the existing transportation network at LANL. Some portion of the traffic shown on Tables J-2 and J-3 is associated with staff that works in TAs along Pajarito Road. Other traffic is through traffic, for instance people traveling from White Rock to TA-3 or the Los Alamos townsite. Implementation of the proposed project in a manner that restricts private vehicles from this section of Pajarito Road would result in increased traffic on other local roads – most likely the truck route (NM 501) and NM 502. Additional traffic information would be needed to fully assess the impacts that the Security-Driven Transportation Modification would have on local traffic. Project design and sequencing would be used to minimize traffic and infrastructure impacts during construction of the proposed bypass roads, bridge, and related access controls, including delayed response times for emergency vehicles.

Traffic control plans would be implemented to minimize delays and congestion during construction. Nevertheless, those traveling to and from LANL would experience some inconvenience and delays during construction. In the long term, traffic patterns would change for commuter traffic between White Rock and TA-3.

The location and access to total available parking would change following construction, possibly resulting in somewhat more circuitous trips and longer walks to work places. Parking lot shuttles would operate within the proposed access-controlled area, and service would not be disrupted because new parking lot access roads would be constructed.

After completion of the Security-Driven Transportation Modifications, current levels of employment at LANL would remain relatively unchanged. Since employment requirements in support of LANL operations would not change, commuter traffic volumes would not change. However, temporary (during construction) and permanent (after construction) road and lane restrictions could affect traffic flow and volumes throughout the site and affect the roads entering LANL. In addition, as noted in the Project Description, traffic patterns at LANL would permanently change.

J.1.3.3 Auxiliary Action A: Construct a Bridge from Technical Area 35 to Sigma Mesa and a New Road toward Technical Area 3

Land Resources

The bridge would be constructed within a 1,000-foot- (300-meter-) wide corridor across Mortandad Canyon in the vicinity of TA-35 (see Figure J-6). Additionally, a new two-lane road would be built from the north end of the new bridge westward through TA-60 to connect TA-35 with TA-3. According to the *Comprehensive Site Plan 2001*, the corridor across the canyon is designated Potential Infill. The route of the proposed road, which would involve new construction and upgrading of an existing unpaved road, passes through areas designated for Primary and Secondary Development. The proposed route itself is designated for Road Improvement (LANL 2001). Thus, although actions taken under this auxiliary action represent a change in land use along the proposed route between TA-35 and TA-3, they are within the scope of the *Comprehensive Site Plan 2001*.

The two parts of this auxiliary action (that is, bridge and road construction) would have varying impacts on the visual environment at LANL. The roadway through TA-60 would involve some new right-of-way, but would in large part follow an existing unpaved road. Thus, construction of the road would have minimal visual impact. However, the proposed bridge over Mortandad Canyon would represent a highly visible change in the appearance of the local environment and would be in contrast to the forested setting of the canyon. Although careful planning related to site selection and bridge design would help mitigate visual impacts, the bridge would nevertheless alter the natural appearance of the canyon as viewed from both nearby locations and higher elevations to the west.

Geology and Soils

Under Auxiliary Action A, direct impacts on geology and soils would occur from the construction of the bridge and road along the top of Sigma Mesa. Approximately 21,600 cubic yards (16,500 cubic meters) of earth moving would be required under this auxiliary action. The bridge crossing would involve some disturbance of geology and soil resources for approaches and pier foundations on the mesas and possibly in Mortandad Canyon. In addition, the degree of induration and fracturing of the Bandelier Tuff would need to be investigated at the crossing site to determine the actions needed to provide sufficient foundations for the bridge piers. Placement of a construction laydown pad to facilitate construction of the proposed bridge spans would have the potential to impact contaminated sediments within the canyon. Construction of the paved road along the mesa in TA-60 would also result in disturbance of geology and soil resources. As with the Proposed Project, this auxiliary action has the potential of encountering potential release sites, either on mesa tops or in Mortandad Canyon. Prior to commencing any ground disturbance, potentially affected areas would be surveyed to determine the extent and nature of any contamination and required remediation in accordance with LANL procedures.

Because the proposed two-lane paved road along Sigma Mesa would generally follow the alignment of the existing two-lane unpaved road, it is anticipated that impacts on geology and soils would be negligible, as best management practices for soil erosion and sediment control would be employed. After construction, disturbed areas that have not been paved would be revegetated or otherwise stabilized and would not be subject to long-term soil erosion.

Geologic resource consumption would be very small under this auxiliary action and would not be expected to deplete local sources or stockpiles of required materials. Approximately 3,400 cubic yards (2,600 cubic meters) of gravel, 2,000 cubic yards (1,500 cubic meters) of asphalt, and 2,500 cubic yards (1,900 cubic meters) of concrete would be needed during construction. Aggregate resources are readily available from onsite borrow areas and otherwise abundant in the region. Concrete and asphalt would be provided by an offsite supplier.

Once constructed, use of the bridge and roadway would not have any ongoing impact on geologic and soil resources.

Water Resources

Minimal impacts to surface water would occur under Auxiliary Action A. Bridge construction would require a general or individual 404 Permit from the U.S. Army Corps of Engineers and a

New Mexico Environment Department 401 Water Quality Certification for linear transportation projects, as the effluent flows and ephemeral streams in the Mortandad Canyon system are considered “waters of the United States.” Impacts to these canyon surface water flows and canyon bottom floodplain would be minimized by the provisions provided in the permit application, which would mitigate impacts to the discharge amounts and water quality of those streams. The additional road construction impacts would be minimized by implementation of the best management practices described in construction storm water pollution prevention plans. These plans meet the requirements of the NPDES Construction General Permit.

Impacts during operation and maintenance of the proposed bridge and road corridor would be minimized by proper maintenance of the bridge, including spill response and cleanup. The Integrated Storm Water Monitoring Program that monitors runoff on a watershed basis would evaluate the effectiveness of these controls.

No adverse affects on groundwater are anticipated from the implementation of this project. Water used during construction is included in the utility requirements for the project. Groundwater quality would not be affected unless the surface water quality controls fail and contaminated surface water infiltrates through the soil to the groundwater.

Air Quality and Noise

Construction of the bridge and roadways associated with this auxiliary action would result in temporary nonradiological air quality impacts from construction equipment, trucks, and worker vehicles. There would also be particulate emissions from wind and equipment disturbance of soil.

Operation under this auxiliary action would result in emissions of criteria and toxic air pollutants from vehicles, including employee vehicles and buses. Since the number of through vehicles is not expected to change as a result of this auxiliary action, the change in emissions is expected to be minimal.

Construction of bridge and roadway associated with this auxiliary action would result in some temporary increase in noise levels from construction equipment and activities. Some disturbance of wildlife near the area could occur as a result of operation of construction equipment. There would be no change in noise impacts to the public outside of LANL as a result of construction activities, except for a small increase in traffic noise levels from construction employees’ vehicles and materials shipment.

Operation of these facilities would result in some change in noise levels along the new bridge and roadway. Some disturbance of wildlife near the area could occur.

Ecological Resources

Construction of the road through TA-60 would have minimal impact on habitat along the right-of-way since it would follow an existing unpaved road for much of its distance. However, short-term impacts to wildlife would likely occur due to increased noise and human presence. This could result in animals avoiding the construction area; however, following construction most animals would likely return. Ensuring that all equipment was properly maintained and posting

construction zone limits would help mitigate these impacts. No wetlands or aquatic resources would be directly affected by roadway construction, and best management practices would prevent erosion and subsequent sedimentation of any such resources in the canyon bottom.

The new road proposed under this option would pass through undeveloped portions of core and buffer habitat within the Sandia-Mortandad Mexican spotted owl Area of Environmental Interest. Additionally, the bridge to be built over Mortandad Canyon is within the Mexican spotted owl Area of Environmental Interest. A biological assessment prepared by NNSA determined that this option would disturb up to 25.3 acres (10.2 hectares) of undeveloped core habitat and 0.1 acres (0.4 hectares) of undeveloped buffer habitat. Further, construction of the road and bridge would cause temporary increases in light and noise; these impacts would be permanent once the bridge was operational. Although reasonable and prudent alternatives would be implemented (such as moving the bridges as far west as possible, avoiding the use of land bridges, avoiding new roads in the canyon, permanently closing hiking trails, and muting back-up indicators on all trucks and heavy equipment), the biological assessment concluded that this option may affect, and was likely to adversely affect, the Mexican spotted owl (LANL 2006c). The USFWS determined that it could not adequately analyze the affects of the proposed action because the exact location and design of the bridge had not been determined. Instead the agency requested that NNSA submit a request for consultation when plans relating to this option were finalized (see Chapter 6, Section 6.5.2).

Areas of Environmental Interest for the bald eagle and southwestern willow flycatcher are not located near the proposed project site. However, recognizing that the bald eagle forages over all of LANL and that some habitat degradation would be associated with construction, the biological assessment concluded that with appropriate reasonable and prudent alternatives (see Section J.1.3.2), the project may affect, but would not likely to adversely affect, the bald eagle. Because the closest southwestern willow flycatcher Area of Environmental Interest is more than 2.3 miles (3.7 kilometers) from the nearest construction there would be no affect on this species (LANL 2006c). The USFWS has concurred with the biological assessment as it relates to bald eagle and southeastern willow flycatcher (see Chapter 6, Section 6.5.2).

Piers for the bridge across Mortandad Canyon would be placed to avoid direct impacts on any wetlands present within the canyon. Best management practices would prevent erosion and subsequent sedimentation of any such resources in the canyon bottom.

Cultural Resources

The corridor within which the bridge over Mortandad Canyon would be built does not contain any known cultural resources, thus, it is unlikely that construction of the bridge would have a direct impact on such resources. There are a number of prehistoric sites and one historic site located to the east and west of the proposed bridge corridor. Due to the relative proximity of these resources to the bridge corridor, it may be necessary to conduct further detailed analyses. Additionally, it may be necessary to fence these sites.

As noted in the above Visual Environment narrative, the proposed bridge would be highly visible from both nearby and distant locations. Thus, the potential exists for it to conflict with views of Mortandad Canyon from sites identified by Native American and Hispanic communities as

traditional cultural properties. Although specific locations have not been identified due to their sensitivity, 54 such locations are present on or near LANL (see Chapter 4, Section 4.7.3, of this SWEIS). Prior to construction of the proposed bridge, it would be necessary to consult with these groups so that consideration to this potential impact could be taken into account early in the planning process.

Socioeconomics and Infrastructure

Utility resource requirements to support Auxiliary Action A are expected to have a negligible impact on site infrastructure. Approximately 370,000 gallons (1.4 million liters) of liquid fuels (diesel and gasoline) would be consumed for site work, mainly by heavy equipment, including that for the construction of new structures. In addition, it is anticipated that about 2.1 million gallons (7.9 million liters) of water would be needed for construction. Finally, some existing utilities might be relocated or rerouted.

Waste Management

During construction under Auxiliary Action A, a relatively small amount of construction-related waste would be generated. Approximately 160 cubic yards (120 cubic meters) of waste materials would be generated as a consequence of this auxiliary action.

Once implemented, a change in the transport of waste that would otherwise use an open Pajarito Road would occur. It is anticipated that this potential transportation routing impact would be minor.

Transportation

Under Auxiliary Action A, it is anticipated that there would be some long-term effects on the existing transportation network at LANL, because a new bridge would be constructed between TA-35 and TA-60 and a new road on to TA-3. Effects on traffic and infrastructure would be minor. Project design and sequencing would be used to minimize traffic and infrastructure impacts during construction of the proposed bypass roads, bridge, and related access controls, including delayed response times for emergency vehicles.

Traffic control plans would be implemented to minimize delays and congestion during construction. Nevertheless, those traveling to and from LANL would experience some inconvenience and delays during construction. In the long term, traffic patterns would change for commuter traffic between White Rock and TA-3.

The current driving distance from the intersection of Route 4 and Pajarito Road to the intersection of Diamond Drive and East Jemez Road via Pajarito Road is approximately 7.6 miles (approximately 12.2 kilometers). Under Auxiliary Action A, the distance between these two end points would be approximately 8.3 miles (approximately 13.4 kilometers), a minor difference. The driving distance from the intersection of Pajarito Road and Route 4 to the intersection of East Jemez Road and Diamond Drive via Route 501 is approximately 10 miles (approximately 16 kilometers), while the driving distance from the intersection of Pajarito Road and Route 4 to the intersection of East Jemez Road and Diamond Drive via Route 502 is approximately 13 miles (approximately 21 kilometers). While this could result in an increase in

vehicle miles traveled, it is anticipated that this would not be a major concern because of the introduction and use of shuttle buses for LANL staff.

After completion of this auxiliary action, current levels of employment at LANL would remain relatively unchanged. Since employment requirements in support of LANL operations would not change, commuter traffic volumes would also not change. However, temporary (during construction) and permanent (after construction) road and lane restrictions could affect traffic flow and volumes throughout the site and affect the roads entering LANL. In addition, as noted in the Project Description, traffic patterns at LANL would permanently change.

J.1.3.4 Auxiliary Action B: Construct a Bridge from Sigma Mesa to Technical Area 61 and a Road to Connect with East Jemez Road

Land Resources

Under Auxiliary Action B, a two-lane bridge would be constructed within a 1,000-foot- (300-meter-) wide corridor across Sandia Canyon (see Figure J-6). Although the terminus of the bridge and the new road to East Jemez Road would be within an area designated as Primary Development in the *Comprehensive Site Plan 2001*, there is no provision in the plan for a corridor for the bridge, as is the case for the bridge over Mortandad Canyon (LANL 2001). Thus, construction of the bridge would represent a departure from the current area development plan.

The two elements of this auxiliary action (that is, bridge and road construction) would have varying impacts on the visual environment at LANL. The roadway through TA-61 would involve a new right-of-way. Thus, construction of the road would alter the generally wooded appearance of the area. The bridge over Sandia Canyon would be constructed within a 1,000-foot- (300-meter-) wide corridor. Its presence would represent a highly visible change in the appearance of the local environment and would be in contrast to the forested setting of the canyon. As is the case for the proposed bridge over Mortandad Canyon, careful planning related to site selection and bridge design would help mitigate visual impacts; nevertheless, the bridge would alter the natural appearance of the canyon as viewed from both nearby locations and higher elevations to the west.

Geology and Soils

Under Auxiliary Action B, the bridge connecting TA-60 with TA-61 would involve some disturbance of geology and soil resources for approaches and pier foundations, and the construction of a paved road connecting the bridge's northern terminus with East Jemez Road would also result in some disturbance. In addition, the degree of induration and fracturing of the Banderier Tuff would need to be investigated at any proposed canyon crossings where potential bridge foundations would be located.

Since the area between the northern terminus of the proposed bridge and East Jemez Road has been already disturbed by previous activities, it is anticipated that little or no impacts to geology or soil resources would occur. After construction, disturbed areas that have not been paved would be stabilized and revegetated and would not be subject to long-term soil erosion.

There are numerous potential release sites in the project area. In implementing the proposed auxiliary action, due care would be taken and appropriate procedures would be followed in order to ensure that contaminants are not released or that workers are not exposed to inappropriate contamination levels.

Major disturbance or consumption of geologic resources is not anticipated under Auxiliary Action B. Approximately 6,700 cubic yards (5,200 cubic meters) of earth would be disturbed as a consequence of implementing this auxiliary action; approximately 870 cubic yards (660 cubic meters) of gravel would be needed; approximately 690 cubic yards (530 cubic meters) of asphalt would be required; and 2,500 cubic yards (1,900 cubic meters) of concrete would be needed. Aggregate resources are readily available from onsite borrow areas and otherwise abundant in Los Alamos County. Concrete and asphalt would be supplied by an offsite supplier.

Following the completion of Auxiliary Action B, it is not anticipated that operations would result in additional impacts on geologic and soil resources at LANL.

Water Resources

Minimal impacts to surface water would likely occur during the construction of the Proposed Project under Auxiliary Action B, a road bridge crossing Sandia Canyon north of TA-60. Bridge construction would also require a general or individual 404 Permit from the U.S. Army Corps of Engineers and a New Mexico Environment Department 401 Water Quality Certification, which should specify project provisions that would minimize adverse impacts on the water quality and quantity of the Sandia Canyon ephemeral stream and canyon bottom floodplain. Adverse impacts from constructing the additional roads required for this auxiliary action would be minimized by implementation of the best management practices described in construction storm water pollution prevention plans. These plans meet the requirements of the NPDES Construction General Permit.

Impacts during operation and maintenance of the proposed bridge and road corridor would be minimized by proper maintenance of the bridge, including spill response and cleanup. The Integrated Storm Water Monitoring Program that monitors runoff on a watershed basis would evaluate the effectiveness of these controls.

Groundwater quality would not be affected unless the surface water quality controls fail and contaminated surface water infiltrates through the soil to the groundwater.

Air Quality and Noise

Operations under this auxiliary action would result in emissions of criteria and toxic air pollutants from vehicles, including employee vehicles and buses. Since the number of through vehicles is not expected to change as a result of this auxiliary action, the change in emissions is expected to be minimal.

Construction of the bridge and roadway associated with this auxiliary action would result in some temporary increase in traffic noise levels from construction equipment and activities. Some disturbance of wildlife near the area could occur as a result of the operation of construction equipment. There would be no change in noise impacts to the public outside of LANL as a result

of construction activities, except for a small increase in traffic noise levels from construction employees' vehicles and materials shipment.

Operation of these facilities would result in some change in noise levels near the new bridge and roadway. Some disturbance of wildlife near the area could occur. Under this auxiliary action, some increased traffic noise near the Royal Crest Mobile Home Park could result from increased traffic along East Jemez Road.

Ecological Resources

This auxiliary action involves the construction of a new bridge across Sandia Canyon and a road connecting the bridge with East Jemez Road. Construction of the road would necessitate the clearing and grading of up to 1.3 acres (0.5 hectares) (assuming a 55-foot [16.8-meter] by 1,000-foot [300-meter] construction corridor) of ponderosa pine forest. Additionally, the bridge would result in the loss of ponderosa pine habitat for its approaches and piers. The destruction of ponderosa pine forest would represent a permanent loss of wildlife habitat. Short-term impacts to wildlife from road construction would occur as a result of increased noise and human presence and would likely result in animals avoiding the construction area. However, following construction, most animals would likely return. Ensuring that all equipment was properly maintained and posting construction zone limits would help mitigate these impacts. No wetlands or aquatic resources would be directly affected by roadway construction, and best management practices would prevent erosion and subsequent sedimentation of any such resources in the canyon bottom.

Road and bridge construction would take place within the buffer zone of the Sandia-Mortandad Canyon and Los Alamos Canyon Mexican spotted owl Areas of Environmental Interest. Additionally, they would impact the core zone of the Sandia-Mortandad Canyon Mexican spotted owl Area of Environmental Interest. Construction would directly impact 37.1 acres (15 hectares) of undeveloped core habitat and 28.7 acres (11.6 hectares) of undeveloped buffer habitat. Further, noise and light levels would be permanently increased in undeveloped core habitat. Due to these factors a biological assessment prepared by NNSA determined that even after implementing reasonable and prudent alternatives (see Section J.1.3.3), this option may affect, and would likely adversely affect, the Mexican spotted owl (LANL 2006c). As is the case for Option A, the USFWS could not adequately analyze the effects of the proposed action because the exact location and design of the bridge had not been determined. The agency requested that NNSA submit a request for consultation when plans relating to this option were finalized (see Chapter 6, Section 6.5.2).

Similar to Option A, the biological assessment determined that with appropriate reasonable and prudent alternatives (see Section J.1.3.2), the project may affect, but would not likely to adversely affect, the bald eagle. Further, because the closest southwestern willow flycatcher Area of Environmental Interest is more than 2.3 miles (3.7 kilometers) from the nearest construction there would be no effect on this species (LANL 2006c). The USFWS has concurred with the biological assessment as it relates to bald eagle and southeastern willow flycatcher (see Chapter 6, Section 6.5.2).

Cultural Resources

The proposed bridge would be highly visible from both nearby and distant locations. Thus, the potential exists for it to conflict with views of Sandia Canyon from sites identified by Native American and Hispanic communities as traditional cultural properties. As noted for the bridge over Mortandad Canyon, prior to construction, it would be necessary to consult with Native American and Hispanic groups so that potential impacts to traditional cultural properties could be taken into account early in the planning process.

Socioeconomics and Infrastructure

Infrastructure effects would primarily occur during construction of the proposed auxiliary action. Several existing utilities, including water and telecommunications, might be relocated or rerouted. While this would have no long-term effect, it would involve trenching and placement of new lines and the capping and abandonment of existing lines or removal of the lines.

Infrastructure effects would primarily occur during construction of the proposed auxiliary action. Approximately 217,000 gallons (821,000 liters) of fuel (diesel and gasoline) would be consumed for site work (including that for the construction of structures). In addition, it is anticipated that about 1.3 million gallons (4.9 million liters) of water would be needed for construction. Finally, some existing utilities might be relocated or rerouted.

Waste Management

During construction under Auxiliary Action B, a relatively small amount of construction-related waste would be generated. Approximately 110 cubic yards (84 cubic meters) of waste materials would be generated as a consequence of this action.

Once implemented, there would be a change in the transportation of waste that would otherwise use an open Pajarito Road. It is anticipated that this potential transportation routing impact would be minor.

Transportation

Traffic control plans would be implemented to minimize delays and congestion during construction. Nevertheless, those traveling to and from LANL would experience some inconvenience and delays during construction. In the long term, traffic patterns would change for commuter traffic between White Rock and TA-3, in that an additional option would be provided for traveling between these two points.

The current driving distance from the intersection of Route 4 and Pajarito Road to the intersection of Diamond Drive and East Jemez Road via Pajarito Road is approximately 7.6 miles (approximately 12.2 kilometers). Under Auxiliary Action B, the distance between these two end points would be approximately 8.5 miles (13.7 kilometers). The driving distance from the intersection of Pajarito Road and Route 4 to the intersection of East Jemez Road and Diamond Drive via Route 501 is approximately 10 miles (16 kilometers), while the driving distance from the intersection of Pajarito Road and Route 4 to the intersection of East Jemez Road and Diamond Drive via Route 502 is approximately 13 miles (21 kilometers). While this

could result in an increase in vehicle miles traveled, it is anticipated that this would not be significant because of the introduction and use of shuttle buses for LANL staff.

Temporary (during construction) and permanent (after construction) road and lane restrictions could affect traffic flow and volumes throughout the site and affect the roads entering LANL. In addition, as noted in the project description, traffic patterns at LANL would permanently change.

J.2 Metropolis Center Increase in Levels of Operation Impacts Assessment

This section presents an assessment of potential impacts for expanding the computer operating capabilities within the existing Metropolis Center in TA-3 at LANL. NNSA plans to operate the Metropolis Center at a higher level than was analyzed in the *SCC EA*. Section J.2.1 presents the purpose and need for the expansion project and a description of the Metropolis Center.

Section J.2.2 presents a description of the Proposed Project of expanding the computer operating capacity of the Metropolis Center, and the No Action Option of operating the Metropolis Center using its existing computing platform. Section J.2.3 provides an overview of the unique characteristics of TA-3 and LANL that could be affected by the expansion, as well as an assessment of impacts from the Proposed Project and the No Action Option. Chapter 4 of this SWEIS presents a description of the affected environment at LANL and TA-3. Any unique characteristics of TA-3 and LANL not covered in Chapter 4 that would be affected by the expansion of operations at the Metropolis Center are presented here.

J.2.1 Introduction, Purpose, and Need for Agency Action

The Metropolis Center (formerly called the Strategic Computing Complex, or SCC) is a 303,000-square-foot (28,179-square-meter) structure built at LANL in 2002 to house “Q,” one of the world’s largest and most advanced computers. The Metropolis Center is an integrated part of NNSA’s tri-lab (LANL, Lawrence Livermore National Laboratory, and Sandia National Laboratories) mission to maintain, monitor, and assure the performance of the nation’s nuclear weapons through the Advanced Simulation and Computing Program. LANL’s Advanced Simulation and Computing Program supercomputers, such as the “Q” machine, run three-dimensional codes that simulate the physics of a nuclear detonation. These supercomputers allow researchers to integrate past weapons test data, materials studies, and current experiments in simulations of unprecedented size (LANL 2004a, 2006d).

Background

In 1998, the *SCC EA* was completed for the construction and operation of the facility now referred to as the Metropolis Center. The *SCC EA* considered the potential impacts associated with constructing and operating this facility with an initial computing capacity of 30 to 50 teraflops (DOE 1998a). Based on that analysis, DOE announced in its Finding of No Significant Impact (FONSI) that constructing and operating the proposed facility at up to 50 teraflops would not result in significant environmental impacts as defined by NEPA (DOE 1998b).

As stated in the *SCC EA*, DOE’s long-term goal was to develop a computer system capable of performing 100 teraflops. By developing technologies to interconnect tens of thousands of

advanced commodity processors, DOE planned to initially provide a collective computing power of at least 30 teraflops, with the 50- and 100-teraflops levels being short-term and long-term goals, respectively. As all of the computer hardware and software would be newly created, DOE's long-term goal of greater computational capability would, by necessity, need to be achieved through a series of technologically path-breaking hardware "platforms" at each of the three nuclear weapons laboratories, developed and employed in a phased-evolution approach (DOE 1998a). As such, the Metropolis Center facility infrastructure was designed to be scalable so that as the projected computing requirements of the Metropolis Center increased, mechanical and electrical equipment could be added in increments without expanding the building. The most recent of these planned incremental platforms is the "Roadrunner", which would provide almost four times the computational power as the Q machine but require only half the floor space (LANL 2006d).

At the time the *SCC EA* was issued in 1998, DOE had not yet made the programmatic decision to pursue levels of operation beyond those then associated with 50 teraflops. However, with the Metropolis Center presently operating near that 50-teraflops level, NNSA is now proposing expanding the existing platform to attain the increased operating capabilities necessary to meet the long-term goals for the Metropolis Center.

Purpose and Need

NNSA's Stockpile Stewardship and Management Program provides an integrated technical program for maintaining the continued safety and reliability of the nuclear weapons stockpile. As an alternative to underground testing, and due to the aging of nuclear weapons beyond original expectations, NNSA must maintain a means to verify the transportation, safe storage, and reliability of nuclear weapons. Without underground nuclear weapons testing, computer simulations that can perform highly complex three-dimensional large-scale calculations have become the only means of integrating the complex processes that occur in the life span of a nuclear weapon. In order to best fulfill its prime stewardship mission to ensure the safety, reliability, and performance of the nation's nuclear weapons stockpile, NNSA needs to increase its existing computer system capability. At LANL's Metropolis Center, a capability of at least 100 teraflops is essential for effectively running these high-fidelity, full system weapon simulations. It is estimated that in the future, an operating level of approximately 1,000 teraflops (1 petaflops) might be requested.

J.2.2 Options Descriptions

J.2.2.1 No Action Option: Continue Metropolis Center Operations Using the Existing Computing Platform

Under the No Action Option, the existing computing center would continue to be operated at up to approximately the 50-teraflops level analyzed in the *SCC EA*. Computing capacity would not be expanded beyond that level, and NNSA would not attain the long-term goal of at least 100 teraflops functional capability that was identified in the *SCC EA* (DOE 1998a).

J.2.2.2 Proposed Project: Modify and Operate the Metropolis Center at an Expanded Computing Platform

Under the Proposed Project, NNSA would expand the computing capabilities of the Metropolis Center at TA-3 to support, at a minimum, a 100-teraflops capability, and approximately 1,000 teraflops (1 petaflops) eventually expected. This action would consist of the addition of mechanical and electrical equipment, including chillers, cooling towers, and air-conditioning units. Because the scope of the *SCC EA* analysis already considered the potential impacts of constructing a building to house equipment for upwards of a 50-teraflops computing capability at LANL, these new proposed enhancements would be added without a need to expand the external dimensions of the building or disturb additional land. These modifications would not result in any changes to the present number of employees operating the center or increase operating hazards (LANL 2006d).

J.2.3 Affected Environment and Environmental Consequences

The Metropolis Center is located in TA-3, which is situated in the west-central portion of LANL and is separated from the Los Alamos townsite by Los Alamos Canyon. It is the main entry point to LANL, and most of the administrative and public access activities are located within its approximately 357 acres (144 hectares). TA-3 is heavily developed and contains numerous buildings located on the top of a mesa between the upper reaches of Sandia and Mortandad Canyons.

The *SCC EA* and FONSI identified potential environmental concerns associated with projected water and electrical requirements. Because the proposed expansion of computing capacity at the existing Metropolis Center (up to a 15-megawatt platform) is expected to only affect water and electrical requirements, this analysis focuses on the affected environment and subsequent potential impacts to these infrastructure resources. The proposed expansion in operations would not physically disturb the building site or environs, result in additional emissions or waste, nor result in changes to the Metropolis Center or regional workforce. Therefore, the following resource areas would not be affected by the Proposed Project and are not part of this impact assessment: land resources, geology and soils, air quality and noise, ecological resources, human health, cultural resources, socioeconomics, transportation, waste management, and environmental justice.

J.2.3.1 No Action Option

Under the No Action Option, NNSA would operate the Metropolis Center only up to the 50-teraflops level analyzed in the *SCC EA*. **Table J-4** summarizes the operational requirements associated with the existing and proposed operating platforms compared with those originally forecast in the *SCC EA*, and current available utility infrastructure capacity.

As shown in Table J-4, the *SCC EA* conservatively estimated water usage of 63 million gallons (239 million liters) per year and an electric load demand of 7.1 megawatts for operating a 50 teraflops platform. Due to continued computer design efficiencies, actual requirements to date have been considerably less. Current water usage for operating the Metropolis Center is

about 19 million gallons (72 million liters) per year and an electric load demand is about 5 megawatts (LANL 2006d).

Although the *SCC EA* and associated FONSI indicated that operating the Metropolis Center at up to 50 teraflops would result in no significant environmental impacts, NNSA acknowledged potential environmental concerns associated with facility water and electrical requirements. To address these concerns, the *SCC EA* indicated that: (1) cooling water for the facility would come from the Sanitary Effluent Recycling Facility, which polishes treated effluent from the Sanitary Wastewater Systems Plant; and (2) electric power constraints, common to all parts of Northern New Mexico, would need to be dealt with through mutual LANL and Los Alamos County Power Pool “shedding procedures” to balance the peak demand with load capabilities. Because the Sanitary Effluent Recycling Facility, which has been proposed to supply the Metropolis Center with its cooling water needs, has not been able to effectively meet the Metropolis Center’s water requirements, much of this water has been supplied through groundwater. However, recently planned improvements to the Sanitary Effluent Recycling Facility have lead to a greater expectation that Metropolis Center cooling water needs shall increasingly use the recycled effluent and that reliance on groundwater shall diminish substantially.

Table J-4 Metropolis Center Operating Requirements

| | <i>Platform Analyzed in SCC EA (No Action)</i> ^a | <i>Existing 5-Megawatt Platform</i> ^b | <i>Expanded 15-Megawatt Platform (Proposed Project)</i> ^b | <i>Total System Demand (2005)</i> ^c | <i>System Capacity (2005)</i> ^c |
|---|---|--|--|--|--|
| Water (million gallons per year) | 63.1 | 19 | 51 | 1,393 (359) | 1,806 |
| Electricity <i>Energy</i> (megawatt-hours per year) | 62,196 ^d | 43,800 ^e | 131,400 ^e | 550,870 (421,413) | 1,138,800 ^f |
| <i>Peak Load</i> (megawatts) | 8.5 ^g | 6 ^g | 18 ^g | 87.8 (69.5) | 130 ^f |
| Workers | 300 | 350 | 350 | Not applicable | Not applicable |

^a DOE 1998a.

^b LANL 2006d.

^c Chapter 4, Section 4.8.2, of this SWEIS. Usage values and capacities reflect that of the utility systems that include LANL and other Los Alamos County users. Total usage is provided first, with LANL’s usage in parenthesis.

^d *SCC EA* projected 7.1 megawatt total load demand × estimated 8,760 hours per year.

^e Megawatt load demand × estimated 8,760 hours per year.

^f The system capacity of the Los Alamos Power Pool increased by 20 megawatts (equivalent to 175,200 megawatt-hours per year) in September 2007 with the installation of a new gas turbine generator at the TA-3 Co-Generation Complex.

^g Megawatt load demand × estimated 1.2 peak loading factor.

Note: To convert gallons to liters, multiply by 3.7853.

J.2.3.2 Proposed Project: Modify and Operate the Metropolis Center at an Expanded Computing Platform

Water

The Los Alamos water supply system consists of 14 deep wells, 153 miles (246 kilometers) of main distribution lines, pump stations, and storage tanks. The system supplies potable water to all of Los Alamos County, LANL, and Bandelier National Monument. In September 2001, DOE completed the transfer of ownership of the water production system to Los Alamos County, along

with 70 percent of its water rights (1,264 million gallons [4,785 million liters] per year). DOE has leased the remaining 30 percent of the water rights (542 million gallons [2,050 million liters] per year) to the county for 10 years, with the option to renew the lease for four additional 10-year terms (DOE 2003, LANL 2006b). In fiscal year 2005, LANL used approximately 359 million gallons (1,360 million liters) of water, of which 19 million gallons (72 million liters) were attributable to the Metropolis Center (LANL 2006b, 2006d). Los Alamos system and LANL site water use and capacity are compared to the Proposed Project and alternatives as presented in Table J-4.

Under the Proposed Project, NNSA would expand the computing capabilities of the Metropolis Center at TA-3. As shown in Table J-4, expanding to a 15-megawatt maximum operating platform is expected to potentially increase current water usage to 51 million gallons (193 million liters) per year. This higher usage would include the additional water lost to cooling tower evaporation and blowdown. Until the Sanitary Effluent Recycling Facility becomes more effective in supplying the Metropolis Center, most of this cooling water would be supplied through groundwater. Nonetheless, this water need would not exceed available system capacities.

During the operating timeframe evaluated in this SWEIS, continued enhancements to the Metropolis Center could theoretically be approximately 1,000 teraflops (1 petaflops) (LANL 2006d). Because each new generation of computing capability machinery continues to be designed with increased computational speed and more efficient cooling systems, it is anticipated that the net cooling water requirements for the Metropolis Center would not increase beyond 51 million gallons (193 million liters). Should use of the Sanitary Effluent Recycling Facility increase as planned, Metropolis Center groundwater requirements could eventually be reduced to zero (LANL 2006d).

Electricity

Electrical service to LANL is supplied through a cooperative arrangement with Los Alamos County, known as the Los Alamos Power Pool, established in 1985. Within LANL, the Contractor also operates a gas-fired steam and electrical power generating plant at TA-3 (TA-3 Co-Generation Complex), and maintains various low-voltage transformers at LANL facilities and approximately 34 miles (55 kilometers) of 13.8-kilovolt distribution lines. Onsite electrical generating capability for the Power Pool is limited by the TA-3 Co-Generation Complex, which is capable of producing up to 20 megawatts of electric power that is shared by the Power Pool under contractual arrangement. A new generator producing an additional 20 megawatts of electric power became operational in September 2007. Generally, onsite electricity production is used to fill the difference between peak loads and the electric power import capability (LANL 2004b, 2006a, 2006d).

As shown in Table J-4, electric power availability from the Power Pool is estimated at 1,138,800 megawatt-hours (reflecting the lower thermal rating of 110 megawatts for 8,760 hours per year on the existing transmission system plus 20 megawatts from the TA-3 Co-Generation Complex). In fiscal year 2005, LANL and other Los Alamos County users combined for a Power Pool total electric energy consumption of 550,870 megawatt-hours of electricity. The fiscal

year 2005 peak load usage was about 69.5 megawatts for LANL and about 18.3 megawatts for the rest of the county (LANL 2006a).

Under the Proposed Project, NNSA would expand the computing capabilities of the Metropolis Center at TA-3 to support a 100-teraflops capability. This action would consist of the installation of additional mechanical and electrical equipment, including chillers, cooling towers, and air-conditioning units. As shown in Table J-4, increasing to a 15-megawatt maximum operating platform is expected to potentially increase current peak electricity consumption to 18 megawatts per year. Nonetheless, this would not exceed available system capacities.

During the operating timeframe evaluated in this SWEIS, continued enhancements to the Metropolis Center could theoretically be approximately 1,000 teraflops (1 petaflops) (LANL 2006d). However, even though the computational capabilities of these computer systems are projected to increase substantially, their power and cooling requirements would not. Because each new generation of computing capability machinery continues to be designed with increased computational speed and enhanced efficiency in electrical requirements, it is anticipated that average electrical requirements associated with such expansion would not exceed 15 megawatts. As newer computing components are installed, older, less efficient components would be retired; therefore, the number of teraflops should increase significantly while the amount of required electrical power stabilizes at less than 15 megawatts (LANL 2006d).

J.3 Increase in the Type and Quantity of Sealed Sources Managed at Los Alamos National Laboratory by the Off-Site Source Recovery Project Impacts Assessment

NNSA proposes to modify the Off-Site Source Recovery Project to recover and store sealed sources² having a wider range of isotopes than that analyzed in previous NEPA analyses. The Off-Site Source Recovery Project has the responsibility to identify, recover, and store excess and unwanted sealed sources in cooperation with NRC. In 2004, the mission of the Off-Site Source Recovery Project was expanded. This section analyzes the impacts of receipt and storage of additional sealed sources at LANL. The analysis of environmental consequences relies on the affected environment descriptions in Chapter 4 of the SWEIS. Where information specific to the Off-Site Source Recovery Project is available and adds to the understanding of the affected environment, it is included here. Section J.3.1 provides background information on the Off-Site Source Recovery Project. Section J.3.2 provides a description of the Proposed Project and the No Action Option. Section J.3.3 provides a brief description of the affected environment and presents an impact assessment of the No Action Option and the Proposed Project.

J.3.1 Introduction, Purpose, and Need for Agency Action

From 1979 through 1999, DOE recovered excess and unwanted radioactive sealed sources containing plutonium-239 and beryllium, and other actinides on a case-by-case basis as requested by NRC. Since 1999, the Off-Site Source Recovery Project has successfully managed actinide-

² Sealed radioactive source means a radioactive source manufactured, obtained, or retained for the purpose of utilizing the emitted radiation. The sealed radioactive source consists of a known or estimated quantity of radioactive material contained within a sealed capsule, sealed between layers of nonradioactive material, or firmly fixed to a nonradioactive surface by electroplating or other means intended to prevent leakage or escape of the radioactive material (10 CFR Part 835). Sealed sources are typically small.

bearing sealed sources, and in 2004 accepted some non-actinide sources. In 2004, following the transfer of management of the project to NNSA as part of the U.S. Radiological Threat Reduction Program, the previous mission of the Off-Site Source Recovery Project was expanded (DOE 2004b). The original scope of the Off-Site Source Recovery Project was to accept sealed sources containing actinide isotopes that exceeded Class C concentrations for these isotopes as listed in the NRC regulation, Title 10 *Code of Federal Regulations* (CFR) Part 61. The expanded scope would include acceptance of sealed sources containing these actinide isotopes in all concentrations (particularly transuranic isotopes), sealed sources containing other isotopes (in any concentration) for which Class C concentration limits are established in 10 CFR Part 61 (particularly strontium-90 and cesium-137), and sealed sources containing cobalt-60, iridium-192, radium-226, and californium-252.

In response to this change, the Off-Site Source Recovery Project began to develop a global inventory and to prepare for the management of a wider range of sealed sources. The Off-Site Source Recovery Project would continue to use commercial or other Federal organizations and facilities where appropriate, and LANL facilities would be used when these organizations and facilities were not appropriate to fulfill the national security mission of the Off-Site Source Recovery Project.

Background

Since the passage of the Atomic Energy Act of 1954, qualified public and private organizations have been licensed to possess and use nuclear materials for a wide variety of applications. These radioactive materials are typically placed within multiple stainless steel jackets and welded closed, or constructed in other ways to meet the NRC definition of a sealed source. During this period of radioactive source manufacture and use, future disposal mechanisms were not defined. Unwanted and excess sealed sources present a public health and safety risk when abandoned, lost, or disposed of inappropriately.

Since 1979, DOE has recovered excess and unwanted radioactive sealed sources containing plutonium-239 and beryllium, and other actinides. Additional sealed sources were recovered from the commercial sector on a case-by-case basis as requested by NRC. These actinide-containing sealed sources were recovered by DOE when there were no other options for their disposition such as reuse or disposal. There was no disposal capacity for commercial waste containing radionuclides in concentrations exceeding Class C limits as defined in 10 CFR Part 61.³ This waste is commonly called Greater-Than-Class C waste. Commercial sealed sources considered waste may be determined to be Greater-Than-Class C waste due to the quantity of radioactive material and their small physical size. Similarly, there were sealed sources and wastes in the Federal sector that also lacked disposal capacity because of similar

³ NRC regulations establish a classification system for disposal of commercially-generated low-level radioactive waste. Classification is determined by the concentrations in waste of a small number of specific isotopes. Waste containing the isotopes listed in 10 CFR 61.55 and in concentrations exceeding their Class C limits must be disposed of using technologies having greater confinement capacity or protection than “normal” near-surface disposal (47 FR 57446). This waste is commonly called Greater-Than-Class C waste. In 10 CFR 61.55, Class C limits are established for these isotopes that are commonly found in sealed sources: alpha-emitting transuranic isotopes having half-lives exceeding five years; strontium-90; and cesium-137. Class C limits are also established for these isotopes that are not commonly found in sealed sources: carbon-14, nickel-59, nickel-63, niobium-94, technetium-99, iodine-129, plutonium-241, and curium-242.

DOE restrictions on disposal of actinide (particularly transuranic) isotopes.⁴ Therefore, the general criterion for DOE acceptance of these actinide sources was that, if considered as waste, their actinide concentrations would exceed the 10 CFR Part 61 Class C limits for these radionuclides.⁵

Recognizing the public danger posed by excess and unwanted radioactive sealed sources, the Congress addressed their disposition in the Low-Level Radioactive Waste Policy Amendments Act of 1985 (Public Law 99-240). This Act assigned the Federal government the responsibility for disposal of commercial low-level radioactive waste containing radionuclides in concentrations exceeding Class C limits as defined in 10 CFR Part 61. This Act also assigned the Federal government the responsibility for disposal of any other low-level radioactive waste owned or generated by DOE, by the U.S. Navy resulting from decommissioning naval vessels, or by the Federal government resulting from research, development, testing, or production of any atomic weapon.

In the early 1990s, DOE had encountered increased costs and inefficiencies associated with the mechanics of case-by-case-type response to NRC requests for the recovery and management of sealed sources. At LANL, these sealed sources were opened, their radioactive contents chemically separated, and the radioactive products and wastes stored separately. Facing the potential recovery of several thousands of these sealed sources, a different approach to recovery and management was required. Consequently, in 1995, DOE chose a management strategy that would continue and enhance the process of chemically separating the radioactive components from certain recovered sources. This nuclear material would be stored for future reuse, and the waste generated from the separation process would be disposed of or stored if a disposal facility was not available. This strategy, identified as the Radioactive Sources Recovery Program, and its environmental effects, were evaluated in DOE's *Environmental Assessment for the Radioactive Source Recovery Program* (DOE 1995) issued December 20, 1995. As of 1999, approximately 1,100 neutron-generating and other sealed sources had been recovered from regulated licensees, DOE sites, and other government agencies and sent to LANL.

An expanded Radioactive Sources Recovery Program was subsequently incorporated into the *1999 SWEIS* (DOE 1999) and the attendant environmental effects assessed. The *1999 SWEIS* Expanded Operations Alternative reflects the activities described for the Radioactive Sources Recovery Program (receiving and storing sealed sources; separating certain radioisotopes such as plutonium-238, plutonium-239, and americium-241; and storing and disposing of radioactive material and waste) at higher rates or greater volumes than analyzed previously in the 1995 environmental assessment. The projected sealed source material chemical separation rate identified in the *1999 SWEIS* was 10,000 curies per year for the 10-year period of analysis (or 100,000 curies total for 10 years). These rates and the resultant process wastes were included in

⁴ These wastes are termed transuranic wastes by DOE. The criterion for transuranic waste determination is comparable to the Part 61 Class C limit for transuranic isotopes.

⁵ In this appendix, the term "actinide source" is used for sealed sources containing actinide isotopes in quantities that could exceed Class C concentrations if disposed of as waste. Actinide sources may exceed Class C concentrations even if the quantity of radioactive material is small. For example, assuming a waste density of 2 grams per cubic centimeter, a 55-gallon (0.21-cubic meter) drum of waste could exceed the Class C concentration limit if it contained more than 0.42 curies of transuranic activity. Nonetheless, numerous sealed sources are in authorized circulation that do not contain sufficient quantities of actinide isotopes to exceed Class C concentration limits.

the impacts analysis for the Chemistry and Metallurgy Research Building, the Plutonium Facility Complex, and Area G at TA-54.

In its 2000 *Supplement Analysis to the Site-Wide Environmental Impact Statement for Continued Operation of the Los Alamos National Laboratory, Los Alamos, New Mexico* (DOE/EIS-0238-SA-01), NNSA decided that rather than chemically separating certain radioactive materials from the recovered sources, storing this separated nuclear material, and transferring the resulting process waste material to the Waste Isolation Pilot Plant (WIPP), NNSA would package sealed sources in multi-functional shielded containers (at the origination point or consolidated at a licensed commercial facility under contract to DOE) and ship them directly to LANL for storage (DOE 2000). Except for those containers of defense-related sealed sources that would be eligible for shipment to WIPP as transuranic waste,⁶ this waste would be managed pursuant to the Low-Level Radioactive Waste Policy Amendments Act of 1985 (Public Law 99-240).

In response to the events of September 11, 2001, NRC conducted a risk-based evaluation of potential vulnerabilities to terrorist threats involving NRC-licensed nuclear facilities and materials. The NRC concluded that possession of unwanted radioactive sealed sources with no disposal path presents a potential vulnerability.

In 2004, NNSA proposed to recover six strontium-90 radioisotope thermoelectric generators⁷ from the commercial sector and to place them in storage at TA-54, Area G, pending future disposal when an appropriate disposal site becomes available. The radioisotope thermoelectric generators contained sealed sources that were different from the actinide-bearing sealed sources previously evaluated through the NEPA compliance process for storage at LANL. The proposed action would result in a small amount of low-level radioactive waste being stored at TA-54 for an indeterminate period of time. After preparation of the *Supplement Analysis to the Site-Wide Environmental Impact Statement for Continued Operation of Los Alamos National Laboratory in the State of New Mexico, Recovery and Storage of Strontium-90 (Sr-90) Fueled Radioisotope Thermal Electric Generators at Los Alamos National Laboratory* (DOE/EIS-0238-SA-04), (DOE 2004a), NNSA concluded that this amount of low-level radioactive waste was not projected to exceed the 1999 SWEIS projections for low-level radioactive waste generation and disposal; four of the strontium-90 radioisotope thermoelectric generators were recovered and stored at LANL's Area G in March 2004. Two additional strontium-90 radioisotope thermoelectric generators were subsequently recovered in 2005.

In March 2004, the mission of the Off-Site Source Recovery Project was expanded as part of NNSA's Radiological Threat Reduction Program. The Project was expanded from recovery of

⁶ Transuranic waste is radioactive waste containing more than 100 nanocuries (3700 becquerels) of alpha-emitting transuranic isotopes per gram of waste, with half lives greater than 20 years, except for: (1) high-level radioactive waste; (2) waste that the Secretary of Energy has determined, with the concurrence of the Administrator of the EPA, does not need the degree of isolation required by the 40 CFR Part 191 disposal regulations; of (3) waste that the NRC has approved for disposal on a case-by-case basis in accordance with 10 CFR Part 61 (DOE 435.1).

⁷ A radioisotope thermoelectric generator is a source of self-contained power for various independent types of equipment with a steady voltage ranging typically 7 to 30 volts or less and the power capacity of a few watts up to 80 watts. Radioisotope thermoelectric generators are used in conjunction with various electrotechnical devices that accumulate and transform the electric energy produced by the generators. Common applications for radioisotope thermoelectric generators include uses as power sources for navigation beacons and seamounts, or other low wattage devices employed in remote locations without reliable sources of electrical energy.

sources containing actinide isotopes in quantities that would exceed Class C concentration limits, if determined to be waste, to sources containing these isotopes in all quantities, plus sealed sources containing any quantity of certain other isotopes for which Class C concentration limits are specified. The Off-Site Source Recovery Project was additionally expanded to receive sealed sources containing isotopes of cobalt-60, iridium-192, radium-226, and californium-252 for which Class C concentration limits are not specified in NRC regulations (DOE 2004b). Thus, the question of whether the sealed sources would contain isotopes exceeding Class C concentration limits is not a constraining factor for the recovery of sources; national security is the primary driving factor for determining the need for recovery of sealed sources containing these isotopes.

A number of the sources that have been delivered to LANL have been determined to result from defense activities and are being shipped to WIPP for disposal. It is expected that many of the other sources stored at LANL will also be determined to be eligible for WIPP disposal. The remaining sources will be dispositioned by other means, such as disposal as Greater-Than-Class C waste pursuant to Public Law 99-240. On July 23, 2007, DOE issued a Notice of Intent (NOI) to prepare an *Environmental Impact Statement for the Disposal of Greater-Than-Class-C Low-Level Radioactive Waste* (72 FR 40135). DOE intends that this environmental impact statement (EIS) would support selection of new or existing disposal locations, facilities, and methods for disposal of commercial Greater-Than-Class C waste and DOE waste having similar characteristics. The EIS will include a forecast of sources that would be considered Greater-Than-Class C wastes if disposed of. The forecast will include an estimate of the sources eligible for such disposal and managed by the Off-Site Source Recovery Project, based on the Off-Site Source Recovery Project recovery rate.

Purpose and Need

The NRC has determined that possession of unwanted sealed sources with no disposal path presents a potential vulnerability. Historically, LANL's Off-Site Source Recovery Project and predecessor projects have received actinide sources for recycling or for storage until a disposal method was determined. Six strontium-90 radioisotope thermoelectric generators were received and stored as waste. The Off-Site Source Recovery Project has now been tasked with managing additional numbers and types of sealed sources. The Off-Site Source Recovery Project would use commercial or other Federal organizations and facilities where appropriate, and LANL facilities when management by these organizations and facilities was not appropriate to fulfill its national security mission.

J.3.2 Options Descriptions

J.3.2.1 No Action Option

Under the No Action Option, LANL would continue to receive and store actinide sources at the previous rate. Actinide sources are packaged offsite at the origination point or consolidated at a licensed commercial facility under contract to DOE and shipped to LANL in compliance with U.S. Department of Transportation (DOT) regulations (49 CFR Part 71). Shipping containers are received at the LANL Supply Chain Management receiving warehouse, SM-30. The containers are then transported by truck over LANL roads to TA-54 or TA-55 for storage; because they are

packaged to DOT specifications, road closures are not required. If materials in a container require additional handling, or are to be used by the Off-Site Source Recovery Project for specific purposes such as dose rate studies, use as calibration sources, or other needs, the containers are trans-shipped to Wing 9 of the Chemistry and Metallurgy Research Building.

Actinide sources that DOE determines were generated as part of defense activities are eligible for disposal at WIPP as transuranic waste. The Off-Site Source Recovery Project also expects to continue to receive a certain number of actinide sources that are not designated defense waste and are not eligible for disposal at WIPP. As NNSA further documents the origin and history of these actinide sources, some of them may meet the criteria for acceptance at WIPP, and others will be managed pursuant to Public Law 99-240 (see Section J.3.3.1).

As of February 2008, the Off-Site Source Recovery Project had managed about 16,750 sources, of which about 15,300 (91 percent) had been delivered to LANL for safe storage, and the remaining 9 percent had been managed by other means such as reuse or disposal by commercial entities. Of the sources that had been delivered to LANL by this date, about 3,500 were sent off site for disposition, mainly to WIPP. The remaining sources will be sent to WIPP if determined to be eligible for WIPP disposal, disposed of as Greater-Than-Class C waste, or managed by other means such as reuse. In the future, NNSA expects to manage about 2,000 actinide sources per year, most of which would be temporarily stored at LANL pending disposal at WIPP, disposal as Greater-Than-Class C waste, or disposition by other means (LANL 2006d). NNSA expects to begin to phase out or greatly downsize the Off-Site Source Recovery Project as Greater-Than-Class C disposal capacity becomes available, which is not expected before 2015.

J.3.2.2 Proposed Project: Increase in the Type and Quantity of Sealed Sources Managed at Los Alamos National Laboratory by the Off-Site Source Recovery Project

Under the Proposed Project, the contractor would be prepared to receive additional sealed sources at LANL in addition to the actinide sources that are currently received by the Off-Site Source Recovery Project. **Table J-5** gives the additional sealed sources registered as of August 2005. As noted above, the Off-Site Source Recovery Project would use LANL facilities when management by commercial or other Federal entities was not appropriate to fulfill its national security mission. Many of the sources identified in Table J-5 may never require storage at LANL but would be transferred directly after recovery by the Off-Site Source Recovery Project to a disposal or other appropriate facility for disposition.

Table J-5 Additional Sources Registered with the Off-Site Source Recovery Project – Newly Eligible Materials

| <i>Nuclide</i> | <i>Number of Sources</i> | <i>Curie Content</i> |
|-----------------|--------------------------|----------------------|
| Cobalt-60 | 354 | 419,919 |
| Strontium-90 | 55 | 3,795,456 |
| Cesium-137 | 419 | 9,366 |
| Radium-226 | 22 | 5.6 |
| Curium-244 | 80 | 135 |
| Californium-252 | 24 | 0.1 |

Sources: LANL 2004d, 2006d.

Management of sealed sources containing additional radionuclides, if directed to LANL, would follow the same approach used for the actinide sources currently under management at LANL. Prior to source packaging and movement to LANL, the Off-Site Source Recovery Project staff would ensure that management at commercial or other Federal locations was not appropriate and would obtain concurrence from NNSA. In addition, existing planning processes would be employed to ensure all prerequisite activities were completed, including:

- Verification that sources meet eligibility requirements for recovery;
- Verification that no recycle or reuse potential exists that would eliminate the necessity for movement of materials to LANL for management;
- Identification that handling and storage facilities exist at LANL for materials to be recovered; and
- Verification that source recovery and management at LANL meet the compliance and authorization envelope of the site.

Upon receipt at LANL, the sealed sources would be managed to minimize impacts on existing and planned NNSA operations within the facilities used to support sealed source management. Shipping containers would be received at the LANL Supply Chain Management receiving warehouse, SM-30, or its replacement. At SM-30, the sealed sources would be subject to standard receiving requirements that include activities such as inspection for damage, radiological survey and, in some cases, verification measurements for special nuclear materials.

Sealed sources that need special handling would be transported to Wing 9 of the Chemistry and Metallurgy Research Building and either stored in DOT-compliant shipping containers or removed from packages for storage in the floor holes. These sealed sources may be moved to the Radiological Sciences Institute at TA-48 after closure of the Chemistry and Metallurgy Research Building (see Section G.3). Most of the remaining sources would remain in their original DOT-compliant shipping containers and would be transported to Area G, TA-54. High activity strontium-90 sources and other high activity sealed sources could be stored in a retrievable configuration in shafts. Radium-226, curium-244 and californium-252, if stored at LANL, would more than likely be stored in pipe overpack containers.

The proposed project would expand the Off-Site Source Recovery Project by a little more than 10 percent. The proposed expansion would require the annual management of about 200 to 250 additional sources compared to the No Action Option. As noted above, many of the additional sources may never require storage at LANL but would be transferred directly to a disposal or other appropriate facility for disposition. Sources delivered to LANL would be safely stored until they could be disposed of as low-level radioactive waste (including Greater-Than-Class C waste if appropriate), or dispositioned by other means such as reuse. NNSA expects to begin to phase out or greatly downsize the Off-Site Source Recovery Project as Greater-Than-Class C disposal capacity becomes available, which is not expected before 2015.

J.3.3 Affected Environment and Environmental Consequences

TA-54 is one of the largest TAs at LANL (943 acres [382 hectares]) (LANL 2003). Its primary function is management of radioactive solid and hazardous chemical wastes. The TA's 3-mile (4.8-kilometer) northern border forms the boundary between LANL and the Pueblo of San Ildefonso, and its southeastern boundary borders the White Rock community in Los Alamos County. Within TA-54, Area G covers approximately 63 acres (25 hectares) at the east end of LANL (LANL 2005). The SM-30 warehouse at TA-3 is LANL's main general warehouse; it can store limited quantities of hazardous or radioactive materials. NNSA has proposed to replace SM-30 with a new warehouse (See Appendix G) that would receive all shipments, including sealed sources.

Because the proposed increase in the type and quantity of increased sealed sources accepted for waste management would potentially affect the waste management and human health areas, this analysis focuses on the affected environment and subsequent potential impacts to these resources. An initial assessment of the potential impacts of the proposed project determined that there would be no or only negligible impacts to the following resource areas and that no further analysis was necessary.

- *Land Resources* – Storage would be in an area that is already disturbed. Activities would comply with land use plans.
- *Geology and Soils* – Activities are not expected to change geology, trigger seismic events, or change slope stability.
- *Water Resources* – Discharges to surface water would not be expected. Groundwater contamination would be highly unlikely because of the containment provided for the sealed sources.
- *Air Quality and Noise* – No air emissions are expected from sealed sources. The only noise would be continued ambient noise at existing levels.
- *Ecological Resources* – Storage of sealed sources would be in developed areas that are devoid of biota.
- *Cultural Resources* – Storage would be in developed areas having no identified cultural resources.
- *Socioeconomics and Infrastructure* – No additional full-time equivalent employees would be expected.
- *Environmental Justice* – No disproportionate impacts to minority or low-income populations are expected.

Transportation, waste management, and human health are discussed in more detail in the following section, because, after arriving at LANL, some of these additional sealed sources would be stored at LANL as waste with no current disposal path.

J.3.3.1 No Action Option

Waste Management

In fiscal year 2003, the DOE General Counsel determined that, due to the source of isotopic materials used in the construction of plutonium-239-bearing sealed sources and the continuous ownership of the contained plutonium-239 by DOE, all plutonium-239 sources resulted from defense activities. This determination made this particular class of sources eligible for disposal at WIPP. As of October 31, 2006, 132 drums of plutonium-239 sealed sources had been shipped to WIPP, and it is expected that remaining plutonium-239 sources will continue to be shipped. This is part of the waste management analysis in the SWEIS.

Table J-6 lists typical types of actinide sources, other than plutonium-239 sources, that have been received or are expected to be received at LANL under the Off-Site Source Recovery Project. Recently, however, the Off-Site Source Recovery Project received a defense determination for some of these plutonium-238 and americium-241 sources. This determination would allow the shipment of 211 drums of plutonium-238 and americium-241 sealed sources from the TA-54 storage site to WIPP. The transportation analysis in this appendix and Chapter 5 addresses the impacts of the shipment of all plutonium-238 and americium-241 sources to WIPP, should a defense determination be made for the remaining material. In addition, there are four strontium-90 radioisotope thermoelectric generators retrievably stored in a below-ground shaft at Area G in TA-54; two other strontium-90 radioisotope thermoelectric generators are being stored above-ground at Area G. The transportation analysis in this appendix and in Chapter 5 addresses the impacts of shipping the generators to the Nevada Test Site, which is being considered for their disposal.

Table J-6 Typical Types of Actinide Sources to be Received at LANL^a

| <i>Source Type^b</i> | <i>Typical Activity (curies/each)</i> |
|--|---------------------------------------|
| Americium-241 calibration sources | 0.005 |
| Plutonium-238 medical sources | 8 |
| Americium-241 medical sources | 0.1 |
| Americium-241 Be well logging sources | 3 |
| Plutonium-238 Be well logging sources | 10 |
| Americium-241 Be general neutron sources | 1 |
| Americium-241 Be and Cesium-137 portable gauge sources | 0.045/0.01 |
| Americium-241 Be portable gauge sources | 0.045 |
| Americium-241 fixed gauges | 0.124 |
| Americium-241 XRF sources | 0.18 |

Be = beryllium, XRF = x-ray fluorescence.

^a Some sources may be eligible for disposal at WIPP. Others would be managed pursuant to Public Law 99-240.

^b Additional plutonium-239 sources from defense activities that may be received by the Project would be disposed of at WIPP.

Note: To convert cubic yards to cubic meters, multiply by 0.76456.

Source: LANL 2004d.

Until DOE identifies a disposal location consistent with the statutory requirements of Public Law 99-240, there would be no defined disposal facility for some of the actinide sources recovered by the Off-Site Source Recovery Project. In July 2007, however, DOE issued an NOI to prepare an *Environmental Impact Statement for the Disposal of Greater-Than-Class-C Low-Level Radioactive Waste* (72 FR 40135). DOE intends that this EIS would enable DOE to select any new or existing disposal locations, facilities, and methods for disposal of commercial Greater-Than-Class C waste and DOE waste having similar characteristics.

Transportation

The 1999 SWEIS addressed the shipment of actinide sealed sources to LANL as part of the transportation analysis. The continued shipment of these sources is included in the No Action Alternative transportation impacts in Chapter 5 of this SWEIS.

As discussed above, some of the actinide sources have received a defense determination and are eligible for disposal at WIPP. This section presents the transportation impacts of shipping actinide sources to WIPP; these impacts are included in the No Action Alternative transportation impacts in Chapter 5 of the SWEIS. It was assumed that about 17,000 actinide sources stored at LANL would be shipped to WIPP. The total numbers of waste containers and shipments were assessed assuming the types of actinide sources listed in Table J-6 and using waste packaging efficiencies estimated by the Off-Site Source Recovery Project (LANL 2004d). This estimate would envelope the impacts from shipping all of the roughly 11,000 actinide sources currently stored at LANL to WIPP. (No sealed sources or other transuranic waste would be shipped to WIPP unless they were determined to be defense-related and met the acceptance criteria for disposal at WIPP.)

Transportation impacts would entail radiation exposure to the transportation crew and to the public along the route from LANL to WIPP, as well as potential radiation exposure and fatalities from traffic accidents. The impacts are presented in terms of doses and latent cancer fatalities (LCFs). (See Appendix K of the SWEIS for a description of the analysis methodology.)

Table J-7 shows the results of this analysis. The maximum total dose to the public for shipment to WIPP would be 0.81 person-rem and the likelihood of an excess LCF would be less than 1 (0.00048 LCF). The collective dose to the crew would be 0.58 person-rem, with less than 1 LCF (0.00035). The risk of an LCF in the population from radiation exposure from a traffic accident is less than 1 (9.9×10^{-8}) and no traffic fatalities would be expected.

As noted, the analysis was for shipping about 17,000 actinide sources from LANL to WIPP. Assuming that LANL annually manages an additional 2,000 actinide sources similar to the types listed in Table J-6, and all are brought to LANL for temporary safe storage (see Section J.3.2.1), then over a 10-year period about 20,000 actinide sources would be managed at LANL in addition to the 11,000 discussed above. If all were sent to WIPP, the impacts for shipping 31,000 actinide sources to WIPP would be about twice as large as those listed in Table J-7.

In addition, six strontium-90 radioisotope thermoelectric generators are stored at LANL until they can be disposed of at a low-level radioactive waste disposal site. The data in Table J-7 show the impacts of shipping them to the Nevada Test Site for disposal. No LCFs would be

expected to the population along the route (0.000028 LCFs) or to the transportation crew (0.000021 LCFs), and no traffic fatalities would be expected.

Table J-7 Incident-Free and Accident Transportation Impacts – No Action Option

| Disposal Location | Number of Shipments | Total Distance Traveled (kilometers) | Crew Dose and Risk | | Public Dose and Risk | | Accidents Radiological and Nonradiological | |
|-------------------|---------------------|--------------------------------------|--------------------|------------|----------------------|------------|--|---------------------------|
| | | | Dose (person-rem) | Risk (LCF) | Dose (person-rem) | Risk (LCF) | Risk (LCF) | Risk (traffic fatalities) |
| WIPP | 21 | 25,402 | 0.58 | 0.00035 | 0.81 | 0.00048 | 9.9×10^{-8} | 0.0003 |
| Nevada Test Site | 1 | 2,500 | 0.035 | 0.000021 | 0.047 | 0.000028 | 5.8×10^{-10} | 0.000025 |

LCF = latent cancer fatality, WIPP = Waste Isolation Pilot Plant.

Note: To convert kilometers to miles, multiply by 0.62137.

J.3.3.2 Proposed Project: Increase in the Type and Quantity of Sealed Sources Managed at Los Alamos National Laboratory by the Off-Site Source Recovery Project

Human Health Impacts

All sealed sources received or planned to be received at LANL are encapsulated or otherwise confined, and no release of the enclosed radioisotopes to the environment is expected during normal operations. Transportation, handling, and storage of sealed sources in properly shielded containers would minimize the radiation dose to involved workers from those sources, which are gamma and neutron radiation emitters. The metal of the sealed source itself would shield beta and alpha radiation emitting radioisotopes. The use of proper operating and administrative procedures coupled with appropriate shielding would ensure that involved worker doses are maintained below their appropriate limits. Noninvolved workers and the public are not expected to receive any measurable doses from the Off-Site Source Recovery Project sources during normal operations.

The *Environmental Assessment for the Radioactive Source Recovery Program* (DOE 1995) provided an estimate of 2.3 millirem for the Chemistry and Metallurgy Research Building Wing 9 Hot Cell involved worker dose for all activities associated with each neutron sealed source. At 100 sources per year, the worker dose would be equivalent to the historical average worker dose at the Chemistry and Metallurgy Research Wing 9 Hot Cell Facility. Furthermore, the environmental assessment estimated a total 15-year campaign worker dose of 17.3 person-rem, which is equivalent to a risk of an LCF in this group of workers of 0.01, or 1 chance in 100.

Waste Management

Under the Proposed Project, the Off-Site Source Recovery Project could bring an expanded range of sealed sources to LANL for storage. Stored sources having radionuclides in concentrations smaller or equal to the Part 61 Class C limits would be evaluated for disposal at existing commercial or DOE low-level radioactive waste disposal facilities. Sources having radionuclides in concentrations larger than the Part 61 Class C limits would be stored until a suitable disposal facility is identified. As noted in Section J.3.3.1, preparation of the *Environmental Impact Statement for the Disposal of Greater-Than-Class C Low-Level*

Radioactive Waste would enable DOE to select any new or existing disposal locations, facilities, and methods for disposal of commercial Greater-Than-Class C waste and DOE waste having similar characteristics.

Transportation

This analysis presents the transportation impacts of each shipment of sealed sources to LANL under the Proposed Project. As discussed above, only the sealed sources for which commercial or other Federal management is not appropriate would be transported to LANL. Because the locations of the sealed sources that would be transported to LANL have not been identified, the analysis used a bounding distant location (Bangor, Maine). Each shipment would involve one sealed source transported by a trailer truck. Each package is assumed to have the same characteristics (dimension and dose rate). The maximum inventories per package for cobalt-60 and cesium-137 isotopes are 6,000 and 10,000 curies, respectively. The maximum inventory for strontium-90 is that of a Sentinel 100F with a maximum of 183,400 curies (as of December 2003). The external dose rate one meter from the trailer is assumed to be 10 millirem per hour.

Table J–8 shows the results of this analysis. The maximum total dose to the public per shipment would be 0.0035 person-rem and the likelihood of an excess LCF would be less than 1 (0.000021 LCF). The collective dose to the crew would be 0.42 person-rem, with less than 1 LCF (0.00025). For each shipment the maximum risk of an LCF in the population from radiation exposure from a traffic accident is less than 1 (9.0×10^{-6}) and no traffic fatalities would be expected.

The stored sources would be ultimately shipped to a facility for disposal or other disposition. Although this facility has not been identified, the impacts of shipment would be bounded by those listed in Table J–8. The impacts from shipping to a facility as distant as Bangor, Maine, would be the same as those for shipping from Bangor, Maine.

Table J–8 Per Shipment Incident-Free and Accident Transportation Impacts – Proposed Project

| <i>Sealed Source Isotope</i> | <i>Total Distance Traveled (kilometers)</i> | <i>Crew Dose and Risk</i> | | <i>Public Dose and Risk</i> | | <i>Accidents Radiological and Nonradiological</i> | |
|------------------------------|---|---------------------------|-------------------|-----------------------------|-------------------|---|----------------------------------|
| | | <i>Dose (person-rem)</i> | <i>Risk (LCF)</i> | <i>Dose (person-rem)</i> | <i>Risk (LCF)</i> | <i>Risk (LCF)</i> | <i>Risk (traffic fatalities)</i> |
| Cesium-137 | 8,144 | 0.42 | 0.00025 | 0.035 | 0.000021 | 1.1×10^{-6} | 0.000092 |
| Cobalt-60 | 8,144 | 0.42 | 0.00025 | 0.035 | 0.000021 | 9.5×10^{-7} | 0.000092 |
| Strontium-90 | 8,144 | 0.42 | 0.00025 | 0.035 | 0.000021 | 9.0×10^{-6} | 0.000092 |

Note: to convert kilometers to miles, multiply by 0.62137.

Facility Accidents

Results of the sealed source accident analysis are presented for two different facilities, Wing 9 of the Chemistry and Metallurgy Research Building and TA-54, Area G, where sealed sources are planned to be handled, stored, and transported. The Wing 9 of the Chemistry and Metallurgy Research Building accident is analyzed at either TA-3 or TA-48. Unlike many other radiological

accidents analyzed for LANL, accidents involving sealed sources involve both an air release and external exposure component because the sealed sources include significant gamma radiation emitters: cobalt-60, cesium-137, and iridium-192. Most other LANL SWEIS accident scenarios involve only plutonium-239 or tritium, neither of which poses an external radiation danger, because they are principally alpha or beta radiation emitters. Therefore, total accident consequences for sealed source bounding accidents are a combination of the airborne release and external radiation contributors. External radiation is a major component of the total noninvolved worker dose, while airborne releases dominate MEI and population dose and contribute to noninvolved worker doses. This is due to the effect of distance on calculated doses. External radiation is reduced by distance and the small, but not insignificant, shielding effect of air over large distances. Airborne releases are diluted over distances, but can maintain significant concentrations, especially if lofted by plume energy resulting from fires and explosions.

As a result of the planning for expanding the project, specific limits on activity of sealed sources to be stored and managed at TA-54, Area G, and Wing 9 of the Chemistry and Metallurgy Research Building were established (LANL 2006d). These limits are based on equivalence to plutonium-239 curies as sources of inhalation dose associated with postulated accidents. The limits refer to the allowable inventory of each nuclide. If one nuclide were present at its limiting inventory, then none of the other nuclides could be present. These limits are presented in **Tables J-9 and J-10**.

Table J-9 Maximum Allowable Sealed Source Radioisotope Inventory at Technical Area 54, Area G

| <i>Radioisotope</i> | <i>All Domes (curies)</i> | <i>Individual Dome (curies)</i> | <i>Shipping Container (curies)^a</i> |
|---------------------|---------------------------------|---------------------------------|--|
| Cobalt-60 | 8.18×10^5 | 1.36×10^5 | 6,000 |
| Strontium-90 | 5.88×10^7 ^b | 9.8×10^6 ^b | 431,000 ^b |
| Cesium-137 | 1.37×10^6 | 2.27×10^5 | 10,000 |
| Iridium-192 | 2.05×10^4 | 3.41×10^3 | 150 |
| Radium-226 | 630 | 105 | 5 |
| Curium-244 | 13,700 | 2,270 | 100 |
| Californium-252 | 30 | 30 | 30 |

^a LANL 2006d.

^b DOE 2004a.

Table J-10 Maximum Allowable Sealed Source Radioisotope Inventory at Chemistry and Metallurgy Research Building Wing 9

| <i>Radioisotope</i> | <i>Total Hot Cell and Corridor (curies)</i> | <i>Floor Including the Pit (curies)</i> | <i>Each Floor Hole (curies)</i> | <i>Security (curies)</i> | <i>Shipping Container (curies)</i> |
|---------------------|---|---|---------------------------------|--------------------------|------------------------------------|
| Cobalt-60 | 3.42×10^6 | 88,400 | 291 | 1.0×10^7 | 6,000 |
| Strontium-90 | 580,000 | 15,000 | 3,880 | No Limit | 431,000 ^a |
| Cesium-137 | 2.35×10^7 | 607,000 | 4,070 | No Limit | 10,000 |
| Iridium-192 | 2.64×10^7 | 681,000 | 530 | 10,000 | 150 |
| Radium-226 | 87,400 | 2,260 | 156 | No Limit | 5 |
| Curium-244 | 2,850 | 73.7 | 129 | 1,000 | 100 |
| Californium-252 | 6,100 | 158 | 60.3 | 200 | 30 |

^a DOE 2004a.

Source: LANL 2006d.

This approach provides a conservative estimate of the doses associated with an accident involving storage of sealed sources because the entire allowable plutonium-239-equivalent inventory at a storage location would not be committed to storage of a single type of sealed source. Instead, most of the allowable inventory would be reserved for other operations in the facility and only a portion would be used for storage of sealed sources. In addition, the portion that would be allowed for storage of sealed sources would likely be used for a variety of sources rather than sources containing a single isotope. Therefore, the results presented in the following discussion provide a hypothetical upper limit of the radiological impacts of an accident. This approach is used to provide an enveloping risk because of the unavailability of accurate data on the magnitude of sealed sources of each type that the Off-Site Source Recovery Project may need to manage at LANL. However, the storage of the sealed sources would be coordinated such that the plutonium-239-equivalent inventory would be managed within each facility's allowable inventory limit.

LANL staff evaluated the storage of sealed sources at TA-54, Area G, and determined that the bounding accident for this location would be an aircraft crash into one dome, with a resulting fire of 300 gallons (1,140 liters) of JP-5 fuel carried by the aircraft (LANL 2004e). This accident would result in a 2-minute fire with a fire energy of 294.3 megawatts. This accident, with an annual frequency of 1.3×10^{-5} (1 chance in 77,000) was analyzed using the MACCS2 computer code for airborne release of sealed source radioisotopes and by the ZYLIND computer code for direct external gamma radiation dose from one shipping container with the maximum allowed sealed source radioisotope content exposed without shielding. MACCS2 was used to calculate noninvolved worker, maximally exposed individual (MEI), and 50-mile (80-kilometer) radius population dose from airborne releases. ZYLIND was used to calculate the external radiation dose to the noninvolved worker and MEI. ZYLIND is a digital interactive computer code that calculates gamma radiation dose rate from cylindrical sources with multiple shielding capabilities (ORNL 1990). ZYLIND accounts for dose buildup factors and shielding effects. External exposure to gamma radiation is not a contributor to the 50-mile (80-kilometer) radius population dose. The accident analysis was repeated for each nuclide using the assumptions and inputs indicated in **Tables J-11** and **J-12**.

Cobalt-60 was found to cause the maximum exposure to the noninvolved worker as a result of the external radiation exposure pathway. Inhalation of transuranics, curium-244 from TA-54, and californium-252 from Wing 9, resulted in the maximum MEI exposure; the direct external radiation exposure at these distances was less important. Cesium-137 resulted in maximum exposure to the surrounding population because of its external dose plus its contribution to internal dose through ingestion of food stuffs. **Table J-13** shows the exposure consequences and risks from this accident, assuming that cesium-137 is present at its limits.

Table J-11 Sealed Source Aircraft Impact Crash Accident at Technical Area 54, Area G Dome Airborne Release Source Term for MACCS2 Calculation

| <i>Sealed Source Radioisotope</i> | <i>Damage Ratio</i> | <i>Airborne Release Fraction</i> | <i>Respirable Fraction</i> | <i>Leak Path Factor</i> | <i>Source Term</i> |
|-----------------------------------|---------------------|----------------------------------|----------------------------|-------------------------|--------------------|
| Impact | | | | | |
| Cobalt-60 | 0.05 | 0.001 | 0.3 | 1.0 | 2.04 |
| Strontium-90 | 0 ^a | 0.001 | 0.3 | 1.0 | 0 |
| Cesium-137 | 0.05 | 0.001 | 0.3 | 1.0 | 3.41 |
| Iridium-192 | 0.05 | 0.001 | 0.3 | 1.0 | 0.0512 |
| Curium-244 | 0.05 | 0.001 | 0.3 | 1.0 | 0.0341 |
| Californium-252 | 0.05 | 0.001 | 0.3 | 1.0 | 0.00045 |
| Fire | | | | | |
| Cobalt-60 | 0.05 | 0.006 | 0.01 | 1.0 | 0.408 |
| Strontium-90 | 0 ^a | 0.006 | 0.01 | 1.0 | 0 |
| Cesium-137 | 0.05 | 0.006 | 0.01 | 1.0 | 0.681 |
| Iridium-192 | 0.05 | 0.006 | 0.01 | 1.0 | 0.0102 |
| Curium-244 | 0.05 | 0.006 | 0.01 | 1.0 | 0.00682 |
| Californium-252 | 0.05 | 0.006 | 0.01 | 1.0 | 0.00009 |

^a Strontium-90 sources will be kept in a covered belowground shaft a distance from any dome.
Source: LANL 2004e.

Table J-12 Sealed Source Aircraft Impact Crash Accident at Technical Area 54, Area G Dome Air Release and Direct Radiation Source Terms (in curies)

| <i>Sealed Source Radioisotope</i> | <i>Air Release Source Term</i> | <i>Direct Radiation Source Term (one shipping container)</i> |
|-----------------------------------|--------------------------------|--|
| Cobalt-60 | 2.45 | 6,000 |
| Strontium-90 ^a | 0 | 0 |
| Cesium-137 | 4.09 | 10,000 |
| Iridium-192 | 0.0614 | 150 |
| Curium-244 | 0.0409 | 100 |
| Californium-252 | 0.00054 | 30 |

^a Strontium-90 sources will be kept in a covered belowground shaft a distance from any dome.
Source: LANL 2004e.

Table J-13 Dose and Risk Consequences of Sealed Source Aircraft Impact Crash Accident at Technical Area 54, Area G Dome

| <i>Accident Component</i> | <i>Noninvolved Worker at (110 Yards [100 meters])</i> | <i>Maximally Exposed Individual</i> | <i>50-Mile (80-kilometer) Population</i> |
|---|---|-------------------------------------|--|
| Airborne Release from One Dome | | | |
| Dose | 0.017 rem ^a | 0.084 rem ^b | 111 person-rem ^c |
| Annual Risk (LCF per year) | 1.3×10^{-10} | 6.6×10^{-10} | 8.7×10^{-7} |
| 2-Hour Exposure to Direct Radiation from One Breached Shipping Container | | | |
| Dose | 0.5 rem ^a | Insignificant | Insignificant |
| Annual Risk (LCF per year) | 3.9×10^{-9} | Insignificant | Insignificant |
| Accident Total | | | |
| Dose | 0.52 rem ^a | 0.084 rem ^b | 111 person-rem ^c |
| Risk (LCF per year) | 4.0×10^{-9} | 6.6×10^{-10} | 8.7×10^{-7} |

LCF = latent cancer fatality.

^a Maximum total dose would result from direct exposure to and airborne release of cobalt-60.

^b Maximum total dose would result from airborne release of curium-244.

^c Maximum total dose would result from airborne release of cesium-137.

Results of this accident are the total of the airborne release and unshielded shipping container direct external radiation dose calculation. The high plume energy from the burning aircraft fuel decreases the dose to the noninvolved worker and MEI because a portion of the plume is carried beyond these close-in locations. This same higher energy plume, however, contributes to a larger population dose by decreasing deposition near the release location. The accident contribution from just one unshielded shipping container is a significant component of the total dose to the noninvolved worker because the effects of direct exposure to external radiation are largest near the accident. The external radiation dose to the 50-mile (80-kilometer) radius population is small because the dose rate would drop as the square of the distance at the relatively large distances of the population. Only the gamma dose rate was calculated for exposure to external radiation, based on a factor of 1,000 to 10,000 lower source term for the neutron emitters curium-244 and californium-252, compared to the gamma emitters cobalt-60, cesium-137, and iridium-192.

Based on the Chemistry and Metallurgy Research Building’s Basis of Interim Operations and other SWEIS calculations of accidents, the bounding, risk-dominant accident was determined to be a severe earthquake collapse followed by a fire in Wing 9.⁸ This accident (plume energy of 2.4 megawatts and 30-minute duration) has a frequency of 2.4×10^{-4} (1 chance in 4,200) per year and can be assumed to cause a level of damage to sealed sources in the corridor and hot cell equivalent to the aircraft crash accident at TA-54, Area G. Using the same values of damage ratio, airborne release fraction, respirable fraction, and leak path factor as for TA-54, Area G, but using the material at risk for Wing 9 of the Chemistry and Metallurgy Research Building, **Table J–14** presents the airborne release and external radiation source terms assuming that one shipping container having the maximum allowed sealed source radioisotope content is exposed without any shielding. Calculation results are presented in **Tables J–15** and **J–16** for both the airborne release and external exposure from sealed sources at Wing 9 of the Chemistry and Metallurgy Research Building or TA-48, a proposed future location for hot cell operations (see Appendix G).

Table J–14 Sealed Source Severe Earthquake and Fire Accident at Chemistry and Metallurgy Research Building Wing 9 Air Release and Direct Radiation Source Terms (in curies)

| <i>Sealed Source Radioisotope</i> | <i>Air Release Source Term</i> | <i>Direct Radiation Source Term (one shipping container)</i> |
|-----------------------------------|--------------------------------|--|
| Cobalt-60 | 61.6 | 6,000 |
| Strontium-90 | 10.4 | 431,000 |
| Cesium-137 | 423 | 10,000 |
| Iridium-192 | 475 | 150 |
| Radium-226 | 1.6 | 5 |
| Curium-244 | 0.051 | 100 |
| Californium-252 | 0.11 | 30 |

⁸ Wing 9 of the Chemistry and Metallurgy Research Building has a hot cell, floor holes, and other storage areas. The Wing 9 hot cell capabilities are planned to be part of the Radiological Sciences Institute proposed to be constructed in TA-48. The accident analysis for materials stored in Wing 9 was performed for the current Chemistry and Metallurgy Research Building location in TA-3 as well as for a location in TA-48.

Table J–15 Sealed Source Severe Earthquake Collapse and Fire Accident at Chemistry and Metallurgy Research Building Wing 9 Dose and Risk Consequences at Technical Area 3 Location

| <i>Accident Component</i> | <i>Noninvolved Worker at 110 Yards (100 meters)</i> | <i>Maximally Exposed Individual</i> | <i>50-Mile (80-kilometer) Population</i> |
|---|---|-------------------------------------|--|
| Airborne Release from Wing 9 Total Hot Cell and Corridor | | | |
| Dose | 0.71 rem ^a | 0.099 rem ^b | 11,600 person-rem ^c |
| Annual Risk | 1.0×10^{-7} | 1.4×10^{-8} | 0.0017 |
| 2-Hour Exposure to Direct Radiation from One Breached Shipping Container | | | |
| Dose | 0.5 rem ^a | Insignificant | Insignificant |
| Annual Risk | 7.2×10^{-8} | Insignificant | Insignificant |
| Accident Total | | | |
| Dose | 1.2 rem ^a | 0.099 rem ^b | 11,600 person-rem ^c |
| Risk | 1.7×10^{-7} | 1.4×10^{-8} | 0.0017 |

^a Maximum total dose would result from direct exposure to and airborne release of cobalt-60.

^b Maximum total dose would result from airborne release of californium-252.

^c Maximum total dose would result from airborne release of cesium-137.

Table J–16 Sealed Source Severe Earthquake Collapse and Fire Accident Dose and Risk Consequences at Technical Area 48 Location

| <i>Accident Component</i> | <i>Noninvolved Worker at 110 Yards (100 meters)</i> | <i>Maximally Exposed Individual</i> | <i>50-Mile (80-kilometer) Population</i> |
|---|---|-------------------------------------|--|
| Airborne Release from Wing 9 Total Hot Cell and Corridor | | | |
| Dose | 0.71 rem ^a | 0.098 rem ^b | 11,400 person-rem ^c |
| Annual Risk | 1.0×10^{-7} | 1.4×10^{-8} | 0.0016 |
| 2-Hour Exposure to Direct Radiation from One Breached shipping Container | | | |
| Dose | 0.5 rem ^a | Insignificant | Insignificant |
| Annual Risk | 7.2×10^{-8} | Insignificant | Insignificant |
| Accident Total | | | |
| Dose | 1.2 rem ^a | 0.098 rem ^b | 11,400 person-rem ^c |
| Risk | 1.7×10^{-7} | 1.4×10^{-8} | 0.0016 |

^a Maximum total dose would result from direct exposure to and airborne release of cobalt-60.

^b Maximum total dose would result from airborne release of californium-252.

^c Maximum total dose would result from airborne release of cesium-137.

As addressed in Appendix D, Section D.4, an updated probabilistic seismic hazard analysis providing an improved understanding of the seismic characteristics of LANL was completed in 2007. Based on the updated information, the probability of exceedance for the ground acceleration used in this accident analysis, and the corresponding radiological risk, is higher than previously estimated by 50 percent. This increase results in a risk of an LCF of 2.1×10^{-8} (1 chance in 48 million) for the MEI and 1.5×10^{-7} (1 chance in 6.5 million) for the noninvolved worker, and an increased chance of an LCF in the general population of 0.0025 (1 chance in 400).

The nearest public access to the Chemistry and Metallurgy Research Building, Diamond Drive, which is approximately 164 feet (50 meters) from the Chemistry and Metallurgy Research Building, is closer than the nearest site boundary to this facility. The same assumptions used to calculate dose to the MEI were applied to an individual at this location. The dose to an individual outside at Diamond Drive during the duration of the release would be 4.32 rem,

42 percent of which would be from external exposure to gamma radiation. Such a dose would result in an increased chance of a fatal latent cancer during the lifetime of the individual of 0.0026, or approximately 1 chance in 385.

The total (airborne release and direct radiation) accident dose and risk to the noninvolved worker, MEI, and population for accidents involving sealed sources at TA-54, Area G, Wing 9 of the Chemistry and Metallurgy Research Building at TA-3, and a facility with capabilities equivalent to Wing 9 located at TA-48 are presented in **Table J-17**.

Table J-17 Total Accident Doses and Risks From Sealed Sources at Technical Area 3, Technical Area 48, and Technical Area 54

| <i>Dose Receptor</i> | <i>Aircraft Crash and Fire at TA-54 Area G</i> | <i>Severe Seismic Event and Fire CMR Wing 9 TA-3</i> | <i>Severe Seismic Event and Fire TA-48</i> |
|-------------------------------|--|--|--|
| Noninvolved Worker Dose (rem) | 0.52 | 1.2 | 1.2 |
| Noninvolved Worker Risk | 4.0×10^{-9} | 1.7×10^{-7} | 1.7×10^{-7} |
| MEI Dose (rem) | 0.084 | 0.099 | 0.098 |
| MEI Risk | 6.6×10^{-10} | 1.4×10^{-8} | 1.4×10^{-8} |
| Population Dose (person-rem) | 111 | 11,600 | 11,400 |
| Population Risk | 8.7×10^{-7} | 0.0017 | 0.0016 |

TA = technical area, CMR = Chemistry and Metallurgy Research Building, MEI = maximally exposed individual.

The higher doses for the Wing 9 accident are principally due to the larger source term. Its larger risks are attributed to the larger accident frequency along with the larger source term.

All three accident scenarios analyzed involving sealed sources result in a risk of a LCF during the lifetime of a noninvolved worker or MEI at no greater than 1.7×10^{-7} (one chance in 5,900,000) per year of operation. The 50-mile (80-kilometer) population would not receive a fatal radiation dose for any of these accidents. The highest LCF risk to the population would result from the Wing 9 accident.

If mitigation measures are needed for potential sealed source accidents, they would include placing sealed sources in locations where they would not be susceptible to damage from an aircraft crash, fire, or seismic event (kept underground like the strontium-90 radioisotope thermoelectric generators at TA-54). Another potential mitigation measure might include the use of lower limits for maximum allowable source radioisotope activity in shipping containers, the TA-54 domes, or Wing 9 of the Chemistry and Metallurgy Research Building. Storage containers that can be shown to maintain their integrity under fire, crash, and seismic event loads also would mitigate the consequences of these potential accidents.

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APPENDIX K
EVALUATION OF HUMAN HEALTH EFFECTS FROM
TRANSPORTATION

APPENDIX K

EVALUATION OF HUMAN HEALTH EFFECTS FROM TRANSPORTATION

K.1 Introduction

Transportation of any commodity involves a risk to transportation crewmembers and members of the public. This risk results directly from transportation-related accidents and indirectly from increased levels of pollution from vehicle emissions, regardless of the cargo. The transportation of certain materials, such as hazardous or radioactive waste, can pose an additional risk due to the unique nature of the material itself. To permit a complete appraisal of the environmental impacts of the alternatives considered in this Site-Wide Environmental Impact Statement (SWEIS), the human health risks associated with the transportation of radioactive materials are assessed in this appendix.

This appendix provides an overview of the approach used to assess the human health risks that could result from transportation. The topics in this appendix include the scope of the assessment, packaging and determination of potential transportation routes, analytical methods used for the risk assessment (such as computer models), and important assessment assumptions. In addition, to aid in the understanding and interpretation of the results, specific areas of uncertainty are described with an emphasis on how the uncertainties could affect comparisons of the alternatives.

The risk assessment results are presented in this appendix in terms of “per-shipment” risk factors, as well as the total risks for a given alternative. Per-shipment risk factors provide an estimate of the risk from a single shipment. The total risks for a given alternative are estimated by multiplying the expected number of shipments by the appropriate per-shipment risk factors.

K.2 Scope of Assessment

The scope of the transportation human health risk assessment, including the alternatives and options, transportation activities, potential radiological and nonradiological impacts, and transportation modes considered, is described in this section. There are several shipping arrangements for various radioactive materials that cover all alternatives evaluated. This evaluation focuses on using onsite and offsite public highway systems. Additional details of the assessment are provided in the remaining sections of this appendix.

K.2.1 Transportation-related Activities

The transportation risk assessment is limited to estimating the human health risks related to transportation for each alternative. The risks to workers or to the public during loading, unloading, and handling prior to or after shipment are not included in the transportation assessment. The transportation risk assessment does not address possible impacts of increased transportation levels on local traffic flow, noise levels, or infrastructure. The risks from these activities are considered as part of the facility operation impacts.

K.2.2 Radiological Impacts

For each alternative, radiological risks (those risks that result from the radioactive nature of the materials) are assessed for both incident-free (normal) and accident transportation conditions. The radiological risk associated with incident-free transportation conditions would result from the potential exposure of people to external radiation in the vicinity of a shipment. The radiological risk from transportation accidents would come from the potential release and dispersal of radioactive material into the environment during an accident and the subsequent exposure of people.

All radiological impacts are calculated in terms of committed dose and associated health effects in the exposed populations. The radiation dose calculated is the total effective dose equivalent (see Title 10 of the *Code of Federal Regulations* [CFR], Part 20), which is the sum of the effective dose equivalent from external radiation exposure and the 50-year committed effective dose equivalent from internal radiation exposure. Radiation doses are presented in units of roentgen equivalent man (rem) for individuals and person-rem for collective populations. The impacts are further expressed as health risks in terms of latent cancer fatalities (LCFs) in exposed populations using the dose-to-risk conversion factors recommended by the U.S. Department of Energy (DOE) Office of NEPA (National Environmental Policy Act) Policy and Compliance, based on Interagency Steering Committee on Radiation Safety guidance (DOE 2003a).

K.2.3 Nonradiological Impacts

In addition to the radiological risks posed by transportation activities, vehicle-related risks are also assessed for nonradiological causes (causes related to the transport vehicles only; not their radioactive cargo) for the same transportation routes. The nonradiological transportation risks, which would be incurred for similar shipments of any commodity, are assessed for accident conditions. The nonradiological accident risk refers to the potential occurrence of transportation accidents that directly result in fatalities unrelated to the shipment of cargo.

Nonradiological risks during incident-free transportation conditions could also be caused by potential exposure to increased vehicle exhaust emissions. As explained in Section K.5.2, these emission impacts were not considered.

K.2.4 Transportation Modes

All shipments are assumed to take place by dedicated truck.

K.2.5 Receptors

Transportation-related risks are calculated and presented separately for workers and members of the general public. The workers considered are truck crewmembers involved in transportation and inspection of the packages. The general public includes all persons who could be exposed to a shipment while it is moving or stopped during transit. For the incident-free operation, the affected population includes individuals living within 0.5 miles (800 meters) of each side of the road. Potential risks are estimated for the affected populations and for the hypothetical maximally exposed individual (MEI). For incident-free operation, the MEI would be a resident living near the transportation route and exposed to all shipments transported on the route. For

accident conditions, the affected population includes individuals residing within 50 miles (80 kilometers) of the accident, and the MEI would be an individual located 330 feet (100 meters) directly downwind from the accident. The risk to the affected population is a measure of the radiological risk posed to society as a whole by the alternative being considered. As such, the impact on the affected population is used as the primary means of comparing alternatives.

K.3 Packaging and Transportation Regulations

K.3.1 Packaging Regulations

The primary regulatory approach to promote safety from radiological exposure is the specification of standards for the packaging of radioactive materials. Packaging represents the primary barrier between the radioactive material being transported and radiation exposure to the public, workers, and the environment. Transportation packaging for radioactive materials must be designed, constructed, and maintained to contain and shield its contents during normal transport conditions. For highly radioactive material, such as high-level radioactive waste or spent nuclear fuel, packagings must contain and shield their contents in the event of severe accident conditions. The type of packaging used is determined by the total radioactive hazard presented by the material within the packaging. Four basic types of packaging are used: Excepted, Industrial, Type A, and Type B.

Excepted packagings are limited to transporting materials with extremely low levels of radioactivity. Industrial packagings are used to transport materials that, because of their low concentration of radioactive materials, present a limited hazard to the public and the environment. Type A packagings are designed to protect and retain their contents under normal transport conditions and must maintain sufficient shielding to limit radiation exposure to handling personnel. Type A packaging, typically a 55-gallon (208-liter) drum or standard waste box, is commonly used to transport radioactive materials with higher concentrations or amounts of radioactivity than Excepted, or Industrial packagings. Type B packagings are used to transport material with the highest radioactivity levels, and are designed to protect and retain their contents under transportation accident conditions. They are described in more detail in the following sections. Packaging requirements are an important consideration for transportation risk assessment. Appendix F of the 1999 *Site-Wide Environmental Impact Statement for Continued Operation of Los Alamos National Laboratory, Los Alamos, New Mexico, (1999 SWEIS)* (DOE 1999a) provides a listing and characteristics of the packagings assumed to be used for this SWEIS.

Radioactive materials shipped in Type A containers, or packagings, are subject to specific radioactivity limits, identified as A1 and A2 values in 49 CFR 173.435 (“Table of A1 and A2 Values for Radionuclides”). In addition, external radiation limits, as prescribed in 49 CFR 173.441 (“Radiation Level Limitations”), must be met. If the A1 or A2 limits are exceeded, the material must be shipped in a Type B container unless it can be demonstrated that the material meets the definition of “low specific activity.” If the material qualifies as low specific activity as defined in 10 CFR Part 71 (“Packaging and Transportation of Radioactive Material”) and 49 CFR Part 173 (Shippers—General Requirements for Shipments and Packagings), it may be shipped in an approved low-specific-activity shipping container. Type B

containers, or casks, are subject to the radiation limits in 49 CFR 173.441, but no quantity limits are imposed except in the case of fissile materials and plutonium.

Type A packages are designed to retain their radioactive contents in normal transport. Under normal conditions, a Type A package must withstand:

- Operating temperatures ranging from -40 degrees Celsius (°C) (-40 degrees Fahrenheit [°F]) to 70 °C (158 °F);
- External pressures ranging from 0.25 to 1.4 kilograms per square centimeter (3.5 to 20 pounds per square inch);
- Normal vibration experienced during transportation;
- Simulated rainfall of 5 centimeters (2 inches) per hour for 1 hour;
- Free fall from 0.3 to 1.2 meters (1 to 4 feet), depending on the package weight;
- Water immersion-compression tests; and
- Impact of a 6-kilogram (13-pound) steel cylinder with rounded ends dropped from 1 meter (40 inches) onto the most vulnerable surface.

Type B packages are designed to retain their radioactive contents in both normal and accident conditions. In addition to the normal conditions outlined earlier, under accident conditions, a Type B package must withstand:

- Free drop from 9 meters (30 feet) onto an unyielding surface in a position most likely to cause damage;
- Free drop from 1 meter (3.3 feet) onto the end of a 15-centimeter (6-inch) diameter vertical steel bar;
- Exposure to temperatures of 800 °C (1,475 °F) for at least 30 minutes;
- For all packages, immersion in at least 15 meters (50 feet) of water;
- For fissile material packages, immersion in at least 0.9 meters (3 feet) of water in an orientation most likely to result in leakage; and
- For spent nuclear fuel packages, immersion in at least 200 meters (660 feet) of water for 1 hour.

Compliance with these requirements is demonstrated by using a combination of simple calculation methods, computer modeling techniques, or scale-model or full-scale testing of transportation packages, or casks.

K.3.2 Transportation Regulations

The regulatory standards for packaging and transporting radioactive materials are designed to achieve four primary objectives:

- Protect persons and property from radiation emitted from packages during transportation by specific limitations on the allowable radiation levels;
- Contain radioactive material in the package (achieved by packaging design requirements based on performance-oriented packaging integrity tests and environmental criteria);
- Prevent nuclear criticality (an unplanned nuclear chain reaction that could occur as a result of concentrating too much fissile material in one place); and
- Provide physical protection against theft and sabotage during transit.

The U.S. Department of Transportation (DOT) regulates the transportation of hazardous materials in interstate commerce by land, air, and water. DOT specifically regulates the carriers of radioactive materials and the conditions of transport, such as routing, handling and storage, and vehicle and driver requirements. DOT also regulates the labeling, classification, and marking of radioactive material packagings.

The U.S. Nuclear Regulatory Commission (NRC) regulates the packaging and transporting of radioactive material for its licensees, including commercial shippers of radioactive materials. In addition, under an agreement with DOT, NRC sets the standards for packages containing fissile materials and Type B packagings.

DOE, through its management directives, Orders, and contractual agreements, ensures the protection of public health and safety by imposing on its transportation activities standards equivalent to those of DOT and NRC. According to 49 CFR 173.7(d), packagings made by or under the direction of DOE may be used for transporting Class 7 materials (radioactive materials) when the packages are evaluated, approved, and certified by DOE against packaging standards equivalent to those specified in 10 CFR Part 71 (“Packaging and Transportation of Radioactive Material”).

The DOT also has requirements that help to reduce transportation impacts. Some requirements affect drivers, packaging, labeling, marking, and placarding. Others specifying the maximum dose rate from radioactive material shipments help to reduce incident-free transportation doses.

The Federal Emergency Management Agency is responsible for establishing policies for, and coordinating civil emergency management, planning, and interaction with, Federal Executive agencies that have emergency response functions in the event of a transportation incident. The Federal Emergency Management Agency, an agency of the Department of Homeland Security, coordinates Federal and state participation in developing emergency response plans and is responsible for the development of the interim Federal Radiological Emergency Response Plan. This plan is designed to coordinate Federal support to state and local governments, upon request, during the event of a transportation incident involving radioactive materials.

K.4 Transportation Analysis Impact Methodology

The transportation risk assessment is based on the alternatives described in Chapter 3 of the SWEIS. **Figure K-1** summarizes the transportation risk assessment methodology. After the SWEIS alternatives were identified and the requirements of the shipping campaign were understood, data were collected on material characteristics and accident parameters.

Transportation impacts calculated in this SWEIS are presented in two parts: impacts of incident-free or routine transportation and impacts of transportation accidents. Impacts of incident-free transportation and transportation accidents were further divided into nonradiological and radiological impacts. Nonradiological impacts could result from transportation accidents in terms of traffic fatalities. Radiological impacts of incident-free transportation include impacts on members of the public and crew from radiation emanating from materials in the shipment. Radiological impacts from accident conditions consider all foreseeable scenarios that could damage transportation packages leading to releases of radioactive materials to the environment.

The impact of transportation accidents is expressed in terms of probabilistic risk, which is the probability of an accident multiplied by the consequences of that accident and summed over all reasonably conceivable accident conditions. Hypothetical transportation accident conditions ranging from low-speed “fender-bender” collisions to high-speed collisions with or without fires were analyzed. The frequencies of accidents and consequences were evaluated using a method developed by NRC and published in the *Final Environmental Impact Statement on the Transportation of Radioactive Materials by Air and Other Modes*, NUREG-0170 (NRC 1977); *Shipping Container Response to Severe Highway and Railway Accident Conditions*, NUREG/CR-4829 (NRC 1987); and, *Reexamination of Spent Fuel Shipping Risk Estimates*, NUREG/CR-6672 (NRC 2000). Hereafter, these reports are cited as: *Radioactive Material Study*, NUREG-0170; *Modal Study*, NUREG/CR-4829; and *Reexamination Study*, NUREG/CR-6672. Radiological accident risk is expressed in terms of additional LCFs, and nonradiological accident risk is expressed in terms of additional immediate (traffic) fatalities. Incident-free risk is also expressed in terms of additional LCFs.

Transportation-related risks are calculated and presented separately for workers and members of the general public. The workers considered are truck crewmembers involved in the actual transportation. The general public includes all persons who could be exposed to a shipment while it is moving or stopped during transit.

The first step in the ground transportation analysis is to determine the distances and populations along the routes. The Transportation Routing Analysis Geographic Information System (TRAGIS) computer program (Johnson and Michelhaugh 2003) was used to choose representative routes and the associated distances and populations. This information, along with the properties of the material being shipped and route-specific accident frequencies, was entered into the RADTRAN 5 computer code (Neuhauser and Kanipe 2003), which calculates incident and accident risks on a per-shipment basis. The risks under each alternative are determined by summing the products of per-shipment risks for each waste type by its number of shipments.

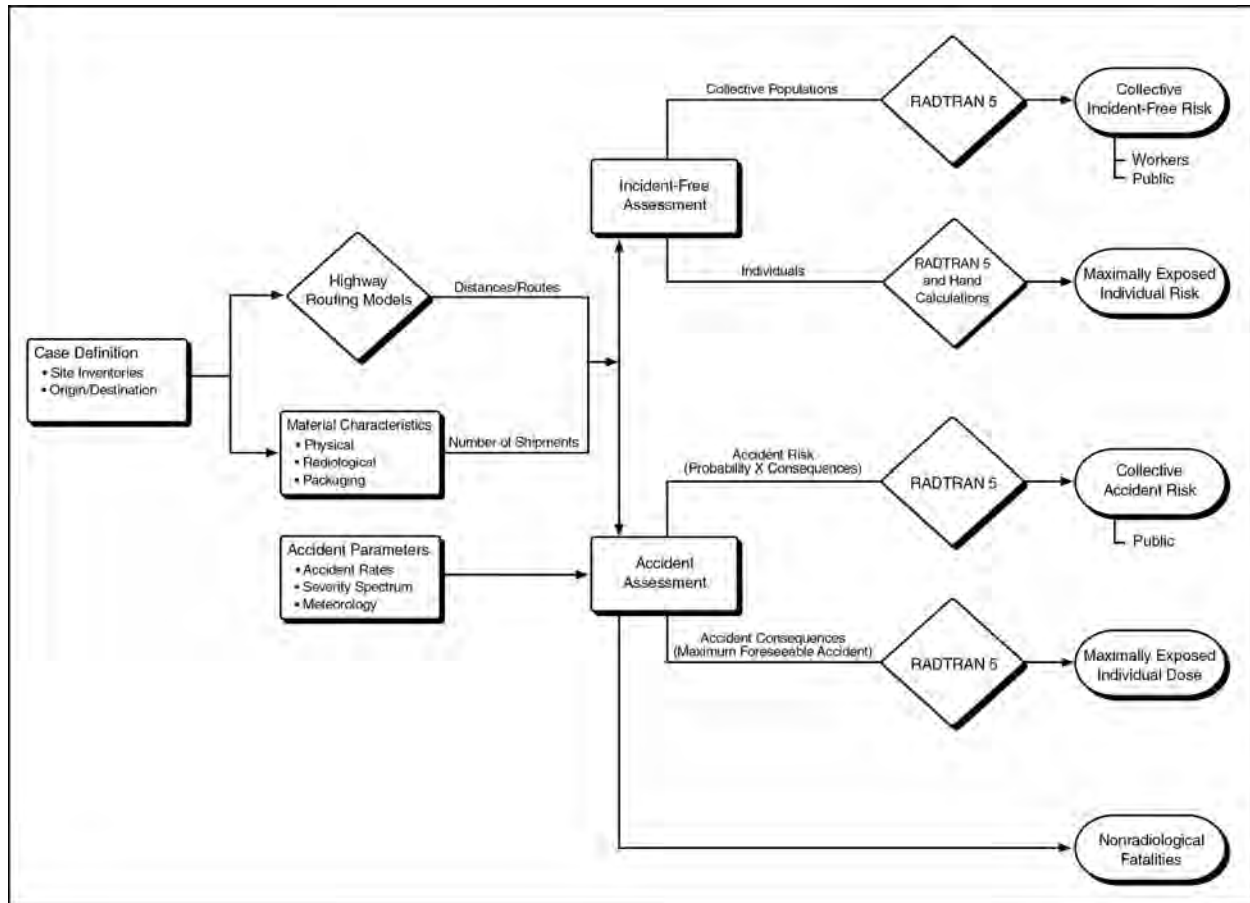


Figure K-1 Transportation Risk Assessment

The RADTRAN 5 computer code (Neuhauser and Kanipe 2003) is used for incident-free and accident risk assessments to estimate the impacts on populations. RADTRAN 5 was developed by Sandia National Laboratories to calculate population risks associated with the transportation of radioactive materials by a variety of modes, including truck, rail, air, ship, and barge. RADTRAN 5 was used to calculate the doses to the MEIs during incident-free operations.

The RADTRAN 5 population risk calculations include both the consequences and probabilities of potential exposure events. The RADTRAN 5 code consequence analyses include cloud shine, ground shine, inhalation, and resuspension exposures. The collective population risk is a measure of the total radiological risk posed to society as a whole by the alternative being considered. As such, the collective population risk is used as the primary means of comparing the various alternatives.

The RISKIND computer code (Yuan et al. 1995) is used to estimate the doses to MEIs and populations for the worst-case maximum reasonably foreseeable transportation accident. The RISKIND computer code was developed for DOE's Office of Civilian Radioactive Waste Management to analyze the exposure of individuals during incident-free transportation. In addition, the RISKIND code was designed to allow a detailed assessment of the consequences to individuals and population subgroups from severe transportation accidents under various environmental settings.

The RISKIND calculations were conducted to supplement the collective risk results calculated using RADTRAN 5. Whereas the collective risk results provide a measure of the overall risks of each alternative, the RISKIND calculations are meant to address areas of specific concern to individuals and population subgroups. Essentially, the RISKIND analyses are meant to address “What if” questions, such as “What if I live next to a site access road?” or “What if an accident happens near my town?”

K.4.1 Transportation Routes

The types of radioactive and nonradioactive materials that would be expected to require offsite transport include special nuclear material, low-level radioactive waste, transuranic waste, irradiated target material, industrial waste, and hazardous waste. These materials would be transported to, from, and on the Los Alamos National Laboratory (LANL) site during routine operations. Offsite shipments, both to and from LANL, are carried by commercial carriers (including truck, air freight, and Government trucks) and by DOE safe secure transport trailers. Air freight transportation is performed for special packages with limited quantities. The amount and form of materials that would be transported using air freight are similar to those evaluated in the 1999 SWEIS (DOE 1999a) with similar impacts, and therefore are not reevaluated.

For offsite transport, highway routes were determined using the routing computer program TRAGIS (Johnson and Michelhaugh 2003). The TRAGIS computer program is a geographic-information-system-based transportation analysis computer program used to identify and select highway, rail, and waterway routes for transporting radioactive materials within the United States. Both the road and rail network are 1:100,000-scale databases, which were developed from the U.S. Geological Survey digital line graphs and the U.S. Bureau of the Census Topological Integrated Geographic Encoding and Referencing System. The population densities along each route are derived from 2000 Census Bureau data (Johnson and Michelhaugh 2003). The features in TRAGIS allow users to determine routes for shipment of radioactive materials that conform to DOT regulations as specified in 49 CFR Part 397.

Offsite Route Characteristics

Route characteristics that are important to the radiological risk assessment include the total shipment distance and population distribution along the route. The specific route selected determines both the total potentially exposed population and the expected frequency of transportation-related accidents. Route characteristics are expressed in terms of travel distances and population densities in rural, suburban, and urban areas according to the following breakdown:

- Rural population densities range from 0 to 139 persons per square mile (0 to 54 persons per square kilometer);
- Suburban population densities range from 140 to 3,326 persons per square mile (55 to 1,284 persons per square kilometer); and
- Urban population densities include all population densities greater than 3,326 persons per square mile (1,284 persons per square kilometer).

To assess incident-free and transportation accident impacts, route characteristics were determined for offsite shipments from the LANL site to the:

- Pantex Site in Amarillo, Texas;
- Lawrence Livermore National Laboratory, California;
- Y-12 Complex, and Oak Ridge National Laboratory in Oak Ridge, Tennessee;
- Savannah River Site in Aiken, South Carolina;
- Nevada Test Site in Mercury, Nevada;
- EnergySolutions site in Clive, Utah as a representative of a commercial disposal site;
- East Tennessee Waste Treatment Center in Oak Ridge, Tennessee; and
- Waste Isolation Pilot Plant (WIPP) in Carlsbad, New Mexico.

These sites would constitute the locations where the majority of shipments would be transported. **Table K–1** summarizes the route characteristics for these sites.

Table K–1 Offsite Transport Truck Route Characteristics

| Origin | Destination | Nominal Distance (kilometers) | Distance Traveled in Zones (kilometers) | | | Population Density in Zone (number per square kilometer) | | | Number of Affected Persons ^a |
|---|-----------------------------------|-------------------------------|---|----------|-------|--|----------|---------|---|
| | | | Rural | Suburban | Urban | Rural | Suburban | Urban | |
| Truck Routes | | | | | | | | | |
| LANL | Pantex | 668 | 617 | 42 | 9 | 4.2 | 451.2 | 2135.1 | 63,989 |
| | SRS | 2,680 | 1,987 | 617 | 76 | 11.9 | 314.8 | 2,240.1 | 622,377 |
| | NTS | 1,250 | 1,069 | 141 | 40 | 7.6 | 338.2 | 2,626.2 | 256,117 |
| | Commercial ^b | 1,076 | 938 | 112 | 26 | 6.9 | 386.2 | 2,464.3 | 183,804 |
| | ETWT | 2,248 | 1,759 | 438 | 51 | 10.8 | 300.4 | 2,243.2 | 425,534 |
| | LLNL | 1,822 | 1,632 | 168 | 22 | 8.0 | 312.6 | 2,369.9 | 189,378 |
| | Y-12 | 2,372 | 1,848 | 465 | 59 | 11.0 | 300.8 | 2,271.4 | 471,946 |
| | WIPP | 605 | 568 | 35 | 2 | 5.9 | 251.1 | 1,891.5 | 25,541 |
| Truck Routes (local from I-25 to LANL) | | | | | | | | | |
| | LANL to Pojoaque | 31 | 27 | 3.8 | 0.2 | 5.8 | 362.6 | 2,408.5 | 3,227 |
| | Pojoaque to Santa Fe ^c | 52 | 44 | 8 | 0 | 18.9 | 178.4 | 0 | 3,563 |

SRS = Savannah River Site, NTS = Nevada Test Site, ETWT = East Tennessee Waste Treatment Center (at K-25 site in Oak Ridge, Tennessee), LLNL= Lawrence Livermore National Laboratory, Y-12 = Y-12 Complex at Oak Ridge, WIPP = Waste Isolation Pilot Plant.

^a The estimated number of persons residing within 0.5 miles (800 meters) along the transportation route.

^b The EnergySolutions site in Clive, Utah, is a representative commercial disposal facility.

^c Pass through Santa Fe bypass (New Mexico 599) to Interstate 25.

Note: To convert kilometers to miles, multiply by 0.6214; number per square kilometer to number per square mile, multiply by 2.59.

The affected population for route characterization and incident-free dose calculation includes all persons living within 0.5 miles (800 meters) of each side of the transportation route.

Analyzed truck routes for shipments of radioactive waste materials are shown in **Figure K–2**.

K.4.2 Radioactive Material Shipments

Transportation of all radioactive material (waste and special nuclear material) types is assumed to be in certified or certified-equivalent packaging on exclusive-use vehicles. Legal-weight heavy-haul combination trucks are used for highway transportation. Type A packages are transported on common flatbed or covered trailers; Type B packages are generally shipped on trailers designed specifically for the packaging being used. For transportation by truck, the maximum payload weight is considered to be about 48,000 pounds (about 22,000 kilograms), based on the Federal gross vehicle weight limit of 80,000 pounds (36,288 kilograms). However, there are large numbers of multitrailer combinations (known as longer combination vehicles) with gross weights in excess of the Federal limit in operation on rural roads and turnpikes in some states (DOT 2003), but for evaluation purposes, the load limit for the legal truck was based on the Federal gross vehicle weight.

Several types of packagings (containers, or casks) would be used to transport the radioactive materials. The various wastes that would be transported under the alternatives in this SWEIS include demolition and construction debris and hazardous waste, low-level radioactive waste, transuranic waste, and mixed low-level radioactive waste. **Table K–2** lists the types of containers used, along with their volumes and the number of containers in a shipment. A shipment is defined as the amount of materials transported on a single truck.

Table K–2 Radioactive Material Type and Container Characteristics

| <i>Material Type</i> | <i>Container</i> | <i>Container Volume (cubic meters)^a</i> | <i>Container Mass (kilograms)^b</i> | <i>Number of Containers per Shipment</i> |
|---|-----------------------------|--|---|--|
| Special Nuclear Material | 9975, 6M, and FL containers | 0.13 and 0.32 | 113-168 | 1 to 40 per safe and secure trailer truck |
| Class A low-level radioactive waste | 208-liter drum | 0.21 | 272 | 80 per truck |
| Low-level radioactive waste and mixed low-level radioactive waste | B-25 Box | 2.55 | 4,536 | 5 per truck |
| Low-level radioactive waste (remote-handled) ^c | 208-liter drum | 0.21 | 272 | 10 per truck cask |
| Low specific activity waste | Soft liner | 7.31 | 10,886 | 2 per truck |
| Transuranic waste (remote-handled) | 208-liter drum | 0.21 | 272 | 3 per truck cask; 1 cask per truck |
| Transuranic waste (contact-handled) | 208-liter drum | 0.21 | 272 | 14 per TRUPACT II; 3 TRUPACT IIs per truck ^d |
| Construction and demolition debris | Roll on/Roll off | 15.30 | Not applicable | 1 per truck |
| Hazardous | 208-liter drum | 0.21 | 272 | 60 to 80 per truck ^e |

^a Container exterior volume. To convert cubic meters to cubic feet, multiply by 35.315; liters to gallons, multiply by 0.26417.

^b Nominal filled container mass. Container mass includes the mass of the container shell, its internal packaging, and the materials within. To convert kilograms to pounds, multiply by 2.2046.

^c Remote-handled low-level radioactive wastes are packaged in 55-gallons (208-liter) drums and transported in Type B shipping casks.

^d Nominal number per truck. Depending on the waste density 2 or 3 TRUPACT IIs are shipped per truck. About 30 percent of transuranic wastes are considered to have high density leading to 2 TRUPACT II per truck shipments (LANL 2006).

^e Depending on the waste density, 60 to 80 drums could be shipped per truck.

Note: Construction debris and hazardous wastes would be shipped to local offsite locations.

The number of shipping containers per shipment was estimated on the basis of the dimensions and weights of the shipping containers; the Transport Index, which is the maximum dose rate at 1 meter (3.3 feet) from a container;¹ limits on special nuclear material mass per shipment; and the transport vehicle dimensions and weight limits. In general, the various wastes were assumed to be transported on standard truck semi-trailers in a single stack.

Special nuclear material is transported on DOE safe and secure transport trailers. Special nuclear material transports include uranium-233, plutonium pits, plutonium oxides and enriched uranium that are used in support of nuclear criticality safety, nuclear weapons, and the production of mixed oxide fuel, or to effect disposition. These materials are transported between LANL, Pantex, Lawrence Livermore National Laboratory, Savannah River Site, Nevada Test Site, Y-12 Complex, and Oak Ridge National Laboratory.

For the purposes of analysis, it was assumed that all low-level radioactive waste would be disposed of at LANL, a DOE site (the Nevada Test Site, in Nevada), or a commercial site (EnergySolutions, in Utah) depending on waste classification. The commercial site only accepts the low-level and mixed low-level radioactive waste known as Class A waste per 10 CFR 61.55, and provided that the waste can be contact-handled. The DOE site accepts all classes of low-level and mixed low-level radioactive waste. Mixed low-level radioactive waste could also be transported to a facility (such as East Tennessee Waste Treatment Center) for treatment and temporary storage, but eventually would have to be transported to an acceptable waste disposal site. The generated transuranic waste would be disposed of at WIPP.

K.5 Incident-Free Transportation Risks

K.5.1 Radiological Risk

During incident-free transportation of radioactive materials, radiological dose results from exposure to the external radiation field that surrounds the shipping containers. The population dose is a function of the number of people exposed, their proximity to the containers, their length of time of exposure, and the intensity of the radiation field surrounding the containers.

Radiological impacts were determined for crewmembers and the general population during incident-free transportation. For truck shipments, the crewmembers are the drivers of the shipment vehicle. The general population is composed of the persons residing within 0.5 miles (800 meters) of the truck routes (off-link), persons sharing the road (on-link), and persons at stops. Exposures to workers who would load and unload the shipments are not included in this analysis, but are included in the occupational estimates for plant workers. Exposures to the inspectors are evaluated and presented separately.

Collective doses for the crew and general population were calculated by using the RADTRAN 5 computer code (Neuhauser and Kanipe 2003). The radioactive material shipments were assigned an external dose rate based on their radiological characteristics. Offsite transportation of the radioactive material has a defined regulatory limit of 10 millirem per hour at 2 meters (6.6 feet) from the cask (10 CFR 71.47 and 49 CFR 173.441). If a waste container shows a high external dose rate that could exceed the DOT limit of 10 millirem per hour 2 meters from the outer, or

¹ Based on the Transport Index definition provided in 10 CFR 71.43 and 49 CFR 173.410.

lateral, edge of the vehicle, it would be transported in a Type A or Type B shielded shipping cask or container.

Waste container dose rate, or its Transport Index, depends on distribution and quantities of radionuclides, waste density, shielding provided by the packaging, and self-shielding provided by the waste mixture. The most important gamma emitting radionuclides in the waste are cobalt-60 and cesium-137. The MicroShield computer program (Grove 2003) was used to estimate the external dose rates for the various waste containers based on unit concentrations of cobalt-60 and cesium-137. Dose rate calculations were performed assuming both shielded and bare containers. For the shielded option, waste containers were assumed to be in appropriate Type A or Type B shipping casks. For example, remote-handled transuranic wastes were assumed to be shipped in CNS 10-160B or RH-72B casks (both are Type B casks), and remote-handled low-level radioactive waste in a CNS 10-160B cask or a CNS 14-195 (a Type A shielded cask).

Waste and nuclear materials that are expected to be transported both on site and off site are usually of low dose rate, on the order of one millirem per hour at 1 meter (3.3 feet). However, exhumation of wastes from material disposal areas (MDAs) would be expected to result in multiple waste types having various levels of radioactive inventory and dose rates. Using an enveloping waste composition for each waste type, a conservative dose rate for its container was calculated. These dose rates were compared with those used in other DOE NEPA documentations, and an appropriate conservative value was assigned to each waste type. The remote-handled and contact-handled transuranic waste package dose rates at 1 meter (3.3 feet) were assigned at 10 millirem per hour and 4 millirem per hour, respectively (DOE 1997). Dose rates for low-level radioactive waste and mixed low-level radioactive waste were assigned at 1 millirem per hour at 1 meter (3.3 feet). Dose rate for low specific activity waste was assigned at 0.10 millirem per hour at 1 meter (3.3 feet). Dose rate for the remote handled low-level radioactive wastes in Type A or Type B casks were assigned at 1 millirem per hour at 1 meter (3.3 feet). Dose rates for the special nuclear material shipments of uranium-233, plutonium, and enriched uranium are assigned at 10, 5 and 1 millirem per hour at 1 meter (3.3 feet), respectively.

To calculate the collective dose, a unit risk factor was developed to estimate the impact of transporting one shipment of radioactive material over a unit distance of travel in a given population density zone. The unit risk factors were combined with routing information, such as the shipment distances in various population density zones, to determine the risk for a single shipment (a shipment risk factor) between a given origin and destination. Unit risk factors were developed on the basis of travel on interstate highways and freeways, as required by 49 CFR Parts 171 to 177 for highway-route-controlled quantities of radioactive material within rural, suburban, and urban population zones, by using RADTRAN 5 and its default data. In addition, it was assumed that 10 percent of the time, travel through suburban and urban zones would encounter rush-hour conditions, leading to lower average speed and higher traffic density. Note that the size of the waste package and assumptions regarding public shielding afforded by the general housing structure within each zone would be major contributing factors in the calculated dose.

The radiological risks from transporting radioactive materials were estimated in terms of the number of LCFs among the crew and the exposed population. A health risk conversion factor of 0.0006 LCFs per person-rem of exposure was used for both the public and workers (DOE 2003a).

K.5.2 Nonradiological Risk

The nonradiological risks, or vehicle-related health risks, resulting from incident-free transport that may be associated with the generation of air pollutants by transport vehicles during shipment are independent of the radioactive nature of the shipment. Historically, the health endpoint assessed under incident-free transport conditions is the excess latent mortality due to inhalation of vehicle emissions. Unit risk factors for pollutant inhalation in terms of mortality have been generated (Rao et al. 1982). The unit risk factors account for the potential fatalities from emissions of particulates and sulfur dioxide, but they are applicable only to the urban population zone. The emission unit risk factor for truck transport in the urban area is estimated to be 5.0×10^{-8} fatalities per kilometer; for rail transport, it is 2.0×10^{-7} fatalities per kilometer (DOE 2002a). These risk factors were only used for estimating emission risk while the transport is in the urban area. The emergence of considerable data regarding threshold values for various chemical constituents of vehicle exhaust has made linear extrapolation to estimate the risks from truck or rail emissions untenable. This calculation has been eliminated from RADTRAN in its recent revision (Neuhauser and Kanipe 2003). Therefore, no risk factors have been assigned to the vehicle emissions in this SWEIS.

K.5.3 Maximally Exposed Individual Exposure Scenarios

The maximum individual doses for routine offsite transportation were estimated for transportation workers and for members of the general population. Three hypothetical scenarios were evaluated to determine the MEI in the general population. These scenarios are (DOE 2002a):

- A person caught in traffic and located 4 feet (1.2 meters) from the surface of the shipping container for 30 minutes;
- A resident living 98 feet (30 meters) from the highway used to transport the shipping container; and
- A service station worker at a distance of 52 feet (16 meters) from the shipping container for 50 minutes.

The hypothetical MEI doses were accumulated over a single year for all transportation shipments. However, for the scenario involving an individual caught in traffic next to a shipping container, the radiological exposures were calculated for only one event because it was considered unlikely that the same individual would be caught in traffic next to all containers for all shipments. For truck shipments, the maximally exposed transportation worker is the driver who was assumed to have been trained as a radiation worker and to drive shipments for up to 2,000 hours per year, or accumulate an exposure of 2 rem per year. The maximum exposure rate for a member of a truck crew as a nonradiation worker is 2 millirem per hour (10 CFR 71.47).

K.6 Transportation Accident Risks and Maximum Reasonably Foreseeable Consequences

K.6.1 Methodology

The offsite transportation accident analysis considers the impact of accidents during the transportation of waste. Under accident conditions, impacts on human health and the environment could result from the release and dispersal of radioactive material. Transportation accident impacts were assessed using an accident analysis methodology developed by NRC. This section provides an overview of the methodologies; detailed descriptions of various methodologies are found in the *Radioactive Material Transportation Study*, NUREG-0170, *Modal Study*, NUREG/CR-4829, and *Reexamination Study*, NUREG/CR-6672 (NRC 1977, 1987, 2000). Accidents that could potentially breach the shipping container are represented by a spectrum of accident severities and radioactive release conditions. Historically, most transportation accidents involving radioactive materials have resulted in little or no release of radioactive material from the shipping container. Consequently, the analysis of accident risks takes into account a spectrum of accidents ranging from high-probability accidents of low severity to hypothetical high-severity accidents that have a correspondingly low probability of occurrence. The accident analysis calculates the probabilities and consequences from this spectrum of accidents.

To provide DOE and the public with a reasonable assessment of radioactive waste transportation accident impacts, two types of analysis were performed. First an accident risk assessment was performed that takes into account the probabilities and consequences of a spectrum of potential accident severities using a methodology developed by the NRC (NRC 1977, 1987, 2000). For the spectrum of accidents considered in the analysis, accident consequences in terms of collective “dose risk” to the population within 50 miles (80 kilometers) were determined using the RADTRAN 5 computer program (Neuhauser et al. 2000). The RADTRAN 5 code sums the product of consequences and probability over all accident severity categories to obtain a probability-weighted risk value referred to in this appendix as “dose risk,” which is expressed in units of person-rem. Second, to represent the maximum reasonably foreseeable impacts to individuals and populations should an accident occur, maximum radiological consequences were calculated in an urban or a suburban population zone for an accidental release with a likelihood of occurrence greater than 1-in-10 million per year using the RISKIND computer program (Yuan et al. 1995).

K.6.2 Accident Rates

For the calculation of accident risks, vehicle accident and fatality rates were taken from data provided in *State-Level Accident Rates for Surface Freight Transportation: A Reexamination*, ANL/ESD/TM-150 (Saricks and Tompkins 1999). Accident rates are generically defined as the number of accident involvements (or fatalities) in a given year per unit of travel in that same year. Therefore, the rate is a fractional value, with accident involvement count as the numerator of the fraction and vehicular activity (total travel distance in truck kilometers) as the denominator. Accident rates were generally determined for a multiyear period. For assessment purposes, the total number of expected accidents or fatalities was calculated by multiplying the total shipment distance for a specific case by the appropriate accident or fatality rate.

For commercial truck transportation, the rates presented are specifically for heavy-haul combination trucks involved in interstate commerce (Saricks and Tompkins 1999). Heavy-haul combination trucks are rigs composed of a separable tractor unit containing the engine and one to three freight trailers connected to each other. Heavy-haul combination trucks are typically used for radioactive material shipments. The truck accident rates are computed for each state based on statistics compiled by the Federal Highway Administration, Office of Motor Carriers, from 1994 to 1996. A fatality caused by an accident is the death of a member of the public who is killed instantly or dies within 30 days due to the injuries sustained in the accident.

For offsite truck transportation, separate accident rates and accident fatality risks were used for rural, suburban, and urban population zones. The values selected were the “mean” accident and fatality rates given in ANL/ESD/TM-150 (Saricks and Tompkins 1999) under interstate, primary, and total categories for rural, suburban, and urban population zones, respectively. The accident rates were 3.15, 3.52, and 3.66 per 10 million truck kilometers, and the fatality rates were 0.88, 1.49, and 2.32 per 100 million truck kilometers for rural, suburban, and urban zones, respectively.

For DOE safe secure trailer truck transport, the DOE operational experience between 1984 and 1999 was used. The mean probability of an accident requiring towing of a disabled trailer truck was about 6 per 100 million kilometers (DOE 2000). The number of safe and secure trailer accidents is too small to support allocating this overall rate among the various types of routes (interstate, primary, others) used in the accident analysis. Therefore, data for the relative rate of accidents on these route types, or influence factor, provided in *Determination of Influence Factor and Accident Rates for Armored Tractor/Safe Secure Trailer* (Phillips, Clauss, and Blower 1994), were used to estimate accident frequencies for rural, urban, and suburban transports. Accident fatalities for the safe secure trailer transports were estimated using the commercial truck transport fatality per accident ratios within each zone.

For local and regional transport, New Mexico State accident and fatality rates were used. The data were provided in ANL/ESD/TM-150 (Saricks and Tompkins 1999). The rates used were 1.13 accidents per 10 million truck kilometers and 1.18 fatalities per 100 million truck kilometers.

K.6.3 Accident Severity Categories and Conditional Probabilities

Accident severity categories for potential radioactive waste transportation accidents are described in the *Radioactive Material Transportation Study* (NRC 1977) for radioactive waste in general and in the *Modal Study* (NRC 1987) and the *Reexamination Study* (NRC 2000) for spent nuclear fuel. The methods described in the *Modal Study* and the *Reexamination Study* are applicable to transportation of radioactive materials in a Type B spent fuel cask. The accident severity categories presented in the *Radioactive Material Transportation Study* would be applicable to all other waste transported offsite.

The *Radioactive Material Transportation Study* (NRC 1977) originally was used to estimate conditional probabilities associated with accidents involving transportation of radioactive materials. The *Modal Study* and the *Reexamination Study* (NRC 1987, 2000) are initiatives taken

by NRC to refine more precisely the analysis presented in *Radioactive Material Transportation Study* for spent nuclear fuel shipping casks.

Whereas the *Radioactive Material Transportation Study* (NRC 1977) analysis was primarily performed using best engineering judgments and presumptions concerning cask response, the later studies rely on sophisticated structural and thermal engineering analysis and a probabilistic assessment of the conditions that could be experienced in severe transportation accidents. The latter results are based on representative spent nuclear fuel casks assumed to have been designed, manufactured, operated, and maintained according to national codes and standards. Design parameters of the representative casks were chosen to meet the minimum test criteria specified in 10 CFR Part 71. The study is believed to provide realistic, yet conservative, results for radiological releases under transport accident conditions.

In the *Modal Study* and the *Reexamination Study*, potential accident damage to a cask is categorized according to the magnitude of the mechanical forces (impact) and thermal forces (fire) to which a cask may be subjected during an accident. Because all accidents can be described in these terms, severity is independent of the specific accident sequence. In other words, any sequence of events that results in an accident in which a cask is subjected to forces within a certain range of values is assigned to the accident severity region associated with that range. The accident severity scheme is designed to take into account all potential foreseeable transportation accidents, including accidents with low probability but high consequences, and those with high probability but low consequences.

As discussed earlier, the accident consequence assessment considers the potential impacts of severe transportation accidents. In terms of risk, the severity of an accident must be viewed in terms of potential radiological consequences, which are directly proportional to the fraction of the radioactive material within a cask that is released to the environment during the accident. Although accident severity regions span the entire range of mechanical and thermal accident loads, they are grouped into accident categories that can be characterized by a single set of release fractions and are, therefore, considered together in the accident consequence assessment. The accident category severity fraction is the sum of all conditional probabilities in that accident category.

For the accident risk assessment, accident “dose risk” was generically defined as the product of the consequences of an accident and the probability of occurrence of that accident, an approach consistent with the methodology used by RADTRAN 5 computer code. The RADTRAN 5 code sums the product of consequences and probability over all accident categories to obtain a probability-weighted risk value referred to in this appendix as “dose risk,” which is expressed in units of person-rem.

K.6.4 Atmospheric Conditions

Because it is impossible to predict the specific location of an offsite transportation accident, generic atmospheric conditions were selected for the risk and consequence assessments. On the basis of observations from National Weather Service surface meteorological stations at over 177 locations in the United States, on an annual average, neutral conditions (Pasquill Stability Classes C and D) occur 58.5 percent of the time, and stable (Pasquill Stability Classes E and G)

and unstable (Pasquill Stability Classes A and B) conditions occur 33.5 percent and 8 percent of the time, respectively (DOE 2002a). The neutral weather conditions predominate in each season, but most frequently in the winter (nearly 60 percent of the observations).

Neutral weather conditions (Pasquill Stability Class D) compose the most frequently occurring atmospheric stability condition in the United States and are thus most likely to be present in the event of an accident involving a radioactive waste shipment. Neutral weather conditions are typified by moderate windspeeds, vertical mixing within the atmosphere, and good dispersion of atmospheric contaminants. Stable weather conditions are typified by low windspeeds, very little vertical mixing within the atmosphere, and poor dispersion of atmospheric contaminants. The atmospheric condition used in RADTRAN 5 is an average weather condition that corresponds to a stability class spread between Class D (for near distance) and Class E (for farther distance).

The accident consequences for the maximum reasonably foreseeable accident (an accident with likelihood of occurrence greater than 1 in 10 million per year) were assessed under both stable (Class F with a windspeed of 1 meter per second [2.2 miles per hour]) and neutral (Class D with a windspeed of 4 meters per second [8.8 miles per hour]) atmospheric conditions. These calculations provide an estimate of the potential dose to an individual and a population within a zone, respectively. The individual dose would represent the MEI in an accident under worst-case weather conditions (stable condition, with minimum diffusion and dilution). The population dose would represent an accident under average weather conditions.

K.6.5 Radioactive Release Characteristics

Radiological consequences were calculated by assigning radionuclide release fractions on the basis of the type of waste, the type of shipping container, and the accident severity category. The release fraction is defined as the fraction of the radioactivity in the container that could be released to the atmosphere in a given severity of accident. Release fractions vary according to material type and the physical or chemical properties of the radioisotopes. Most solid radionuclides are nonvolatile and are, therefore, relatively nondispersible.

Representative release fractions were developed for each waste and container type on the basis of DOE and NRC reports (DOE 1994, 2002b, 2003a; NRC 1977, 2000). The severity categories and corresponding release fractions provided in the NRC documents cover a range of accidents from no impact (zero speed) to impacts with speed in excess of 120 miles (193 kilometers) per hour onto an unyielding surface. Traffic accidents that could occur at the LANL site would be of minor impact due to lower local speed, with no release potential.

For radioactive materials transported in a Type B cask, the particulate release fractions were developed consistent with the models in the *Reexamination Study* (NRC 2000) and adapted in the *West Valley Demonstration Project Waste Management Environmental Impact Statement* (DOE 2003b). For materials transported in Type A containers (such as 55-gallon [208-liter] drums, boxes, and soft liners), the fractions of radioactive material released from the shipping container were based on recommended values from *Radioactive Material Transportation Study* and *DOE Handbook on Airborne Release and Respirable Fractions* (NRC 1977, DOE 1994). For contact-handled and remote-handled transuranic waste, the release fractions corresponding to

the *Radioactive Material Transportation Study* severity categories (NRC 1977) and adapted in the *WIPP Supplemental Environmental Impact Statement* were used (DOE 1997, 2002b).

K.6.6 Acts of Sabotage or Terrorism

In the aftermath of the tragic events of September 11, 2001, DOE is continuing to assess measures to minimize the risk or potential consequences of radiological sabotage. While it is not possible to determine terrorists' motives and targets with certainty, DOE considers the threat of terrorist attacks to be real, and makes all efforts to reduce any vulnerability to this threat. DOE considers, evaluates, and plans for potential terrorist attacks during transportation and storage of special nuclear materials such as plutonium and enriched uranium. These materials would be transported using DOE's safe and secure transport equipment escorted by protective force personnel. DOE has a proven record of protecting these assets; no diversion of any DOE nuclear material has occurred. The details of any postulated terrorist attack, as well as DOE's plans for the security of its facilities and terrorist countermeasures are classified. A classified appendix has been prepared for this SWEIS that includes impact analyses for intentional acts of destruction related to transportation.

Additionally, DOE has evaluated the impacts of acts of sabotage and terrorism on transportation of spent nuclear fuel and high-level radioactive waste shipments (DOE 1996, 2002a). The spectrum of events considered ranges from direct attack on the shipping cask from afar to hijacking and exploding the cask in an urban area. Both of these actions would result in damaging the cask and its contents and releasing radioactive materials. The fraction of the materials released is dependent on the nature of the attack (type of explosive or weapon used). The sabotage event evaluated in the *Final Environmental Impact Statement for a Geologic Repository for the Disposal of Spent Nuclear Fuel and High-Level Radioactive Waste at Yucca Mountain, Nye County, Nevada (Yucca Mountain EIS)* was considered as an enveloping analysis for most transportation activities in this LANL SWEIS. The event was assumed to involve either a truck-sized, or a rail-sized cask containing light water reactor spent nuclear fuel. The consequences of such an act were calculated to result in an MEI dose (at 140 meters [460 feet]) of 40 to 110 rems for events involving a rail-sized or truck-sized cask, respectively. These events would lead to an increase in risk of fatal cancer to the MEI by 2 to 7 percent (DOE 2002a). The quantity of radioactive materials transported under all LANL SWEIS alternatives and the associated transuranic radionuclide source term would be less than that considered in this analysis. Therefore, estimates of risk in the *Yucca Mountain EIS* envelope the risks from an act of sabotage or terrorism involving the radioactive waste transported under all alternatives in this LANL SWEIS.

K.7 Risk Analysis Results

Per-shipment risk factors have been calculated for the collective populations of exposed persons and for the crew for all anticipated routes and shipment configurations. Radiological risks are presented in doses per-shipment for each unique route, material, and container combination. Radiological risk factors per-shipment for incident-free transportation and accident conditions for the offsite disposal locations are presented in **Table K-3**. **Table K-4** presents the radiological risk factors per-shipments for travel on two route segments between LANL and Santa Fe. This analysis was performed to be consistent with those evaluated in the *1999 SWEIS* (DOE 1999a).

Table K-3 Risk Factors per Truck Shipment of Radioactive Material

| Waste Materials | Transport Origin or Destination | Incident-Free | | | | Accident | |
|-------------------------------|---------------------------------|------------------------|-----------------------|------------------------------|-----------------------|-------------------------|--|
| | | Crew Dose (person-rem) | Crew Risk (LCF) | Population Dose (person rem) | Population Risk (LCF) | Radiological Risk (LCF) | Non-radiological Risk (traffic fatalities) |
| LLW (B) ^a | Nevada Test Site | 0.0124 | 7.46×10^{-6} | 0.00392 | 2.35×10^{-6} | 1.67×10^{-8} | 0.0000249 |
| LLW (D) ^b | | 0.0149 | 8.97×10^{-6} | 0.00664 | 3.99×10^{-6} | 2.18×10^{-8} | 0.0000249 |
| High activity ^c | | 0.0124 | 7.46×10^{-6} | 0.00392 | 2.35×10^{-6} | 1.67×10^{-8} | 0.0000249 |
| LLW (RH) ^d | | 0.0108 | 6.49×10^{-6} | 0.00203 | 1.22×10^{-6} | 3.28×10^{-13} | 0.0000249 |
| DD&D bulk ^e | | 0.00137 | 8.21×10^{-7} | 0.000274 | 1.64×10^{-7} | 1.80×10^{-10} | 0.0000249 |
| LSA | | 0.00137 | 8.21×10^{-7} | 0.000274 | 1.64×10^{-7} | 1.30×10^{-8} | 0.0000249 |
| LSA | Commercial ^f | 0.00118 | 7.06×10^{-7} | 0.000234 | 1.40×10^{-7} | 9.63×10^{-9} | 0.0000211 |
| DD&D bulk ^e | | 0.00118 | 7.06×10^{-7} | 0.000234 | 1.40×10^{-7} | 1.34×10^{-10} | 0.0000211 |
| LLW (B) ^a | | 0.0107 | 6.41×10^{-6} | 0.00334 | 2.01×10^{-6} | 1.41×10^{-8} | 0.0000211 |
| LLW (D) ^b | | 0.0129 | 7.71×10^{-6} | 0.00567 | 3.40×10^{-6} | 1.84×10^{-8} | 0.0000211 |
| CH-TRU | WIPP | 0.0228 | 0.0000137 | 0.00725 | 4.35×10^{-6} | 3.30×10^{-11} | 0.0000143 |
| RH-TRU | | 0.0346 | 0.0000208 | 0.00919 | 5.51×10^{-6} | 7.66×10^{-13} | 0.0000143 |
| SNM | Pantex | 0.00637 | 3.82×10^{-6} | 0.00726 | 4.36×10^{-6} | 9.23×10^{-11} | 1.73×10^{-6} |
| SNM | LLNL | 0.00349 | 2.09×10^{-6} | 0.00396 | 2.37×10^{-6} | 3.56×10^{-10} | 4.83×10^{-6} |
| SNM | Y-12 | 0.00459 | 2.75×10^{-6} | 0.00529 | 3.18×10^{-6} | 1.01×10^{-15} | 6.94×10^{-6} |
| SNM | SRS | 0.0260 | 1.56×10^{-5} | 0.0302 | 1.81×10^{-5} | 8.89×10^{-10} | 8.08×10^{-6} |
| SNM | NTS | 0.00240 | 1.44×10^{-6} | 0.00281 | 1.68×10^{-6} | 2.76×10^{-10} | 3.50×10^{-6} |
| PuO ₂ ^g | SRS | 0.00785 | 4.71×10^{-6} | 0.00804 | 4.82×10^{-6} | 4.35×10^{-8} | 8.08×10^{-6} |
| PuO ₂ ^h | SRS | 0.0393 | 0.0000236 | 0.0270 | 0.0000162 | 9.25×10^{-8} | 8.08×10^{-6} |
| U-233 ^{i,j} | ORNL | 0.0516 | 0.000031 | 0.0705 | 0.000042 | 1.25×10^{-9} | 6.94×10^{-6} |
| U-233 ⁱ | NTS | 0.0435 | 0.000026 | 0.0371 | 0.000022 | 4.91×10^{-10} | 3.50×10^{-6} |
| U-233R ^k | WIPP | 0.0346 | 0.0000208 | 0.00919 | 5.51×10^{-6} | 1.61×10^{-11} | 0.0000143 |

LCF = latent cancer fatality, LLW = low-level radioactive waste, RH = remote-handled, DD&D = decontamination, decommissioning, and demolition, LSA = low specific activity waste, CH = contact-handled, TRU = transuranic waste, WIPP = Waste Isolation Pilot Plant, LLNL = Lawrence Livermore National Laboratory, NTS = Nevada Test Site, Y-12 = Y-12 Complex in Oak Ridge, SNM = special nuclear material, PuO₂ = plutonium dioxide, SRS = Savannah River Site, U-233 = uranium-233.

^a Low-level radioactive waste transported in Type A B-25 boxes.

^b Low-level radioactive waste transported in 55-gallon (208-liter) drums.

^c High activity low-level radioactive waste containing more than 10 nanocuries per gram of transuranic waste transported in Type A, B-25 boxes. This waste is comparable to Class B or Class C of 10 CFR Part 61 waste classification.

^d Remote-handled low-level radioactive waste transported in 55-gallon (208-liter) drums.

^e Decommissioning and demolition bulk managed waste, with a radioactive inventory of equivalent 0.0001 curies of plutonium-239 per cubic yard.

^f Commercial site is in Utah.

^g Polished plutonium oxide (very low decay impurities).

^h Unpolished plutonium oxide (high concentration of decay impurities).

ⁱ Uranium-233 oxide and metal suitable for the support of criticality experiment programs with very low uranium-232 impurities.

^j Uranium-233 oxide that is currently at LANL and is considered surplus material to be shipped to ORNL for processing for disposal.

^k Uranium-233 oxide residue that is contaminated with plutonium and to be disposed as RH-TRU waste at WIPP.

Table K-4 Risk Factors per Truck-Shipment of Radioactive Material at Nearby Routes

| Waste Materials | Transport Route Segment | Incident-Free | | | | Accident | |
|-------------------------------|-----------------------------------|------------------------|-----------------------|------------------------------|-----------------------|-------------------------|--|
| | | Crew Dose (person-rem) | Crew Risk (LCF) | Population Dose (person rem) | Population Risk (LCF) | Radiological Risk (LCF) | Non-radiological Risk (traffic fatalities) |
| LLW (B) ^a | LANL to Pojoaque | 0.000309 | 1.85×10^{-7} | 0.0000938 | 5.63×10^{-8} | 3.95×10^{-10} | 7.34×10^{-7} |
| LLW (D) ^b | | 0.000371 | 2.23×10^{-7} | 0.000159 | 9.55×10^{-8} | 5.16×10^{-10} | 7.34×10^{-7} |
| High activity ^c | | 0.000309 | 1.85×10^{-7} | 0.0000938 | 5.63×10^{-8} | 3.95×10^{-10} | 7.34×10^{-7} |
| LLW (RH) ^d | | 0.000269 | 1.61×10^{-7} | 0.0000486 | 2.92×10^{-8} | 4.84×10^{-15} | 7.34×10^{-7} |
| DD&D bulk ^e | | 0.0000340 | 2.04×10^{-8} | 6.56×10^{-6} | 3.94×10^{-9} | 2.66×10^{-12} | 7.34×10^{-7} |
| LSA | | 0.0000340 | 2.04×10^{-8} | 6.56×10^{-6} | 3.94×10^{-9} | 1.92×10^{-10} | 7.34×10^{-7} |
| CH-TRU | | 0.00118 | 7.08×10^{-7} | 0.000384 | 2.30×10^{-7} | 4.25×10^{-12} | 7.34×10^{-7} |
| RH-TRU | | 0.00179 | 1.08×10^{-6} | 0.000486 | 2.92×10^{-7} | 9.87×10^{-14} | 7.34×10^{-7} |
| SNM ^f | | 0.000298 | 1.79×10^{-7} | 0.000336 | 2.02×10^{-7} | 5.92×10^{-12} | 8.33×10^{-8} |
| PuO ₂ ^g | | 0.000090 | 5.40×10^{-8} | 0.000090 | 5.4×10^{-8} | 2.89×10^{-10} | 8.33×10^{-8} |
| PuO ₂ ^h | | 0.00045 | 2.70×10^{-7} | 0.00030 | 1.80×10^{-7} | 6.16×10^{-10} | 8.33×10^{-8} |
| U-233 | | 0.00067 | 4.02×10^{-7} | 0.000889 | 5.33×10^{-7} | 1.05×10^{-11} | 8.33×10^{-8} |
| LLW (B) ^a | Pojoaque to Santa Fe ⁱ | 0.000517 | 3.10×10^{-7} | 0.000154 | 9.22×10^{-8} | 6.31×10^{-10} | 1.23×10^{-6} |
| LLW (D) ^b | | 0.000622 | 3.73×10^{-7} | 0.000261 | 1.56×10^{-7} | 8.25×10^{-10} | 1.23×10^{-6} |
| High activity ^c | | 0.000517 | 3.10×10^{-7} | 0.000154 | 9.22×10^{-8} | 6.31×10^{-10} | 1.23×10^{-6} |
| LLW (RH) ^d | | 0.000450 | 2.70×10^{-7} | 0.0000797 | 4.78×10^{-8} | 5.62×10^{-15} | 1.23×10^{-6} |
| DD&D bulk ^e | | 0.0000569 | 3.42×10^{-8} | 0.0000108 | 6.45×10^{-9} | 3.09×10^{-12} | 1.23×10^{-6} |
| LSA | | 0.0000569 | 3.42×10^{-8} | 0.0000108 | 6.45×10^{-9} | 2.23×10^{-10} | 1.23×10^{-6} |
| CH-TRU | | 0.00198 | 1.19×10^{-6} | 0.000629 | 3.77×10^{-7} | 4.94×10^{-12} | 1.23×10^{-6} |
| RH-TRU | | 0.00300 | 1.80×10^{-6} | 0.000797 | 4.78×10^{-7} | 1.15×10^{-13} | 1.23×10^{-6} |
| SNM ^f | | 0.000500 | 3.00×10^{-7} | 0.000552 | 3.31×10^{-7} | 1.45×10^{-11} | 1.40×10^{-7} |
| PuO ₂ ^g | | 0.000151 | 9.05×10^{-8} | 0.000138 | 8.28×10^{-8} | 8.49×10^{-10} | 1.40×10^{-7} |
| PuO ₂ ^h | | 0.000754 | 4.53×10^{-7} | 0.000493 | 2.96×10^{-7} | 1.81×10^{-9} | 1.40×10^{-7} |
| U-233 | | 0.00112 | 6.74×10^{-7} | 0.00146 | 8.73×10^{-7} | 3.10×10^{-11} | 1.40×10^{-7} |

LCF = latent cancer fatality, LLW = low-level radioactive waste, RH = remote-handled, DD&D = decontamination, decommissioning, and demolition, LSA = low specific activity waste, CH = contact-handled, TRU = transuranic waste, SNM = special nuclear material, PuO₂ = plutonium dioxide, U-233 = uranium-233.

^a Low-level radioactive waste transported in Type A B-25 boxes.

^b Low-level radioactive waste transported in 55-gallon (208-liter) drums.

^c High activity low-level radioactive waste containing more than 10 nanocuries per gram of transuranic waste transported in Type A, B-25 boxes. This waste is comparable to Class B or Class C of 10 CFR Part 61 waste classification.

^d Remote-handled low-level radioactive waste transported in 55-gallon (208-liter) drums.

^e Decommissioning and demolition bulk managed waste, with a radioactive inventory of equivalent 0.0001 curies of plutonium-239 per cubic yard.

^f Calculations are based on the shipment transport index of 5. Transport indices for SNM shipments are 1 and 5, as explained in Section K.5.1.

^g Polished plutonium oxide (very low decay impurities).

^h Unpolished plutonium oxide (high concentration of decay impurities).

ⁱ Shipments pass through the Santa Fe bypass (New Mexico 599) to Interstate 25.

All radioactive material transports would pass through the LANL to Pojoaque route segment, and those that would be destined for the Nevada Test Site, WIPP, Savannah River Site, and Pantex would pass through the second segment; that is, Pojoaque to Santa Fe. Therefore, the populations in these route segments would receive the maximum impacts.

In these tables, for incident-free transportation, both dose and LCF risk factors are provided for the crew and exposed population. The radiological risks would result from potential exposure of people to external radiation emanating from the packaged radioactive materials. The exposed population includes the off-link public (people living along the route), on-link public (pedestrian and car occupants along the route) and public at rest and fuel stops. Doses are calculated for the crew and public (people living along the route, pedestrians and drivers along the route, and the public at rest and fueling stops). For onsite shipments, the stop dose (doses to the public at rest and refueling stops) is set at zero, because a truck is not expected to stop during a shipment that takes less than an hour. For transportation accidents, the risk factors are given for both the radiological, in terms of potential LCF in the exposed population, and the nonradiological, in terms of number of traffic fatalities. The LCF represents the number of additional latent fatal cancers among the exposed population.

Both the radiological dose risk factor and the nonradiological risk factor for transportation accidents are presented in Tables K-3 and K-4. The radiological and nonradiological accident risk factors are provided in terms of potential fatalities per shipment. The radiological risks are in terms of LCFs. For the population, the radiological risks were calculated by multiplying the accident dose risks by the health risk factor of 6×10^{-4} latent cancer fatalities per person-rem of exposure. The nonradiological risk factors are nonoccupational traffic fatalities resulting from transportation accidents.

As stated earlier (see Section K.6.3), the accident dose is called “dose risk” because the values incorporate the spectrum of accident severity probabilities and associated consequences (such as dose). The accident dose risks are very low because accident severity probabilities (the likelihood of accidents leading to confinement breach of a package or shipping cask and release of its contents) are small, and the content and form of the wastes (solid dirt-like contamination) are such that would lead to nondispersible and mostly noncombustible release. Although persons reside in a 50-mile (80-kilometer) radius along the transportation route, they are generally quite far from the route. Because RADTRAN 5 uses an assumption of homogeneous population, it would greatly overestimate the actual doses.

At LANL, radioactive materials are transported both on site, between the Technical Areas (TAs), and off site to multiple locations. Onsite transport constitutes the majority of activities that are part of routine operations in support of various programs. The radioactive materials transported onsite between TAs are mainly of limited quantities, short travel distances, and frequently on closed roads. The impacts of these activities are part of the normal operations at these areas. For example, worker dose from handling and transporting the radioactive materials are included as part of operational activities. Specific analyses performed in the 1999 SWEIS (DOE 1999a) indicated that the projected collective radiation dose for LANL drivers from a projected 10,750 onsite shipments to be 10.3 person-rem per year, or on the average, less than one millirem per transport. Review of the onsite radioactive materials transportation within the last 4 years

indicates a much smaller number of shipments than those projected in the *1999 SWEIS*. Therefore, the *1999 SWEIS* projection of impacts would envelop the impacts for the routine onsite transportation. The nonroutine onsite transport activities, such as waste transport from facility decommissioning and demolition or from MDA remediation, were evaluated and presented in the *SWEIS* where applicable.

Offsite transports would occur using both trucks and air freight. Materials transported by air freight would be similar in number, type, and forms as those considered in the *1999 SWEIS*, and would hence result in similar impacts. The aircrew dose from air freight radioactive transport was estimated at 2.4 person-rem per year (DOE 1999a). Therefore, only truck (both commercial and DOE safe secure trailer) transport is analyzed here. The *1999 SWEIS* provides a comprehensive listing of various radioactive material types, forms, origin-destination, quantities and the projected number of shipments. The radioactive materials transported included tritium, plutonium, uranium (both depleted and enriched), offsite source recovery project sealed sources, medical isotopes, small quantities of activation products, low-level radioactive waste, and transuranic waste. The specific origins-destinations, except for Rocky Flats, are expected to be applicable for future transports. For analysis purposes in this *SWEIS*, the focus was on those origins-destinations that would have the greatest effect, including Pantex and Savannah River Site (for plutonium transports) and waste disposal sites (such as the Nevada Test Site, a commercial site in Utah, and WIPP). Transports of other radioactive materials would remain similar to those projected in the *1999 SWEIS*.

Table K-5 provides the estimated number of shipments for various materials under each alternative. In addition, this table provides the estimated number of shipments from activities associated with the MDA removal and capping options and those resulting from increase in pit production from 20 to 80 pits per year. The waste shipments under the No Action Alternative include those expected to be generated during LANL operations over the next 10 years (between 2007 and 2016), baseline remediation of MDAs, and transport of transuranic wastes currently stored above ground. The shipments under the Expanded Operations Alternative include operational wastes, the TA-18 and TA-21 decommissioning and demolition wastes, demolition and refurbishment wastes from implementation of selected project-specific actions as detailed in Appendices G and H, and a range of generated wastes from remediation options on MDAs as detailed in Appendix I. The MDA remediation options include capping and remediation, and removal and remediation of various MDAs and other potential release sites under the Consent Order. The shipments under the Reduced Operations Alternative include generated wastes from LANL operations, the TA-18 decommissioning and demolition activities, and baseline remediation of MDA activities. For the remediation options for MDAs, see Appendix I. In addition, Table K-5 provides the required number of shipments of special nuclear material in support of pit production and Advanced Recovery and Integrated Extraction System, uranium-233 for the criticality safety program, and polished plutonium oxides for the mixed oxide fabrication program under each alternative, as applicable.

LANL currently possess about 16.5 pounds (7.5 kilograms) of uranium-233 metal and oxides. The impacts of shipping about 9.9 to 11 pounds (4.5 to 5 kilograms) of these materials to Oak Ridge National Laboratory for processing and disposition are evaluated in the LANL *SWEIS*. Further investigation of the uranium-233 needs has identified that 6.2 pounds (2.8 kilograms) are considered surplus, of which 0.5 pounds (240 grams) may not meet

acceptance requirements at Oak Ridge National Laboratory. The revised requirement reduces the number of uranium-233 shipments to Oak Ridge, and therefore the current analysis encompasses the impacts of the proposal to transport a lesser quantity.

Table K-5 Estimates of the Number of Radioactive Shipments Under Each Alternative and Selected Activities

| Alternative (Activities) | Number of Shipments | | | | | | | | | | |
|--|-----------------------|--------------|-------------------------|-------------------------------|-------------------------|---------------|------------------|-------|------------------|-----------------|---------------------|
| | Radioactive Materials | | | | | | | | | Miscellaneous | |
| | LSA | DD&D Bulk | LLW (B) ^a | High Activity ^b | LLW- RH ^c | Mixed LLW | TRU ^d | SNM | PuO ₂ | Hazardous | Others ^e |
| No Action | 624 | 812 | 9,217 | 312 | 0 | 196 | 1,460 | 958 | 20 | 946 | 10,778 |
| Reduced Operations | 624 | 812 | 7,883 | 312 | 0 | 196 | 1,460 | 958 | 20 | 932 | 10,778 |
| Expanded Operations ^f | 1,436- 49,940 | 9,538 | 9,919 | 3,418- 36,521 | 196- 856 | 297- 9,019 | 2,405- 5,044 | 1,558 | 50 | 2,781- 4,749 | 35,419- 41,506 |
| Expanded Operations (without MDA Remediation) ^g | 681 | 9,538 | 9,919 | 3,418 | 196 | 240 | 2,397 | 1,558 | 50 | 1,000 | 31,856 |
| (MDA Remediation) ^h | 755- 49,259 | 0 | 0 | 0- 33,103 | 0- 660 | 57- 8,779 | 8- 2,647 | 0 | 0 | 1,781- 3,749 | 3,563- 9,650 |
| (Increase in Pit Production) ⁱ | 0 | 0 | 701 | 0 | 0 | 6 | 246 | 600 | 0 | 0 | 0 |

LSA = low specific activity, DD&D = decontamination, decommissioning, and demolition, LLW = low-level radioactive waste, RH = remote handled, TRU = transuranic waste, SNM = special nuclear material, PuO₂ = plutonium dioxide.

^a Low-level radioactive waste transported in drums or Type A, B-25 boxes. The values here also include shipments of evaporator bottoms from Radioactive Liquid Waste Treatment Facility to an offsite location and the returned dried wastes.

^b High activity low-level radioactive waste containing more than 10 nanocuries per gram of transuranic waste transported in Type A, B-25 boxes. This waste is comparable to Class B or Class C of 10 CFR Part 61 waste classification. This waste is generated during MDA waste retrieval, and from decontamination and demolishing of some of the buildings. The shipments also include one shipment of strontium-90 radioisotope thermoelectric generators under all alternatives.

^c Remote-handled low-level radioactive waste transported in 55-gallon (208-liter) drums.

^d The sum of remote-handled and contact-handled transuranic waste shipments.

^e Others include industrial, sanitary, and asbestos wastes.

^f The range of values represent the estimated number of shipments for options of capping and remediation and removal and remediation of all MDAs.

^g Expanded Operations Alternative with baseline MDA remediation (without capping or removal).

^h The range values represent the estimated number of shipments for options of capping and removal of all MDAs.

ⁱ The waste shipment values presented are based on the differences between the No Action and the Expanded Operation Alternatives' projected waste volumes for routine operation.

In order to provide flexibility for potential disposition of all surplus uranium-233 at WIPP, per shipment and total transportation impacts for shipment of 6.2 pounds (2.8 kilograms) uranium-233 to WIPP is provided in this appendix. The surplus materials are assumed to be packaged in pipe overpack containers and shipped as remote-handled transuranic waste. Pipe overpack containers could be transported in either of two certified casks; 10 drums per cask could be transported in the CNS10-160 B or 3 drums per cask could be transported in the RH-72B. For purposes of analysis, it was assumed that the RH-72B cask, which results in a higher number of shipments, would be used. The per-shipment doses and risks to the transport crew and the population are provided in Table K-3. Use of RH-72B cask would require a total of 63 shipments. Therefore, the total dose to the crew and population would be 2.18 and 0.58 person-rem, respectively. This is small fraction of the total dose under any one of the alternatives analyzed.

Table K–6 shows the risks of transporting radioactive materials under each alternative, and for the MDA remediation options and the increased pit production activities. The risks are calculated by multiplying the previously given per-shipment factors by the number of shipments over the duration of the program and, for radiological doses, by the health risk conversion factors. The risks are for the total offsite transport of the radioactive materials between 2007 and 2016. The risks to the individuals and population from transport of radioactive materials beyond 2016 would be slightly greater than those provided under the No Action Alternative.

Table K–6 Ten-Year Risks of Transporting Radioactive Materials Under Each Alternative and Selected Activities

| Transport Segments | Offsite Disposal Option ^a | Number of Shipments | Round Trip Kilometers Traveled (million) | Incident-Free | | | | Accident | |
|--|--------------------------------------|---------------------|--|-------------------|-------------------|-------------------|-------------------|--------------------------------|-----------------------------------|
| | | | | Crew | | Population | | Radiological Risk ^b | Nonradiological Risk ^b |
| | | | | Dose (person-rem) | Risk ^b | Dose (person-rem) | Risk ^b | | |
| No Action | | | | | | | | | |
| LANL to Pojoaque | NTS | 13,599 | 0.85 | 5.04 | 0.00303 | 1.81 | 0.00109 | 3.9×10 ⁻⁶ | 0.0093 |
| Pojoaque to Santa Fe | | 13,599 | 1.15 | 8.77 | 0.00526 | 3.29 | 0.00198 | 7.1×10 ⁻⁶ | 0.0164 |
| Total | | 13,599 | 31.88 | 163.75 | 0.09825 | 58.37 | 0.03502 | 0.00017 | 0.3041 |
| LANL to Pojoaque | Commercial | 13,599 | 0.85 | 5.04 | 0.00303 | 1.81 | 0.00109 | 3.9×10 ⁻⁶ | 0.0093 |
| Pojoaque to Santa Fe | | 2,893 ^c | 0.30 | 3.89 | 0.00233 | 1.85 | 0.00111 | 1.1×10 ⁻⁶ | 0.0032 |
| Total | | 13,599 | 28.16 | 147.30 | 0.08838 | 52.99 | 0.03179 | 0.00014 | 0.263 |
| Reduced Operations | | | | | | | | | |
| LANL to Pojoaque | NTS | 12,265 | 0.76 | 4.63 | 0.00278 | 1.69 | 0.00101 | 3.4×10 ⁻⁶ | 0.0088 |
| Pojoaque to Santa Fe | | 12,265 | 1.05 | 8.08 | 0.00485 | 3.09 | 0.00185 | 6.2×10 ⁻⁶ | 0.0147 |
| Total | | 12,265 | 28.54 | 147.17 | 0.08830 | 53.14 | 0.03188 | 0.00015 | 0.271 |
| LANL to Pojoaque | Commercial | 12,265 | 0.76 | 4.63 | 0.00278 | 1.69 | 0.00101 | 3.4×10 ⁻⁶ | 0.0088 |
| Pojoaque to Santa Fe | | 2,893 ^c | 0.30 | 3.89 | 0.00233 | 1.85 | 0.00111 | 1.1×10 ⁻⁶ | 0.0032 |
| Total | | 12,265 | 25.28 | 133.05 | 0.07983 | 48.53 | 0.02912 | 0.00013 | 0.235 |
| Expanded Operations (with MDA Removal Option) | | | | | | | | | |
| LANL to Pojoaque | NTS | 122,445 | 7.62 | 25.94 | 0.01556 | 8.14 | 0.00488 | 0.000032 | 0.089 |
| Pojoaque to Santa Fe | | 122,445 | 9.70 | 43.46 | 0.02608 | 13.31 | 0.00799 | 0.000047 | 0.149 |
| Total | | 122,445 | 299.94 | 910.31 | 0.54619 | 286.77 | 0.17206 | 0.0016 | 2.96 |
| LANL to Pojoaque | Commercial | 122,445 | 7.62 | 25.94 | 0.01556 | 8.14 | 0.00488 | 0.000032 | 0.089 |
| Pojoaque to Santa Fe | | 44,205 ^c | 3.52 | 30.37 | 0.01822 | 9.79 | 0.00587 | 0.000024 | 0.0532 |
| Total | | 122,445 | 272.76 | 866.16 | 0.51970 | 273.62 | 0.16417 | 0.0014 | 2.67 |
| Expanded Operations (with MDA Capping Option) | | | | | | | | | |
| LANL to Pojoaque | NTS | 28,817 | 1.79 | 8.04 | 0.00482 | 2.84 | 0.00171 | 5.7×10 ⁻⁶ | 0.0205 |
| Pojoaque to Santa Fe | | 28,817 | 2.31 | 13.47 | 0.00808 | 4.64 | 0.00278 | 9.8×10 ⁻⁶ | 0.0343 |
| Total | | 28,817 | 69.28 | 255.88 | 0.15353 | 89.07 | 0.05344 | 0.00025 | 0.660 |
| LANL to Pojoaque | Commercial | 28,817 | 1.79 | 8.04 | 0.00482 | 2.84 | 0.00171 | 5.7×10 ⁻⁶ | 0.0205 |
| Pojoaque to Santa Fe | | 7,803 ^c | 0.65 | 7.65 | 0.00459 | 2.98 | 0.00179 | 3.1×10 ⁻⁶ | 0.0085 |
| Total | | 28,817 | 61.98 | 236.26 | 0.14175 | 82.86 | 0.04972 | 0.00022 | 0.580 |

| Transport Segments | Offsite Disposal Option ^a | Number of Shipments | Round Trip Kilometers Traveled (million) | Incident-Free | | | | Accident | |
|---|--------------------------------------|---------------------|--|-------------------|-------------------|-------------------|-------------------|--------------------------------|-----------------------------------|
| | | | | Crew | | Population | | Radiological Risk ^b | Nonradiological Risk ^b |
| | | | | Dose (person-rem) | Risk ^b | Dose (person-rem) | Risk ^b | | |
| Expanded Operations (without MDA Removal or Capping Options) | | | | | | | | | |
| LANL to Pojoaque | NTS | 27,997 | 1.74 | 7.98 | 0.00479 | 2.83 | 0.00170 | 5.5×10 ⁻⁶ | 0.0199 |
| Pojoaque to Santa Fe | | 27,997 | 2.24 | 13.38 | 0.00803 | 4.62 | 0.00277 | 9.6×10 ⁻⁶ | 0.0333 |
| Total | | 27,997 | 67.24 | 253.96 | 0.15237 | 88.58 | 0.05315 | 0.00024 | 0.640 |
| LANL to Pojoaque | Commercial | 27,997 | 1.74 | 7.98 | 0.00479 | 2.83 | 0.00170 | 5.5×10 ⁻⁶ | 0.0199 |
| Pojoaque to Santa Fe | | 7,795 ^c | 0.64 | 7.63 | 0.00458 | 2.97 | 0.00178 | 3.1×10 ⁻⁶ | 0.0085 |
| Total | | 27,997 | 60.22 | 234.58 | 0.14075 | 82.44 | 0.04946 | 0.00021 | 0.563 |
| MDA Removal Option Activities | | | | | | | | | |
| LANL to Pojoaque | NTS | 94,448 | 5.87 | 17.95 | 0.01077 | 5.31 | 0.00319 | 0.000026 | 0.069 |
| Pojoaque to Santa Fe | | 94,448 | 7.46 | 30.08 | 0.01805 | 8.70 | 0.00522 | 0.000037 | 0.088 |
| Total | | 94,448 | 232.70 | 656.35 | 0.39381 | 198.19 | 0.11892 | 0.0013 | 2.320 |
| LANL to Pojoaque | Commercial | 94,448 | 5.87 | 17.95 | 0.01077 | 5.31 | 0.00319 | 0.000026 | 0.069 |
| Pojoaque to Santa Fe | | 36,410 ^c | 2.88 | 22.73 | 0.01364 | 6.82 | 0.00409 | 0.000021 | 0.034 |
| Total | | 94,448 | 212.54 | 631.58 | 0.37895 | 191.18 | 0.11471 | 0.0012 | 2.100 |
| MDA Capping Option Activities | | | | | | | | | |
| LANL to Pojoaque | NTS | 820 | 0.05 | 0.05 | 0.00003 | 0.01 | 0.00001 | 1.7×10 ⁻⁷ | 0.0006 |
| Pojoaque to Santa Fe | | 820 | 0.06 | 0.09 | 0.00005 | 0.02 | 0.00001 | 2.0×10 ⁻⁷ | 0.00076 |
| Total | | 820 | 2.04 | 1.92 | 0.00115 | 0.49 | 0.00029 | 0.00001 | 0.0203 |
| LANL to Pojoaque | Commercial | 820 | 0.05 | 0.05 | 0.00003 | 0.01 | 0.00001 | 1.7×10 ⁻⁷ | 0.00060 |
| Pojoaque to Santa Fe | | 8 ^c | 0.0006 | 0.02 | 0.00001 | 0.005 | 0.000003 | 3.9×10 ⁻¹¹ | 0.00001 |
| Total | | 820 | 1.76 | 1.68 | 0.00101 | 0.42 | 0.00025 | 0.000008 | 0.0172 |
| Increase in Pit Production Activities | | | | | | | | | |
| LANL to Pojoaque | NTS | 1,553 | 0.097 | 0.68 | 0.00041 | 0.36 | 0.00022 | 2.7×10 ⁻⁷ | 0.00075 |
| Pojoaque to Santa Fe | | 1,553 | 0.15 | 1.14 | 0.00068 | 0.59 | 0.00035 | 1.9×10 ⁻⁶ | 0.00125 |
| Total | | 1,553 | 3.63 | 18.0 | 0.01083 | 8.95 | 0.00537 | 0.000011 | 0.0239 |
| LANL to Pojoaque | Commercial | 1,553 | 0.097 | 0.68 | 0.00041 | 0.36 | 0.00022 | 2.7×10 ⁻⁷ | 0.00075 |
| Pojoaque to Santa Fe | | 879 ^c | 0.08 | 0.79 | 0.00047 | 0.49 | 0.00029 | 1.4×10 ⁻⁶ | 0.00043 |
| Total | | 1,553 | 3.39 | 16.87 | 0.01012 | 8.56 | 0.00514 | 9.6×10 ⁻⁶ | 0.0214 |

NTS = Nevada Test Site, MDA = material disposal area.

^a Under this option, low-level radioactive waste would be shipped to either the Nevada Test Site or a commercial site in Utah. Transuranic wastes would be shipped to WIPP. Pantex, Y-12, Oak Ridge, Nevada Test site, Lawrence Livermore and the Savannah River Site would ship or receive special nuclear materials. Also note that the number of shipments along the Pojoaque to Santa Fe segment would be lower when the commercial site in Utah is used as an offsite disposal option for low-level radioactive waste.

^b Risk is expressed in terms of latent cancer fatalities, except for the nonradiological risk, where it refers to the number of traffic accident fatalities.

^c Shipments of low-level radioactive waste to a commercial disposal site in Utah would not pass along the Pojoaque to Santa Fe segment of highway.

The values presented in Table K-6 show that the total radiological risks (the product of consequence and frequency) are very small under all alternatives. It should be noted that the

maximum annual dose to a transportation worker would be 100 millirem per year, unless the individual is a trained radiation worker who would have an administratively controlled annual dose limit of 2,000 millirem (DOE 1999b). The potential for a trained radiation worker to develop a latent fatal cancer from the maximum annual exposure is 0.0012 (about 1 chance in 800). Therefore, no individual transportation worker would be expected to develop a latent fatal cancer from exposures during the activities under all alternatives.

Nonradiological accident risks (the potential for fatalities as a direct result of traffic accidents) present the greatest risks. Considering that the transportation activities analyzed in this SWEIS would occur over a 10-year period and the average number of traffic fatalities in the United States is about 40,000 per year (DOT 2006), the traffic fatality risk under all alternatives would be very small.

The risks to various exposed individuals under incident-free transportation conditions have been estimated for hypothetical exposure scenarios identified in Section K.5.3. The estimated doses to workers and the public are presented in **Table K-7**. Doses are presented on a per-event basis (person-rem per event), as it is unlikely that the same person would be exposed to multiple events; for those that could have multiple exposures, the cumulative dose could be calculated. The maximum dose to a crewmember is based on the same individual being responsible for driving every shipment for the duration of the campaign. Note that the potential exists for larger individual exposures if multiple exposure events occur. For example, the dose to a person stuck in traffic next to a shipment of remote-handled transuranic waste for one-half hour is calculated to be 0.012 rem (12 millirem). This is considered a one-time event for that individual.

Table K-7 Estimated Dose to Maximally Exposed Individuals During Incident-Free Transportation Conditions

| <i>Receptor</i> | <i>Dose to Maximally Exposed Individual</i> |
|---------------------------------------|---|
| Workers | |
| Crewmember (truck drivers) | 2 rem per year ^a |
| Inspector | 0.028 rem per event per hour of inspection |
| Public | |
| Resident (along the truck route) | 3.0×10^{-7} rem per event |
| Person in traffic congestion | 0.012 rem per event per one-half hour stop |
| Persons at a rest stop or gas station | 0.00020 rem per event per hour of stop |
| Gas station attendant | 0.00026 rem per event |

^a Maximum administrative dose control level per year for a trained radiation worker (truck crewmember).

A member of the public residing along the route would likely receive multiple exposures from passing shipments. The cumulative dose to this resident can be calculated assuming all shipments passed his or her home. The cumulative dose is calculated assuming that the resident is present for every shipment and is unshielded at a distance of about 98 feet (30 meters) from the route. Therefore, the cumulative dose depends on the number of shipments passing a particular point and is independent of the actual route being considered. If one assumes the maximum resident dose provided in Table K-7 for all transports, then the maximum dose to this resident would be about 37 millirem if all radioactive materials were shipped via this route. This dose corresponds to that for shipments under the Expanded Operations Alternative with the MDA

Removal Option, which has an estimated number of shipments of about 122,450 over 10 years. This dose translates to less than 4 millirem per year, with a risk of developing a latent fatal cancer of 2.4×10^{-6} per year (or one chance in 41,700 that the exposed individual would develop a latent fatal cancer from exposure to all shipments over 10 years).

The accident risk assessment and the impacts shown in Table K–6 take into account the entire spectrum of potential accidents, from a fender-bender to extremely severe accidents. To provide additional insight into the severity of accidents in terms of the potential dose to a MEI and the public, an accident consequence assessment has been performed for a maximum reasonably foreseeable hypothetical transportation accident with a likelihood of occurrence greater than 1 in 10 million per year. The results, presented in Table K–6, include all conceivable accidents, irrespective of their likelihood.

The following assumptions were used to estimate the consequences of maximum reasonably foreseeable offsite transportation accidents:

- The accident is the most severe with the highest release fraction; high-impact and high-temperature fire accident (highest severity category).
- The individual is 330 feet (100 meters) downwind from a ground release accident.
- The individual is exposed to airborne contamination for 2 hours and ground contamination for 24 hours with no interdiction or cleanup. A stable weather condition (Pasquill Stability Class F) with a wind speed of 1 meter per second (2.2 miles per hour) is considered.
- The population is assumed at a uniform density to a radius of 50 miles (80 kilometers), and exposed to the entire plume passage and 7 days of ground exposure without interdiction and cleanup. A neutral weather condition (Pasquill Stability Class D) with a wind speed of 4 meters per second (8.8 miles per hour) is considered. Since the consequences are proportional to the population density, the accident is assumed to occur in an urban area with the highest density, see Table K–1.
- The number of containers involved in the accident is listed in Table K–2. When multiple Type B or shielded Type A shipping casks are transported in a shipment, a single cask is assumed to have failed in the accident. It is unlikely that a severe accident would breach multiple casks.

Table K–8 provides the estimated dose and risk to an individual and population from a maximum foreseeable truck or rail transportation accident with the highest consequences under each alternative and disposal option.

Table K–8 Estimated Dose to the Population and to Maximally Exposed Individuals during Most Severe Accident Conditions

| Alternative | Material in the Accident With the Highest Consequences | Likelihood of the Accident (per year) ^a | Population ^a | | Maximally Exposed Individual ^b | |
|--|--|--|-------------------------|------------|---|----------------------|
| | | | Dose (person-rem) | Risk (LCF) | Dose (rem) | Risk (LCF) |
| No Action | CH-TRU | 1.9×10^{-7} | 310 | 0.186 | 0.0062 | 3.7×10^{-6} |
| Reduced Operations | CH-TRU | 1.9×10^{-7} | 310 | 0.186 | 0.0062 | 3.7×10^{-6} |
| Expanded Operations, MDA Removal Option | CH-TRU | 5.2×10^{-7} | 310 | 0.186 | 0.0062 | 3.7×10^{-6} |
| Expanded Operations, MDA Capping Option ^c | CH-TRU | 2.7×10^{-7} | 310 | 0.186 | 0.0062 | 3.7×10^{-6} |

LCF = latent cancer fatality, CH-TRU = contact-handled transuranic waste, MDA = material disposal area.

^a The population doses, risks, and the likelihood of the accident are presented for an urban area on the transportation route. Population extends at a uniform density to a radius of 50 miles (80 kilometers). The weather condition was assumed to be Pasquill Stability Class D with a wind speed of about 9 miles per hour (4 meters per second).

^b The individual is assumed to be 330 feet (100 meters) downwind from the accident and exposed to the entire plume of the radioactive release. The weather condition is assumed to be Pasquill Stability Class F with a wind speed of 2.2 miles per hour (1 meter per second).

^c The values presented here are also applicable to Expanded Operations without MDA removal or capping.

K.8 Impact of Construction and Hazardous Material Transport

This section evaluates the impacts of transporting materials required to construct new facilities, as well as nonradioactive and hazardous materials generated during each alternative. The construction materials considered are concrete, cement, sand, gravel, dirt, and steel. The impacts were evaluated based on the number of truck shipments required for each of the materials and the distances from their point of origin to the LANL site. The origins of construction materials were assumed to be at an average distance of 100 miles (160 kilometers) from the site. The truck kilometers for all material shipments under each alternative were calculated by summing all of the activities from construction through closure (where applicable). The truck accident and fatality rates were assumed to be those that were provided earlier for the onsite and local area transports. **Table K–9** summarizes the impacts in terms of total number of kilometers, accidents, and fatalities for all alternatives. The results in Table K–9 indicate that there are no large differences in the impacts among all alternatives. Under all alternatives, the expected potential traffic fatalities are very low.

Table K–9 Estimated Impacts of Construction and Operational Material Transport

| Alternative | Total Distance Traveled (kilometers) | Number of Accidents | Number of Fatalities |
|--------------------------------|--------------------------------------|---------------------|----------------------|
| No Action | 5.67×10^6 | 0.64 | 0.070 |
| Reduced Operations | 5.53×10^6 | 0.62 | 0.070 |
| Expanded Operations | | | |
| Without MDA Capping or Removal | 22.08×10^6 | 2.50 | 0.26 |
| With MDA Capping | 24.52×10^6 | 2.77 | 0.29 |
| With MDA Removal | 28.12×10^6 | 3.18 | 0.33 |

MDA = material disposal area.

Note: To convert kilometers to miles, multiply by 0.6214.

K.9 Conclusions

Based on the results presented in the previous section, the following conclusions have been reached (see Tables K-5 through K-9):

- It is unlikely that the transportation of radioactive waste would cause an additional fatality as a result of radiation either from incident-free operation or postulated transportation accidents.
- The highest risk to the public would be under the Expanded Operations Alternative (with the MDA Removal Option) and the Nevada Test Site disposal site option, where about 122,450 truck shipments of radioactive materials would be transported to the Nevada Test Site, WIPP, Pantex, Lawrence Livermore National Laboratory, Oak Ridge (Y-12 Complex and K-25), and the Savannah River Site.
- The lowest risk to the public would be under the Reduced Operations Alternative and a commercial site disposal option, with about 12,270 truck shipments of radioactive materials to similar locations as those in the Expanded Operations Alternative.

The nonradiological accident risks (the potential for fatalities as a direct result of traffic accidents) present the greatest risks. The maximum risks would occur under the Expanded Operations Alternative (with the MDA Removal Option) and the Nevada Test Site disposal site option. Considering that the transportation activities would occur over a 10-year period and that the average number of traffic fatalities in the United States is about 40,000 per year, the traffic fatality risks under all alternatives are very small.

K.10 Long-Term Impacts of Transportation

The *Yucca Mountain EIS* (DOE 2002a, 2007) analyzed the cumulative impacts of the transportation of radioactive material, consisting of impacts of historical shipments of radioactive waste and spent nuclear fuel, reasonably foreseeable actions that include transportation of radioactive material, and general radioactive material transportation that is not related to a particular action. The collective dose to the general population and workers was the measure used to quantify cumulative transportation impacts. This measure of impact was chosen because it may be directly related to LCFs using a cancer risk coefficient. **Table K-10** provides a summary of the total worker and general population collective doses from various transportation activities. The table shows that the impacts of this program are quite small compared with the overall transportation impacts. The total collective worker dose from all types of shipments (historical, the alternatives, reasonably foreseeable actions, and general transportation) was estimated to be about 382,400 person-rem (229 LCFs) for the period 1943 through 2073 (131 years). The total general population collective dose was estimated to be about 343,900 person-rem (206 LCFs). The majority of the collective dose for workers and the general population was due to the general transportation of radioactive material. Examples of these activities are shipments of radiopharmaceuticals to nuclear medicine laboratories and shipments of commercial low-level waste to commercial disposal facilities. The total number of LCFs (among the workers and the general population) estimated to result from radioactive material transportation over the period between 1943 and 2073 is about 435, or an average of less than

4 LCFs per year. Over this same period (131 years), approximately 73 million people would die from cancer, based on the National Center for Health Statistics data on the average annual number of cancer death in the United States of about 554,000, with less than 1 percent fluctuation in the number of cancer fatalities in any given year (CDC 2007). The transportation-related LCFs would be 0.0006 percent of the total number of cancers, therefore, it is indistinguishable from the natural fluctuation in the total annual death rate from cancer.

Table K–10 Cumulative Transportation-Related Radiological Collective Doses and Latent Cancer Fatalities (1943 to 2073)

| <i>Category</i> | <i>Collective Worker Dose (person-rem)</i> | <i>Collective General Population Dose (person-rem)</i> |
|---|--|--|
| Transportation Impacts in this SWEIS^a | 910 ^a | 287 ^a |
| Other Nuclear Material Shipments | | |
| Historical | 330 | 230 |
| Reasonably Foreseeable Actions ^b | 25,300 | 42,200 |
| General Radioactive Material Transport (1943 to 2073) | 350,000 | 300,000 |
| <i>Yucca Mountain EIS</i> ^c (maximum transport) (up to 2073) | 5,900 | 1,200 |
| Total collective dose ^d (up to 2073) | 382,400 | 343,900 |
| Total latent cancer fatalities | 229 | 206 |

^a Maximum values from Tables K–6 for transports from 2007 through 2016.

^b Includes transportation impacts associated with Complex Transformation activities related to radioactive material transports (DOE 2007b, Table 6.3.2-1).

^c Impacts for the Proposed Action in the *Draft Yucca Mountain Supplemental EIS* (DOE 2007, Table 8-14). [Similar impacts in the *Yucca Mountain EIS* (DOE 2002a) were 4600, and 1,600 person-rem for workers and population, respectively.] If DOE decides to expand the program to include all potential high-level and Greater-Than-Class C wastes and spent nuclear fuel (implement inventory Module 2), then the worker and public doses would be about 15,000 and 2,700 person-rem, respectively.

^d The values are rounded to the nearest hundred.

Source: DOE 2002a, 2007.

K.10.1 Uncertainty and Conservatism in Estimated Impacts

The sequence of analyses performed to generate the estimates of radiological risk for transportation includes: 1) determination of the inventory and characteristics, 2) estimation of shipment requirements, 3) determination of route characteristics, 4) calculation of radiation doses to exposed individuals (including estimating of environmental transport and uptake of radionuclides), and 5) estimation of health effects. Uncertainties are associated with each of these steps. Uncertainties exist in the way that the physical systems being analyzed are represented by the computational models; in the data required to exercise the models (due to measurement errors, sampling errors, natural variability, or unknowns caused simply by the future nature of the actions being analyzed); and in the calculations themselves (such as the approximate algorithms used in the computer programs used for the analyses).

In principle, one can estimate the uncertainty associated with each input or computational source and predict the resultant uncertainty in each set of calculations. Thus, one can propagate the uncertainties from one set of calculations to the next and estimate the uncertainty in the final, or absolute, result; however, conducting such a full-scale quantitative uncertainty analysis is often impractical and sometimes impossible, especially for actions to be initiated at an unspecified time in the future. Instead, the risk analysis is designed to ensure, through uniform and judicious

selection of scenarios, models, and input parameters, that relative comparisons of risk among the various alternatives are meaningful. In the transportation risk assessment, this design is accomplished by uniformly applying common input parameters and assumptions to each alternative. Therefore, although considerable uncertainty is inherent in the absolute magnitude of the transportation risk for each alternative, much less uncertainty is associated with the relative differences among the alternatives in a given measure of risk.

In the following sections, areas of uncertainty are discussed for the assessment steps enumerated above. Special emphasis is placed on identifying whether the uncertainties affect relative or absolute measures of risk. The reality and conservatism of the assumptions are addressed. Where practical, the parameters that most affect the risk assessment results are identified.

K.10.2 Uncertainties in Material Inventory and Characterization

The inventories and physical and radiological characteristics are important input parameters to the transportation risk assessment. The potential number of shipments for all alternatives is primarily based on the projected dimensions of package contents, the strength of the radiation field, the heat that must be dissipated, and assumptions concerning shipment capacities. The physical and radiological characteristics are important in determining the material released during accidents and the subsequent doses to exposed individuals through multiple environmental exposure pathways.

Uncertainties in inventory and characterization are reflected in the transportation risk results. If the inventory is overestimated (or underestimated), the resulting transportation risk estimates are also overestimated (or underestimated) by roughly the same factor. However, the same inventory estimates are used to analyze the transportation impacts of each of the alternatives. Therefore, for comparative purposes, the observed differences in transportation risks among the alternatives, as given in Table K-6, are believed to represent unbiased, reasonably accurate estimates from current information in terms of relative risk comparisons.

K.10.3 Uncertainties in Containers, Shipment Capacities, and Number of Shipments

The transportation required for each alternative is based in part on assumptions concerning the packaging characteristics and shipment capacities for commercial trucks. Representative shipment capacities have been defined for assessment purposes based on probable future shipment capacities. In reality, the actual shipment capacities may differ from the predicted capacities such that the projected number of shipments and, consequently, the total transportation risk, would change. However, although the predicted transportation risks would increase or decrease accordingly, the relative differences in risks among alternatives would remain about the same.

K.10.4 Uncertainties in Route Determination

Analyzed routes have been determined between all origin and destination sites considered in the SWEIS. The routes have been determined to be consistent with current guidelines, regulations, and practices, but may not be the actual routes that would be used in the future. In reality, the actual routes could differ from the representative ones with regard to distances and total

population along the routes. Moreover, because materials could be transported over an extended time starting at some time in the future, the highway infrastructure and the demographics along routes could change. These effects have not been accounted for in the transportation assessment; however, it is not anticipated that these changes would substantially affect relative comparisons of risk among the alternatives considered in the SWEIS. Specific routes for certain shipments cannot be identified in advance because the routes are classified to protect national security interests.

K.10.5 Uncertainties in the Calculation of Radiation Doses

The models used to calculate radiation doses from transportation activities introduce a further uncertainty in the risk assessment process. Estimating the accuracy or absolute uncertainty of the risk assessment results is generally difficult. The accuracy of the calculated results is closely related to the limitations of the computational models and to the uncertainties in each of the input parameters that the model requires. The single greatest limitation facing users of RADTRAN, or any computer code of this type, is the scarcity of data for certain input parameters. Populations (off-link and on-link) along the transportation routes, shipment surface dose rates, and individuals residing near the routes are the most uncertain data in dose calculations. In preparing these data, one makes assumptions that the off-link population is uniformly distributed; the on-link population is proportional to the traffic density, with an assumed occupancy of two persons per car; the shipment surface dose rate is the maximum allowed dose rate; and a potential exists for an individual to be residing at the edge of the highway. It is clear that not all assumptions are accurate. For example, the off-link population is mostly heterogeneous, and the on-link traffic density varies widely within a geographic zone (urban, suburban, rural). Finally, added to this complexity are the assumptions regarding the expected distance between the public and the shipment at a traffic stop, rest stop, or traffic jam and the afforded shielding.

Uncertainties associated with the computational models are reduced by using state-of-the-art computer codes that have undergone extensive review. Because many uncertainties are recognized but difficult to quantify, assumptions are made at each step of the risk assessment process that are intended to produce conservative results (such as overestimating the calculated dose and radiological risk). Because parameters and assumptions are applied consistently to all alternatives, this model bias is not expected to affect the meaningfulness of relative comparisons of risk; however, the results may not represent risks in an absolute sense.

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APPENDIX L
CATEGORICAL EXCLUSION SUMMARY

APPENDIX L

CATEGORICAL EXCLUSION SUMMARY

The U.S. Department of Energy (DOE) National Environmental Policy Act (NEPA) Implementing Procedures identify classes of actions that DOE has determined do not individually or cumulatively have a significant effect on the human environment (Title 10 *Code of Federal Regulations* [CFR] Part 1021 Subpart D). Appendix B of Subpart D, “Categorical Exclusions Applicable to Specific Agency Actions,” identifies conditions that are integral elements of the classes of action that are categorically excluded. These conditions are that a proposed activity would not threaten a violation of applicable statutory, regulatory, or permit requirements for environment, safety or health, including requirements of DOE and Executive Orders; require siting and construction or major expansion of waste storage, disposal, recovery, or treatment facilities; disturb hazardous substances, pollutants, or contaminants that preexist in the environment such that there would be uncontrolled or unpermitted releases; or adversely affect environmentally sensitive resources. These classes of items are normally “categorically excluded” from the need for the preparation of an environmental assessment or environmental impact statement. The Los Alamos National Laboratory (LANL) experience has shown that there are groups of actions or activities that meet the standard for receiving a categorical exclusion from further NEPA analysis. These activities range from facility work, such as routine maintenance and safety and environmental improvements, to research and development activities in chemistry, materials science, detector technology, geology, and other areas. The following sections describe the range and types of activities (LANL 2007) that are performed in Key or non-Key Facilities at LANL that would typically receive a categorical exclusion.

Routine Maintenance Activities

Maintenance activities are frequently and routinely performed for operational support of LANL facilities and property. These actions range from ongoing custodial services to corrective, preventive, and predictive actions required to maintain and preserve buildings, structures, roads, infrastructure, and equipment in a condition suitable for fulfillment of their designated purpose. Such activities are intended to maintain current operations and do not substantially extend the useful life of a facility or allow for substantial upgrades or improvements. Routine maintenance includes maintenance, repair, replacement, removal, relocation, fabrication, and installation actions.

Safety, Environmental, and Equipment Improvements

LANL staff routinely conducts safety and environmental improvements to facilities, including the installation of and improvements to equipment for personnel safety and health. This includes installation, replacement, or improvements to alarm systems and monitors, bottled gas racks, electrical components, guardrails, air and water filtration devices, safeguards and security equipment, nondestructive assay instruments, remote monitoring systems, emergency exits, radiation shielding, door interlocks, and similar systems. Facility safety risks are reduced by improving containment of hazardous materials, installing remote handling equipment, providing firebreaks and fire roads, and other related actions. Risks to the public are reduced by

eliminating contaminants in outfalls, removing underground storage tanks, and installing water disinfection tanks, among other activities. Environmental improvements include minor operational changes and equipment additions or modifications that reduce the volume of waste produced, and facilitate reuse and recycling of materials.

Support Structure Activities

LANL staff constructs, modifies, and operates support buildings and other structures within or contiguous to developed areas. Support buildings and structures are those used for offices, health services, welding shops, storage space, vehicle maintenance, waste collection and staging areas, and other purposes. Construction and modification activities include providing elements needed for proper functioning of the structures, such as fencing, aboveground storage tanks, parking lots, utilities, and ducting. LANL staff constructs short new access roads and modifies existing roads to improve access to and within technical areas (TAs), to facilitate traffic and pedestrian flow, and to improve worker safety. New support buildings and structures are constructed, and existing structures (such as transportables, trailers, and tension domes), their contents, and processes are relocated. Support buildings and structures that are vacated and determined to be excess to current and foreseeable needs are decommissioned. Decommissioning may include decontamination activities and removal or demolition. Cultural resource evaluations are completed prior to demolition.

General Shop Operations

LANL activities and operations are supported by a variety of shops, including machine shops, carpentry shops, and electronics shops. Many different types of equipment are used, including drill presses, lathes, bench grinders, table saws, sanders, welding equipment, small power tools, hand tools, and other common shop equipment. Commonly used materials include nonhazardous metals, ceramics, wood, plastics, rubber, epoxies and glues, paint, solder, sealant, small quantities of cleaning solvents, and other common shop materials. Specialized shops may also use a variety of hazardous or radioactive materials in fabrication and construction.

Security and Protection Operations

A live firing range and a live-fire shoot house at TA-72 are used to train protective force personnel to meet DOE and LANL protective force requirements. LANL's TA-49 firing site facility is used to train LANL employees and other Federal and state agency personnel to identify suspect devices and properly respond to bomb threats. This training includes demonstration of a variety of standard explosive materials and response devices (such as a disrupter that uses a high-pressure jet of liquid to quickly disassemble electronics within a simulated suspect explosive device).

Radiation Detection and Monitoring Training

LANL trains personnel from LANL, other DOE facilities, and other Federal and state agencies in the use of radiation detectors and monitors. The purpose of the training is teach and demonstrate procedures for determining the contents of vehicles, equipment, buildings, or other structures that contain radiation sources, hazardous material surrogates, or radioactive materials, including small

quantities of special nuclear material. Training is conducted in buildings and outdoor areas that meet the appropriate safety and authorization basis criteria.

Wildfire Response

The Interagency Helibase Operation is located at the junction of the entrance road to TA-49 and State Road 4 and is used for wildfire response and storage for interagency wildfire response equipment and supplies. Personnel from LANL, Los Alamos County, the National Park Service, and the U.S. Forest Service staff the facility, which consists of three helicopter pads (helipads), two at-grade dip tanks (one 1500-gallon (5,680-liter) and one 3500-gallon (13,250-liter)); a building that houses two fire engines, fire equipment, and office space for emergency management; an office trailer; and other associated infrastructure. During fire season, helicopter crews plus additional maintenance staff also staff the facility.

Environmental Characterization and Limited Removals

LANL staff routinely conducts short-term, low-cost environmental actions to characterize and reduce risks to human health or the environment from the release or threat of release of hazardous substances. Field investigations that include screening for radiological materials or volatile organic vapors are used to determine the types and locations of contaminants. Temporary onsite immunoassay laboratory and equipment are used to aid the screening process. Corrective actions may include excavation or consolidation of contaminated soils or materials; removal of containers of hazardous substances or petroleum products; removal of underground storage tanks; repair or replacement of leaking containers; containment of contaminated soils or sludges; drainage or closing of manmade surface impoundments; use or stabilization of berms or other above- or belowground barriers to the spread of contamination; or installing runoff or runoff diversion structures. Additional actions may include segregation of potentially reactive wastes; use of chemicals or other materials to neutralize wastes or to retard the spread of contaminants, or to mitigate their consequences; installation of ventilation systems in soil to remove methane or petroleum vapors; or installation of fences, signs, or other site control precautions. Finally, if the water supply of a household or industry becomes contaminated, an alternative water supply may be provided until the contaminated water source is remedied.

Hydrology, Geology, and Geochemistry Research

Basic and applied hydrology, geology, and geochemistry research studies are conducted on rock, concrete, soil, and other geological samples. Outdoor hydrological and geochemistry field experiments are conducted at TA-51 and other LANL locations. Laboratory and outdoor research is focused on various areas including transport of contaminants in saturated and unsaturated hydrologic systems, carbon sequestration, basin-scale hydrology, zero-emission coal technology, volcanic geology and hazards, and planetary astrobiology and geology. Thousands of geological samples are analyzed annually, and instrumentation for conducting these studies is designed, tested, or modified. A number of different laboratories and capabilities are used, including a wet chemistry laboratory, an x-ray diffraction laboratory, thermal analysis capabilities, optical equipment, a light-stable isotope laboratory, electron microanalysis, an x-ray fluorescence laboratory, and a mass spectrometry laboratory. Equipment used includes, but is not limited to, electron microprobes, infrared spectrometers, optical microscopes, scanning

electron microscopes, scanning probe microscopes, inductively coupled plasma emission spectrometers, gas chromatographs, mass spectrometers, ion-liquid chromatographs, atomic absorption spectrometers, high-pressure liquid chromatographs, gas chromatographs, x-ray diffractometers, x-ray fluorescent spectrometers, autoclaves, and similar equipment.

Atmospheric, Climate and Environmental Dynamics

Research is performed using modeling, simulation, field measurements, and data analysis in the atmospheric, ocean, and ecohydrologic sciences. Types of projects include: (1) atmospheric, climate, and ocean modeling (wildfire behavior modeling, biogeochemistry and ocean carbon cycle modeling, climate applications to high performance computing); (2) ecology (semiarid systems ecology, soil science, carbon sequestration, micrometeorological instrumentation and analysis); (3) hydrology (surface and subsurface modeling, water resource prediction, contaminant fate and transport, erosion); and (4) weapons phenomenology and infrasound (physics and chemistry of atmospheric composition, theory and modeling of electromagnetic radiation, data analysis from satellites and ground sensors) and (5) others in these fields.

Geotechnical Engineering and Research

Geotechnical research includes underground and surface geologic, seismic, volcanic, hydrologic, hydrogeologic, geophysical, and geochemical field testing, monitoring experiments, and managing of samples. Research includes studies in support of geologic repositories such as Yucca Mountain, including evaluating engineering barrier systems, coordinating field testing, and studying the potential effects of a volcanic eruption.

Environmental Geology and Spatial Analysis

Environmental geology and spatial analysis research focuses on studying uncertainties associated with complex natural environmental systems and solving problems that arise as the result of human activities. Research capabilities include volcanic and seismic hazards, geomorphology and surface processes, geochemistry, geographic information systems, environmental modeling and risk assessment, and quality assurance and data validation. Researchers conduct the quality assurance program at Yucca Mountain; perform environmental restoration work at LANL to evaluate existing human health and ecological risks from contaminants that have entered the canyon areas; evaluate seismic hazards to LANL's nuclear facilities; and conduct paleoseismic and structural geology studies.

Geophysics

Basic and applied geophysics research at LANL involves exploring the seismic and acoustic signals that provide information about natural and manmade disturbances within the Earth's crust. Research is conducted in the following areas: (1) nuclear explosion monitoring (processing and interpreting geophysical and geological data for the national ground-based nuclear explosion monitoring program); (2) geodynamics (developing and applying computational tools and experimental methods for predicting the response of geological materials to large and rapid deformations); (3) seismic modeling and imaging (conducting basic and applied research in wave propagation, seismic imaging, scattering, and the interaction of

acoustic waves with rock mass structure, fabric, and pore fluids); (4) drilling (developing advanced drilling methods and tools for drilling operations for LANL environmental restoration activities and for oil exploration for National Energy Security); and (5) national defense (offering geology/geophysics expertise in the geologic phenomena associated with explosion dynamics both subsurface and above ground, and intelligence gathering and interpretation using remote sensing techniques).

Planetary Physics

Scientists promote and coordinate basic research on the origin, structure, and evolution of the Earth, the Solar System, and the Universe and develop the science base to predict future changes as they affect human life. Research is conducted in the following areas: (1) astrophysics (theoretical, observational, and instrumentation research on gamma-ray astrophysics, space instrumentation, stellar dynamics, and other topics); (2) space physics (theoretical, computational, and observational research into the plasma environment of the Earth); and (3) solid planetary geoscience (numerical, seismic, paleomagnetic, and laboratory studies of the geophysical and geochemical structure, properties, processes, and fluid dynamics of terrestrial and giant planets).

Archaeological Site Evaluation

Qualified LANL personnel evaluate archaeological sites in LANL TAs and surrounding locations (such as U.S. Forest Service land) to establish site integrity that would subsequently be used to determine National Register of Historic Places eligibility. Both invasive and noninvasive evaluation techniques are used. Geophysical instrumentation (such as ground penetrating radar) is used to identify the location of potential subsurface archaeological deposits. Auger holes or shovel tests are used to determine if intact subsurface cultural deposits exist at specific grid locations across the site. Test pits are used to verify the existence of deposits that have been suggested by other tests.

Biological Field Studies

LANL biologists conduct field studies to inventory, monitor, and assess vegetation and animal populations. Vegetation, fruit, and produce samples may be collected from LANL or offsite locations for analysis of biomass, fuel-loading, contamination, or other attributes. Small-scale netting or live trapping is conducted to collect specimens for examination. Reproductive patterns, species distribution and densities, and habitat use are recorded. Specimens may be marked before release for later identification. LANL scientists may also conduct phytoremediation and bioremediation studies in both natural and constructed settings.

Water and Soil Monitoring

Water monitoring stations are installed, maintained, and operated to measure flows, evaluate water quality, and test for contamination. Locations for monitoring stations are based on the characteristics to be studied. The locations are reviewed by cultural and biological resources specialists to ensure protection of sensitive resources. Soils and sediments are sampled regularly from a variety of LANL and offsite locations.

Groundwater monitoring wells are used to monitor groundwater characteristics and determine the presence of contamination. Locations are reviewed by cultural and biological resources specialists to ensure protection of sensitive resources. The monitoring wells are designed to prevent surface contamination from reaching subsurface water.

Automation and Robotics Research and Fabrication

Researchers develop automated and robotic systems (such as mills and lathes) in support of the National Nuclear Security Administration's Stockpile Stewardship Program. These systems increase worker productivity, reduce human exposure to hazardous situations, and minimize overall waste production. Prototypes are developed and tested in nonradioactive laboratories, then transferred to radioactive facilities throughout the DOE nuclear complex. Personnel design parts and conduct small-scale production, mechanical and electrical assembly and integration, system operation and integration, and prototype instrument testing on nonhazardous materials.

Electronic Control Systems Fabrication

Electronic control systems are fabricated for industrial, academic, and Federal agency applications. These systems control many different apparatuses, such as remote-handling systems, radiofrequency systems, lasers, experimental devices, surveillance equipment, alarm and safety equipment, measurement systems, and many others; they monitor performance, control operating parameters, and serve other similar functions. Personnel construct control systems, write software to control those systems, and then integrate them with the apparatus being controlled.

Antenna and Pulse Power Outdoor Test Range

The Antenna and Pulse Power Outdoor Test Range is a 1400-acre facility that is used for open air testing and field development of very-high-power radiofrequency and high-power-microwave sources and antennas to support DOE and Department of Defense equipment requirements. Antenna design and fabrication is conducted within laboratory space at TA-49. The facility also is used to design, construct, and test specialized diagnostic equipment for testing high-power radiofrequency and microwave sources.

Small-Scale Basic Laser Science Research and Development

Basic laser science research focuses on combining traditional analytical instrumentation with lasers. Research areas include chemical kinetics, materials processing and characterization, fluid chemistry, spectroscopic characterization, chemical diagnostics, and mass spectrometry diagnostics. Researchers use traditional analytical instrumentation and lasers in new ways, for example by combining two methodologies into one instrument, developing field-usable instruments for measuring samples in real-time, developing new sampling techniques, or developing new uses for existing analytical instrumentation. Many types of equipment are used, such as mass spectrometers, radiation detectors, gas chromatographs, infrared and visible lasers, and light detecting and ranging systems.

Industrial Hygiene Research and Development

Personnel conduct industrial-hygiene-related research and development activities that anticipate, recognize, evaluate, and control health and safety hazards in the workplace. This work includes design and testing of respiratory protection and other personal protective devices, including respirators, respirator cartridges or canisters, protective suits, self-contained breathing apparatus, and similar equipment. Both commercially available equipment and LANL shop-fabricated equipment are used.

Radiation Monitoring Techniques

Researchers develop and test techniques and instrumentation for nondestructive monitoring and detection of radiation sources. These nondestructive measurements work by detecting and analyzing radioactive emissions from nuclear materials. Both active and passive techniques are used to accurately measure the mass of nuclear materials in an object. Active techniques involve bombarding nuclear materials with neutrons or gamma rays, then detecting emitted radiation. Such techniques may use a variety of sources including isotopic sources, deuterium-tritium neutron generators, or portable linear accelerators. Passive techniques do not involve active bombardment of the material to be measured, but measure some characteristic of the material or constituents of the material using such techniques as calorimetry, which involves measuring the heat generated by nuclear materials. Most instrumentation consists of printed circuit boards, electronics equipment, and mechanical assemblies, constructed both in LANL shops and by external vendors.

Physical Detector Research and Development

For physical science research, researchers develop and use a wide variety of detectors capable of identifying and measuring ionizing radiation, x-rays, photons, electrical and magnetic fields, chemicals, gases, pressure, gravity, explosives, biological materials, dense materials, and other materials. The detectors consist of a medium that responds to the primary condition of interest, such as liquid (for example, mineral oil), solid (for example, crystalline materials), or gaseous materials (for example, isobutane) in a support housing for mechanical and electrical stability, coupled to electronic circuitry and assemblies. Researchers characterize physical media, then fabricate and test detectors using a variety of equipment and materials.

Advanced Image Sensor Research and Development

Sensitive and fast sensors and imaging systems are developed for weapons and nonweapons applications, including “smart” weapons, tracking systems, and high-speed data acquisition. Equipment used to develop these sensors and imaging systems includes computers, oscilloscopes, voltmeters, arbitrary function generators, image monitors, optical light sources, high-voltage power supplies, charge-coupled device cameras, commercial image intensifiers, and lasers.

Space and Atmospheric Instrumentation

Flight hardware, satellite instrumentation, and small satellite systems are developed at LANL. Flight hardware and satellite instrumentation are used for remote sensing applications, such as nonproliferation, detection of nuclear explosions, climate studies, and environmental measurements. Types of instrumentation typically developed include optical and infrared remote sensing instruments; x-ray, gamma-ray, neutron, alpha particle, radiofrequency, and energetic particle measurement instruments; astrophysical instruments for conducting studies of the atmosphere, ionosphere, magnetosphere, and solar wind; and other instrumentation for deployment on satellites or other atmospheric testing vehicles. Outdoor experiments are often conducted as part of this research, to measure fluctuations in the atmosphere and ionosphere and to calibrate satellite receivers that are in orbit. Outdoor experiments are conducted at various locations around LANL, the United States, and around the world.

Materials Characterization Research and Development

Researchers study a number of different materials to determine molecular structure, thermal conductivity, electronic magnetization, heat capacity, thermal expansion, resistance, and other properties. Materials characterized include transition metals and metal oxides, rare earth metal and intermetallic compounds, ceramics, crystals, polymers, amino acids, and others. Personnel prepare samples as necessary and characterize them using equipment such as magnetic resonance imagers, magnetometers, laser interferometers, ultraviolet lights, and x-rays. Research also includes developing techniques for improving equipment sensitivity in detecting certain responses.

General Optical Characterization and Calibration

LANL staff performs optical characterization for a variety of applications; this includes measuring solar radiation and reflectance from computer chips and wafer samples. Staff members use light signals such as lamps having different wavelengths, including visible, infrared, ultraviolet, and vacuum ultraviolet. Light is shone onto the component, and calibrated detectors and other measuring devices (such as reflectometers) are used to measure the reflectance or transmission of the light. Low-level lasers are used to align the light signal onto the test component being characterized and onto the detector.

Ion Beam Materials Science Laboratory Research

Researchers characterize and modify surfaces using ion beams at the Ion Beam Materials Science Laboratory at TA-3, Building 34. The main experimental equipment includes a 3-megavolt tandem accelerator and a 200-kilovolt ion source implanted together with several beam lines. A series of experimental stations are attached to each beam line; they include the nuclear microprobe, surface modification, ultra-high vacuum, small stainless steel, and general-purpose experimental chambers. Samples used in the Ion Beam Materials Science Laboratory include geological samples, metallic films, polymers, ceramics, metal alloys, plutonium-contaminated metal, and metal semiconductors.

High Magnetic Field Research

Researchers study the behavior of materials under very high strength magnetic fields that are produced by pulsed magnets powered by high-voltage stored energy systems. Research is normally conducted at TA-35, Building 125. Magnets currently in operation have maximum magnetic field intensities ranging from 20 to 300 tesla. Very small samples of a wide variety of materials are studied, including plutonium-239 and plutonium-242, depleted uranium, thorium compounds, high-temperature superconductors, and other metals and semiconductors.

Ultra-High Strength and High Energy Density Materials Research and Development

LANL researchers investigate, evaluate, and demonstrate new ultra-high strength materials and very high energy density materials. Ultra-high strength materials are produced using a variety of metals, including copper, silver, or aluminum, which are encapsulated in glass and heated and drawn into small wires. Thin-film samples of high-density materials are synthesized under nonequilibrium conditions. Both materials are characterized by measuring the material composition, chemical structure, mechanical and thermal properties, and energy content and release of these materials.

X-Ray Tomography and Ultrasound Testing

Researchers x-ray (using computed tomography) and ultrasonically analyze samples of sand, soil, plastics, foam, mock high explosives, composite materials, pressure vessels, or other nonradioactive specimens, as well as specimens containing naturally occurring radioactivity such as rocks and soils. The computed tomography equipment is used to generate three-dimensional images and density maps and to detect cracks or flaws, or precisely locate parts or features within an object. The ultrasonic equipment is used to detect cracks, voids, inclusions, and density variations. Techniques are combined to determine if data from the two methods improve evaluation of the sample.

Materials Science Research and Development at the Los Alamos Neutron Science Center

Small-scale experiments using the beam at the Los Alamos Neutron Science Center encompass a wide range of research topics, including materials science, engineering, condensed-matter physics, geoscience, chemical science, biological sciences, and fundamental neutron science. Research includes viewing and studying defects in light materials that lie inaccessibly beneath heavy materials, well beyond the range of x-rays; measuring the behavior of materials under extreme conditions, such as high temperature or pressure; studying the interior of materials to obtain either microscopic or structural information; and imaging hydrogenous material, such as water or oil, in parts or components to deduce lifetimes, corrosion, safety, and quality control issues. Both neutron- and proton-induced experiments are conducted.

Energetic Neutral Beam Facility Research and Development

The Energetic Neutral Beam Facility, located at TA-46, Building 31, consists of two neutral beam sources and is used by personnel from other Federal agencies, universities, and industry. The beam sources have diagnostic capabilities that include mass spectrometry and time-of-flight. The primary activity at this facility is to investigate surfaces, specifically gas-surface interactions,

including scattering or reaction mechanisms, or both. Thin film work and detector studies using sealed sources are also conducted. The first beam source produces continuous high-energy atomic beams with energies from approximately 1 to 5 electron volts. The second beam source is a continuous medium-energy molecular beam source.

Basic and Applied Chemistry Research and Development

Chemistry research and development at LANL supports a number of programs. The programs and purpose of chemistry research include: 1) nuclear weapons support that focuses on planning the next generation of nuclear facilities for safely handling actinide metals and their compounds; 2) nonproliferation and counterproliferation and Homeland Security support that focuses on detecting, preventing, assessing, and responding to nuclear, chemical, and biological threats; 3) isotope science support that focuses on the production of medical radioisotopes and the development of a national isotope strategy with other DOE laboratories to rejuvenate the U.S. isotope production capability and encourage research; 4) applied energy research that studies novel methods of hydrogen production, storage, and utilization; carbon measurement, management, and carbon dioxide sequestration; and other research areas; and 5) nanoscale science and engineering that focuses on nanoscale chemical synthesis and processing, chemical kinetics and molecular dynamics, and instrumentation and diagnostics. Chemistry operations are focused on instrumental analysis and spectroscopy, synthetic chemistry, materials chemistry, analytical chemistry and sample preparation, beryllium work, pressure work, radiochemistry and radiological work, biological chemistry, and explosives work. These operations use a variety of equipment and materials and occur LANL-wide.

Electronic and Electrochemical Materials and Devices Research and Development

LANL staff conducts research on electronic and electrochemical materials and devices that are relevant to a wide range of areas, including electrochemistry and the fuel cell program; semiconductor physics research and device development; high temperature superconductivity; general electronic materials characterization and theory; and nondestructive testing through acoustic techniques. Researchers develop and fabricate prototype electronic and electrochemical devices (including fuel cells, sensors, polymer light emitting diodes, and others) and conduct physical and chemical material analyses in support of these activities. Part of this effort involves synthesizing and processing materials, such as polymers and complex oxides.

Advanced Oxidation Technology Research and Development

Advanced oxidation technology research involves the generation and use of highly reactive free radicals, such as oxygen, hydroxide, hydrogen, and nitrogen, as efficient chemical energy sources for breaking molecular bonds in organic compounds. Advanced oxidation technologies are nonthermal and require no chemical additives; therefore, large secondary waste streams are not generated. Advanced oxidation technology can be used to treat a variety of hazardous components in aqueous- and gaseous-based effluents, such as contaminated soil or groundwater, diesel- or aircraft-engine exhaust, and incinerator offgases. The free radicals involved in advanced oxidation technologies either reduce or oxidize chemicals to simpler, less hazardous, or benign components. Nonthermal plasma is a technique currently used; similar nonthermal techniques are also being studied.

High-Temperature/High-Pressure Fluids Research and Development

Research is conducted to develop, test, and verify high-temperature and high-pressure fluid technologies, including hydrothermal processing, “supercritical” water oxidation, “supercritical” carbon dioxide, and similar technologies. When certain fluids are driven by high temperatures and pressure to the “supercritical” region, they may be used as a gas and as a liquid. These supercritical fluids are particularly useful as solvents. Researchers explore these technologies by conducting basic research on the physical properties of fluids and other materials, reaction kinetics and process parameters, oxidation and reduction chemistry, and related chemical reactions. They also apply these technologies to many uses, including precision cleaning, extraction of contaminants and residual solvents, chemical synthesis, polymer synthesis, chemical waste destruction (such as hazardous, mixed, or high explosives waste), semiconductor processing, chemical separations, materials modification, and other applications.

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APPENDIX M
CONTRACTOR DISCLOSURE STATEMENT

**NEPA DISCLOSURE STATEMENT FOR PREPARATION OF A SITE-WIDE EIS
FOR CONTINUED OPERATION OF LOS ALAMOS NATIONAL LABORATORY,
LOS ALAMOS, NEW MEXICO**

CEQ regulations at 40 CFR 1506.5(c), which have been adopted by DOE (10 CFR 1021), require contractors who will prepare an EIS to execute a disclosure specifying that they have no financial or other interest in the outcome of the project. The term "financial interest or other interest in the outcome of the project," for the purposes of this disclosure, is defined in the March 23, 1981 guidance "Forty Most Asked Questions Concerning CEQ's National Environmental Policy Act Regulations," 46 FR 18026-18038 at Question 17a and b.

"Financial or other interest in the outcome of the project 'includes' any financial benefit such as a promise of future construction or design work in the project, as well as indirect benefits the contractor is aware of (e.g., if the project would aid proposals sponsored by the firm's other clients)," 46 FR 18026-18038 at 18031.

In accordance with these requirements, the offeror and any proposed subcontractors hereby certify as follows: (check either (a) or (b) to assure consideration of your proposal)

- (a) X Offeror and any proposed subcontractor have no financial interest in the outcome of the project.
- (b) _____ Offeror and any proposed subcontractor have the following financial or other interest in the outcome of the project and hereby agree to divest themselves of such interest prior to award of this contract.

Financial or Other Interests:

- 1.
- 2.
- 3.

Certified by:



Signature

Elizabeth C. Saris

Name

Vice President

Energy Solutions Operations

November 2005

Date

**NEPA DISCLOSURE STATEMENT FOR PREPARATION OF A SITE-WIDE EIS
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Financial or Other Interests:

- 1.
- 2.
- 3.

Certified by:

Signature



Timothy G. George

Name

President

Time Solutions Corporation

June 2005

Date

**NEPA DISCLOSURE STATEMENT FOR PREPARATION OF A SITE-WIDE EIS
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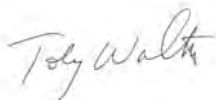
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- (b) _____ Offeror and any proposed subcontractor have the following financial or other interest in the outcome of the project and hereby agree to divest themselves of such interest prior to award of this contract.

Financial or Other Interests:

- 1.
- 2.
- 3.

Certified by:



Signature

Toby Walters, Program Manager
URS Corporation

Name

5/17/07

Date

